Advantages of electro-Fenton over electrocoagulation for

2 disinfection of dairy wastewater

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12 Abstract

This study is focused on the disinfection of raw dairy wastewater by means of a sequential 13 14 treatment including an electrocoagulation (EC) step with an Fe|Fe cell followed by electro-Fenton (EF) or UVA-assisted photoelectro-Fenton (PEF). The two latter methods were run with 15 an air-diffusion cathode for H₂O₂ generation and either a boron-doped diamond (BDD) or a 16 RuO2-based anode. The inactivation of heterotrophic and lactic acid bacteria, Escherichia coli 17 and enterococci was assessed. Low removal of organic load was found in all cases, whereas the 18 19 bacteria were poorly removed by the flocs formed in EC but largely inactivated in EF and PEF. EF was also advantageous because it prevented the formation of harmful sludge containing 20 active bacteria, in contrast to EC. Heterotrophs were the most stable bacteria, whereas the others 21 22 were totally inactivated in most cases. In the sequential EC/EF process involving a BDD anode 23 in the latter step, the inactivation rate for the lactic acid bacteria was higher at circumneutral pH, due to the great ability of produced active chlorine to oxidize the molecules of the cell 24 25 walls. The use of a RuO₂-based anode also led to a quick inactivation at pH 3.0. A better performance was achieved when PEF replaced EF, regardless of the anode, owing to the 26 enhanced bacterial inactivation by UVA radiation. The raw dairy wastewater at natural pH 5.7 27 treated by single EF step with a RuO₂-anode also yielded a faster removal of lactic acid bacteria, 28 Escherichia coli and enterococci as compared to BDD, always remaining small contents of 29 30 active heterotrophs in solution.

Keywords: Dairy wastewater; Electrocoagulation; Electro-Fenton; Heterotrophic bacteria;
Lactic acid bacteria; Photoelectro-Fenton

33 **1. Introduction**

Milk processing in caseiculture consumes large quantities of water, producing about 10 L 34 of wastewater per liter of processed milk [1]. Dairy wastewater is composed of high 35 concentrations of organic matter, salts and bacteria, and its management is difficult because of 36 its variable composition. In general, it contains different proportions of process water, non-37 valorized cheese whey and cleaning water [2]. As a result, it contains milk and whey proteins, 38 along with other components such as sodium, calcium, chloride or lactic acid [3]. Before its 39 discharge into the sewer system, it is necessary to reduce both, bacterial content and organic 40 matter load. Lactose (0.18-45 g L⁻¹), proteins (1.8-34 g L⁻¹) and fat (0.08-6 g L⁻¹) account for 41 the largest part of chemical oxygen demand (COD) and biological oxygen demand (BOD) [4,5]. 42 The whey proteins are globular and are composed of 60% β -lactoglobulin, 22% α -lactalbumin, 43 9% immunoglobulins and 5.5% bovine serum albumin. 44

Electrocoagulation (EC) and Fenton-based treatments seem the most promising technologies to remove the bacteria and organic matter from dairy wastewater [5,6]. EC is an efficient, environmentally friendly phase-separation method based on the release of Fe^{2+} or Al^{3+} ions from sacrificial Fe and Al anodes [7-10]. Reaction (1) causes the dissolution of the Fe anode. The released Fe^{2+} can then be converted into $Fe(OH)_3$ in the presence of O₂ by reaction (2). At the cathode, OH⁻ ion and H₂ gas is formed from reaction (3).

51 Fe
$$\rightarrow$$
 Fe²⁺ + 2e⁻ (1)

52
$$4Fe + 10H_2O + O_2(g) \rightarrow 4Fe(OH)_3(s) + 4H_2(g)$$
 (2)

53
$$2H_2O + 2e^- \rightarrow 2OH^- + H_2(g)$$
 (3)

Iron hydroxides (Fe(OH)₂ and Fe(OH)₃) are relatively non-toxic and form flocs that allow pollutant removal, yielding a sludge that may precipitate [11]. The flocs entrap colloidal particles by surface complexation or electrostatic attraction and by sweep flocculation [12]. Additionally, the H_2 gas bubbles generated at the cathode cause the flotation of some pollutants and, consequently, the separation process is facilitated [13]. As a conventional electrochemical method, EC requires simple equipment and is easy to operate. The periodic replacement of the sacrificial anodes, their passivation and the electricity cost have been reported as the main drawbacks of this technology.

Several authors used EC for disinfection in urban wastewater treatment facilities 62 (WWTFs), describing total inactivation (>99.99%) of *Escherichia coli* [14-16], total coliforms 63 [17,18] or Staphylococcus aureus [19]. EC has also been applied to minimize the organic load 64 of dye and textile wastewater [13,20-23], urban wastewater [24], olive oil mill wastewater [25] 65 66 and cheese whey or dairy wastewater [3,26-29]. For a synthetic whey solution, Un et al. [3] described a maximum COD removal of 86.4% using a reactor in continuous with Fe electrodes 67 and proposed a mathematic model to explain the abatement based on response surface 68 69 methodology. Similarly, for a deproteinated whey wastewater, Guven et al. [26] found a maximum COD decay of 53.3% after 8 h of EC with Fe electrodes at a cell voltage of 11.3 V. 70 Fayad et al. [28] obtained total removal of whey proteins from wastewater of pH 4 using Al 71 electrodes in batch mode at 4.5 A. However, no previous studies about bacterial removal from 72 whey and dairy wastewater have been reported in the literature. 73

74 Electrochemical advanced oxidation processes (EAOPs) based on Fenton's reaction chemistry like electro-Fenton (EF) and photoelectro-Fenton (PEF) are also becoming 75 interesting approaches for the removal of organic pollutants from wastewater [30-33]. In EF, 76 the strong oxidant hydroxyl radical (•OH) is generated in the bulk solution from Fenton's 77 reaction (4). The most characteristic feature is the cathodic H_2O_2 electrogeneration from the 78 two-electron reduction of injected O_2 at Fenton's optimum pH \approx 3. Suitable cathodes for H₂O₂ 79 production are carbon felt [34-37] and carbon-polytetrafluoroethylene (PTFE) coated on air-80 diffusion substrates [38-41]. The PEF process involves additional illumination of the solution 81

with UVA light ($\lambda = 365$ nm), producing •OH from the photoreduction of Fe(OH)²⁺, the photoactive species of aqueous Fe(III) ion, by reaction (5). Moreover, the incident photons can also photolyze oxidation products, like Fe(III)-carboxylate complexes by reaction (6) [38,39]. Note that UVA radiation does not photolyze H₂O₂ to •OH, a reaction that requires a more powerful radiation like UVC ($\lambda = 254$ nm).

87
$$\operatorname{Fe}^{2+} + \operatorname{H}_2\operatorname{O}_2 \to \operatorname{Fe}^{3+} + \operatorname{OH}^- + {}^{\bullet}\operatorname{OH}$$
 (4)

88
$$\operatorname{Fe}(\operatorname{OH})^{2+} + hv \to \operatorname{Fe}^{2+} + {}^{\bullet}\operatorname{OH}$$
 (5)

89
$$\operatorname{Fe}(\operatorname{OOCR})^{2+} + hv \rightarrow \operatorname{Fe}^{2+} + \operatorname{CO}_2 + \operatorname{R}^{\bullet}$$
 (6)

Apart from homogeneous [•]OH, other oxidizing agents can be generated in an undivided 90 cell, depending on the electrolyte and anode nature [30-32]. In non-chlorinated medium, the 91 heterogeneous M([•]OH) is formed as main species at the anode M from water discharge via 92 reaction (7). Boron-doped diamond (BDD) thin-films are the most convenient anodes for this, 93 since they produce great amounts of oxidant BDD([•]OH) [31,40]. In chloride medium, active 94 chlorine species (Cl₂/HClO/ClO⁻) are also formed, thus competing with M([•]OH) and [•]OH to 95 destroy the organics or microorganisms. Chloride is anodically oxidized to Cl₂ via reaction (8), 96 which is hydrolyzed to hypochlorous acid (HClO) via reaction (9) [8]. Cl₂ predominates at pH 97 < 3 and has lower oxidation power than HClO, the most abundant species from pH 3 to 8. At 98 higher pH, HClO is dissociated to ClO⁻. The oxidation of Cl⁻ is enhanced at dimensionally 99 stable anodes (DSA[®]) like RuO₂, but with low ability to produce adsorbed hydroxyl radicals 100 (RuO₂([•]OH)) [33,40]. 101

102
$$M + H_2O \rightarrow M(^{\bullet}OH) + H^+ + e^-$$
 (7)

$$103 \quad 2\mathrm{Cl}^{-} \to \mathrm{Cl}_{2} + 2\mathrm{e}^{-} \tag{8}$$

A limited number of papers has been devoted to explore the disinfection power of EF in 105 real wastewater matrices [42,43]. For example, Durán Moreno et al. [42] found that this process 106 allowed the overall inactivation of total coliforms, Escherichia coli, Shigella and Salmonella 107 sp. from municipal wastewater. In earlier work [24], we reported that a sequential EC/EF 108 treatment of primary and secondary WWTF effluents allowed the complete removal of all the 109 active microbiota, namely E. coli, enterococci, C. perfringens spores, somatic coliphages and 110 eukaryotes, with partial inactivation of the heterotrophic (HT) bacteria. Worth mentioning, the 111 PEF process has not been tested for disinfection. 112

113 This work aims to compare the ability of single EC with Fe|Fe cell with that of EF and 114 sequential EC/EF and EC/PEF processes to inactivate the microorganisms contained in a real 115 dairy wastewater sample. EF and PEF were comparatively performed with a BDD/air-diffusion 116 or RuO₂-based/air-diffusion cell to assess the role of generated oxidants. Considering the 117 microbiological complexity of this wastewater, HT and lactic acid (LA) bacteria, *E.coli* and 118 enterococci were selected as indicators to monitor the disinfection.

119 2. Materials and methods

120 *2.1. Chemicals*

121 Analytical grade heptahydrate Fe(II) sulfate was purchased from Sigma-Aldrich. The EF 122 and PEF assays after the EC-pre-treated wastewater were made after adjusting the pH at 3.0 123 with analytical grade H₂SO₄ or HClO₄ supplied by Merck. Analytical solutions were prepared 124 with ultrapure water (Millipore Milli-Q, resistivity >18.2 M Ω cm), whereas reagents and 125 organic solvents were of HPLC or analytical grade supplied by Merck, Panreac and Sigma-126 Aldrich.

127 2.2. Sample of dairy wastewater

Fresh dairy wastewater was treated in all the assays. The raw wastewater was obtained from a small dairy industry located in Lliçà d'Amunt (northeastern Spain). Samples were collected in polyethylene bottles and stored at 4 °C before usage in 24-48 h. The main average physicochemical characteristics were: pH 5.7±0.2, conductivity 2.95±0.12 mS cm⁻¹, 1416±24 mg C L⁻¹ of total organic carbon (TOC), 850±17 mg L⁻¹ of K⁺, 115±9 mg L⁻¹ of Na⁺, 1345±28 mg L⁻¹ of Cl⁻, 98±5 mg L⁻¹ of SO₄²⁻ and 0.045±0.002 mg L⁻¹ of Fe²⁺.

134 2.3. Microbial enumeration

LA and HT bacteria were quantified after 10-fold dilution with ¹/₄-strength Ringer's 135 solution and culture, respectively, by duplicate on Plate Count Agar (PCA) and Man, Rogosa 136 and Sharpe Agar (MRS), purchased from Scharlab. The incubation for HT was made at 30 °C 137 for 48 h and that of LA, at 30°C for 4 d, according to ISO 9308-2:2012. The theoretical detection 138 limit was 1 colony-forming units per mL (CFU mL⁻¹). E. coli and enterococci were quantified 139 by most probably number (MPN) using MUG/EC and MUD/SF Kit 96-well microplates 140 supplied by Bio-Rad Laboratories. Both bacteria were incubated at 42 °C for 48 h, following 141 ISO 9308-2:2012, with detection limit of 0.35-1.35 CFU mL⁻¹. 142

143 2.4. Electrolytic systems

All the electrolytic assays were performed with an open, undivided, jacketed, cylindrical cell. The temperature of the treated wastewater was kept at 25 °C by thermostated water and it was always vigorously stirred at 800 rpm with a magnetic PTFE bar. After each trial and before the next, the cell was cleaned with a H_2O_2/H_2SO_4 mixture for 10 min, rinsed with ultrapure water and dried in an oven at 80 °C.

In EC, 175 mL of raw dairy wastewater were electrolyzed with two 10-cm² Fe (mild carbon steel) plates as the anode and cathode, separated about 1 cm. A constant current was applied provided by an Amel 2053 potentiostat-galvanostat. Before each EC run, the surface of both Fe

electrodes was mechanically abraded with SiC paper, chemically cleaned with 0.1 M H₂SO₄
and ultrasonically cleaned in ultrapure water, followed by drying with an air stream.

The subsequent EF and PEF assays were carried out at constant current provided by the 154 above potentiostat-galvanostat with 120 mL of the supernatant liquid, which already contained 155 soluble iron ions formed in the EC treatment of the wastewater. In some cases, the pH was 156 adjusted to 3.0 with HClO₄ in order to maintain the same SO_4^{2-} and Cl⁻ ions content in the 157 sample. The EF runs of the raw dairy wastewater at natural pH were conducted with 150 mL of 158 sample after addition of 0.25 mM Fe^{2+} . The anode was either a BDD thin-film electrode over 159 160 Si substrate purchased from NeoCoat or a RuO₂-based plate supplied by NMT Electrodes. The cathode was a carbon-PTFE air-diffusion electrode purchased from Sainergy Fuel Cell. The 161 immersed area of all electrodes was 3 cm^2 and the interelectrode gap of about 1 cm. The cathode 162 produced H_2O_2 upon injecting compressed air at 1 L min⁻¹, as described elsewhere [39]. In the 163 PEF treatments, the wastewater was illuminated with UVA light (300-420 nm, λ_{max} = 360 nm) 164 165 emitted by a Philips TL/6W/08 fluorescent black light blue tube that was placed at 6 cm above the solution. The UVA irradiance of this tube was 5 W m⁻². Prior to the initial EF run, the 166 surface of the BDD and RuO₂-based anodes were cleaned in 0.050 M Na₂SO₄ at 300 mA for 167 168 180 min. Under these conditions, the air-diffusion cathode was activated as well. Before each further EF or PEF experiment, the BDD and RuO₂-based anodes were immersed in ultrapure 169 water at 100 °C for 10 min and dried under an air stream, whereas the air-diffusion cathode was 170 cleaned with a 1:3 (v/v) H₂O/HCl mixture and rinsed with ultrapure water, followed by air-171 drying. 172

173 2.5. Analytical methods

The pH was measured with a Crison GLP 22 pH-meter. The conductivity was determined on a Metrohm 644 conductometer. TOC analysis was carried out with a Shimadzu TOC-VCNS analyzer, with an accuracy of $\pm 1\%$ by injecting 50 µL aliquots previously filtered with 0.45 µm filters purchased from Whatman. The concentrations of cations and anions was determinedfollowing the procedures above reported [25].

The inactivation profiles for all the microorganisms were monitored from the decay of the logarithm of their concentration N (in CFU mL⁻¹). For each experimental condition, at least two independent tests were made, and the average log N value is given in the graphs along with the standard deviation (95% confidence interval).

183 **3. Results and discussion**

184 *3.1. Microbiological characterization of the dairy wastewater*

The samples of the dairy wastewater showed certain variability of pH with time and for 185 this reason, they were processed within 24 h and treated before 48 h as maximal. The 186 microscopic vision evidenced the presence of filamentous fungi, fat, yeasts and bacteria. 187 188 Protozoa were not observed, at least in detectable quantity. The initial microbiological analysis of the samples gave, in average, the following results: $(4.3\pm0.3)\times10^6$ CFU mL⁻¹ of HT, 189 $(3.4\pm0.1)\times10^5$ CFU mL⁻¹ of LA, $(2.6\pm0.2)\times10^5$ CFU mL⁻¹ of *E. coli*, $(1.2\pm0.1)\times10^6$ CFU mL⁻¹ 190 of total coliforms, $(2.5\pm0.1)\times10^2$ CFU mL⁻¹ of *Staphylococcus* and $(1.8\pm0.1)\times10^5$ CFU mL⁻¹ of 191 yeast and fungi. 192

193 *3.2. Electrocoagulation with Fe/Fe cell*

The EC of the dairy wastewater was performed with a Fe anode since its dissolution provided the amount of iron ions required for EF and PEF post-treatments [22,25]. First assays were made with 175 mL of the wastewater at natural pH 5.7 using a stirred Fe|Fe tank reactor and by applying 100 and 200 mA (current density of 10 and 20 mA cm⁻², respectively) for 60 min to assess the effect of increasing amounts of generated coagulants over disinfection. Under these conditions, a consumption of 1.93 electrons per Fe atom was determined from the anode weight loss [25], in good agreement with the expected two-electron Fe oxidation (reaction (1)).

Fig. 1 depicts the low drop of log N for HA and LA bacteria in the above trials. HA was 201 202 poorly inactivated at 100 mA, only in the order of 0.6 log units, whereas a slightly superior inactivation close to 1.0 log units was found at 200 mA. It is then apparent that the increase of 203 current yielded a quicker disappearance of both bacteria that remained entrapped in the major 204 amounts of Fe(OH)_n flocs and sludge formed. In the EC process, a gradual clarification of the 205 206 wastewater samples was observed, changing from initial white to final dark-green color. This 207 transition can be mainly related to the presence of iron ions and iron hydroxide flocs in suspension that give such dark-greenish coloration. The accumulation of released iron ions was 208 also confirmed from the increase of the conductivity from 2.95 to 4.4 mS cm⁻¹ at the end of the 209 210 run at 200 mA. It is noticeable that the wastewater was alkalinized during the EC treatment 211 because of the continuous uncompensated production of OH⁻ ion from reaction (3), since the Fe anode was dissolved according to reaction (1) without significant H^+ generation from H₂O 212 oxidation. This is in contrast to that occurring when using insoluble anodes like BDD and RuO₂ 213 214 [8,30-33]. For example, after 60 min at 200 mA, the pH rose from 5.7 to 7.8.

A poor loss of TOC of 185 and 255 mg C L⁻¹ (13% and 18% of initial value) after 60 min 215 of EC at 100 and 200 mA, respectively, was found as well. This reveals a low ability of the 216 217 $Fe(OH)_n$ flocs to coagulate the high amounts of pollutant molecules contained in the dairy wastewater, except whey proteins. Since the isoelectric point of these proteins is of 5.2 for β -218 lactoglobulin, 4.2-4.5 for α-lactalbumin, 5.5-6.8 for immunoglobulins and 4.7-4.9 for bovine 219 serum albumin, it is expected that they were rather removed by the flocs due to its low solubility 220 under our experimental conditions [44]. In contrast, it has been shown that soluble molecules 221 222 such as lactose, glucose and fatty acids cannot be removed by EC with Fe anode [20,21,27]. The large presence of the latter molecules in the organic load of dairy wastewater could explain 223 its very low TOC removal achieved by this treatment. Also worth highlighting, a low specific 224

energy consumption of 2.3 and 8.2 kWh m⁻³ was obtained for the EC treatment at 100 and 200
mA, respectively.

To corroborate that the microorganisms were retained on the dark-reddish sludge formed 227 by the Fe(OH)_n flocs, the remaining wastewater from a 200 mA trial was decanted to be 228 separated from the sludge and its flocs were subsequently collected by filtration. Analysis of 229 these wastes showed the existence of a higher content of heterotrophs still actives in the flocs 230 $(3.2 \times 10^5 \text{ CFU mL}^{-1})$ than in the sediment $(8.3 \times 10^2 \text{ CFU mL}^{-1})$. For a whey wastewater, Un and 231 Kandemir [29] reported the presence of hematite (Fe_2O_3) and magnetite (Fe_3O_4) phases in the 232 233 dried sludge obtained through EC with Fe anode. They proposed that part of this sludge could be used as an iron source in other applications and its excess could be used as a fertilizer or 234 incinerated if it is very toxic. Our results for the sludge produced from dairy wastewater reveal 235 the retention of an important content of active bacteria, meaning that it should be incinerated to 236 avoid their infection in living beings. 237

238 3.3. Sequential EC/EF with BDD at pH 3.0 and circumneutral pH

Next, the sequential assays were carried out for 60 min in EC and 120 min in EF. The EC 239 step was firstly performed as explained in section 3.2, i.e., 175 mL of sample at natural pH with 240 Fe|Fe cell at 200 mA. Once ended, the wastewater was filtered and 120 mL of the transparent 241 242 and greenish supernatant liquid were introduced in a rinsed and cleaned cell to be post-treated by EF. The pH of this liquid was adjusted to pH 3.0 with H₂SO₄ (optimum acidity for EF) and 243 it already contained enough soluble iron ions from the previous EC process (about 3 mg L⁻¹ 244 [22]), to generate homogeneous [•]OH upon optimum conditions of Fenton's reaction (4). The 245 EF process was then run after introducing a BDD anode and an air-diffusion cathode in the 246 stirred cell and by applying a current of 100 mA (current density of 33.3 mA cm⁻²) for 120 min. 247 No significant change in pH was found during this post-treatment. 248

Fig. 2 shows the evolution of log N for HT and LA bacteria in the above sequential EC/EF 249 250 treatment. Worth mentioning, after filtration of the resulting wastewater from EC and adjustment to pH 3.0 before EF, the initial concentration of both microorganism was reduced 251 by about 2 log units, resulting average values of 8.75×10² CFU mL⁻¹ for HT bacteria and 252 4.76×10^3 CFU mL⁻¹ for LA bacteria. The decay of the former bacteria could be related to two 253 effects: (i) the retention of the microorganisms onto the flocs that remain in the filter and (ii) 254 their larger inactivation at the acidic pH of the wastewater. However, the latter explanation 255 256 seems not valid for the LA bacteria, which are acid tolerant and can survive between pH 3.2 to 9.6, with optimum growth in the pH range 4.0-4.5 [45]. This bacterial group is composed of a 257 258 large variety of microorganisms, cocci or rods, with common Gram-positive, anaerobic, microaerophilic or aerotolerant, non-espore-forming, non-pathogens, non-toxigenic, and 259 260 negative oxidase, catalase and benzidine characteristics, and lactic acid production as the major 261 end by-product of the fermentation of carbohydrates [46,47].

Fig. 2 shows that in the EF step, the HT bacteria underwent a loss of 2.3 log units, which 262 remained invariable between 60 and 120 min of electrolysis, whereas the LA bacteria were 263 inactivated gradually to larger extent up to 3.3 log units. The greater LA reduction would be 264 related to its higher initial concentration in the wastewater. It seems unreasonable to explain the 265 266 decay on the basis of the toxicity produced by the electrogenerated H₂O₂, because this bacteria group, especially the rod-shaped lactobacilli, in presence of O₂ already produces certain amount 267 268 of H₂O₂ that is chemically and enzymatically transformed into oxygen radicals with more potent 269 antimicrobial activity than H₂O₂ itself [48,49]. The inactivation of HT and LA bacteria in EF 270 can then be associated to the action of strong oxidizing agents generated, including •OH from Fenton's reaction (4), BDD(•OH) from reaction (7) and active chlorine (Cl₂/HClO) from 271 272 reactions (8) and (9), as established elsewhere [50,51]. These strong oxidants are expected to attack the molecules of the cell walls causing the lysis and death of bacteria [24,52]. In contrast, 273

the weaker oxidant H_2O_2 is expected to contribute to the disinfection to a much smaller extent [48,49], being rather inactive for LA bacteria, as stated above.

Unlike the EC step where the pH and conductivity of the treated dairy wastewater 276 underwent large variations, the subsequent EF process at pH 3.0 showed a good stability of 277 both parameters. After 120 min of EF, the pH decayed slightly to 2.6, suggesting the formation 278 of acidic by-products, and the initial conductivity of 6.4 mS cm⁻¹ (due to H₂SO₄ addition for 279 pH adjustment) rose up to 7.0 mS cm⁻¹. Moreover, the sequential EC/EF treatment only yielded 280 a small TOC reduction of 385 mg C L⁻¹ (27% of the initial 1416 mg C L⁻¹), indicating not only 281 the low ability of the Fe(OH)n flocs for organic coagulation in EC, as stated above, but also the 282 283 low oxidizing power of [•]OH, BDD([•]OH) and active chlorine to mineralize them in EF. It is also noticeable that the dark-green wastewater obtained after EC was clarified upon acid 284 addition before EF and at the end of this treatment, it reached a clear vellow-brown color due 285 286 to the removal of suspended solids and the presence of iron ions.

To assess the disinfection power of the generated oxidizing agents under non-optimum 287 conditions of Fenton's reaction (4), another sequential EC/EF treatment of the raw dairy 288 wastewater was made, but without varying the pH of the filtered supernatant liquid obtained by 289 EC to be treated by EF. Thus, the EC step with Fe|Fe cell was carried out by applying 200 mA 290 for 30 min, where the pH increased from 5.7 to 7.5. The subsequent EF with BDD at 100 mA 291 was carried out for 60 min, showing a pH decay from 7.5 to 6.8. The conductivity also rose up 292 to 4 mS cm⁻¹ in the former case, remaining practically unchanged in the second one. Moreover, 293 about 20% of the initial TOC was removed in this sequential EC/EF process, corroborating 294 again the low ability of the species formed in each step to coagulate/mineralize the organic 295 matter of the wastewater. 296

For the aforementioned experiment, Fig. 3 reveals a little drop of 0.8 log units in the concentration of both HT and LA bacteria after 30 min of EC. After filtration of the liquid

supernatant, the content of these groups of bacteria were reduced by 2.3 log and 2.8 log units, 299 respectively. It should be noteworthy the large inactivation achieved after 60 min of EF, where 300 15 CFU mL⁻¹ were only detected for HT, whereas the LA bacteria disappeared completely. 301 Compared with the results of Fig. 2, one can infer that the oxidizing agents formed at 302 circumneutral pH were more effective to disinfect the wastewater than those produced at pH 303 304 3.0, although with a slightly lower inactivation power over the HT bacteria. This indicates that the disinfection of the sequential EC/EF process over dairy wastewater is so good operating at 305 306 circumneutral pH that it is not necessary to regulate the optimum pH 3.0 for the EF posttreatment. At circumneutral pH, active chlorine is mainly in the form of HClO, which is more 307 308 powerful than Cl₂ that is also present at pH 3.0 [31-33]. The specific energy consumption for this assay was 19.5 kWh m⁻³, arising from 4.1 kWh m⁻³ (21%) of EC plus 15.4 kWh m⁻³ (79%) 309 of EF. Although the EF post-treatment was much more efficient for disinfection, it demanded 310 311 greater energy consumption than the EC step.

312 *3.4. Comparative sequential EC/EF and EC/PEF with BDD and RuO*₂*-based at pH 3.0*

A series of comparative trials was made to check the influence of the anode, BDD or RuO₂based, over the disinfection power of the EF post-treatment, as well as considering that of the incident UVA light using the PEF one. The EC step was performed again with 175 mL of a sample of dairy wastewater in a stirred Fe|Fe cell at 200 mA for 45 min. The EF or PEF steps were carried out with 120 mL of the filtered supernatant liquid once adjusted at pH 3.0 with HClO₄ (to no alter the Cl⁻ and SO₄²⁻ content of the samples) and by applying 100 mA, for 120 min as maximal.

As expected, the initial pH of 5.7 and conductivity of 2.9 mS cm⁻¹ of the raw wastewater rose up to 7.8 and 4.4 mS cm⁻¹, respectively, after the EC pretreatment. In contrast, no significant change of pH close to 3 and conductivity of about 6.4 mS cm⁻¹ was observed after the EF and PEF post-treatments. For the latter steps, the use of a BDD anode always caused a

higher TOC abatement than that of RuO₂-based. The initial TOC was reduced by 25% and 28% 324 325 for EC/EF and EC/PEF with BDD, respectively, and to lesser extent of 21% and 24% for the analogous runs with RuO₂-based. In all cases, the EC step yielded the higher TOC removal of 326 327 about 17%-18%. These findings agree with the superior ability of BDD([•]OH) compared to RuO₂([•]OH) to destroy the organic matter [31-33], thereby confirming the important oxidative 328 role of the former radical. The enhancement of TOC removal by PEF can be accounted for by 329 330 the oxidation action of UVA light that can photolyze photoactive intermediates, e.g. from reaction (6), and originate more amounts of •OH from reaction (5) and photo-excitation of 331 active chlorine [53]. 332

333 A different trend can be observed in Fig. 4a and b for the inactivation of HT and LA bacteria by the above trials. An important and similar loss of bacterial concentration of 3-4 log units 334 always occurred after conditioning the supernatant liquid of EC at pH 3.0 with HClO₄ (probably 335 336 more toxic than H₂SO₄), whereas both groups of bacteria disappeared rapidly after 60 min of EF and 30 min of PEF, regardless the anode used. This means that the disinfection process in 337 EF takes place thanks to [•]OH and active chlorine as the most efficient oxidants for lysing the 338 cells. The quicker inactivation attained by PEF is due to the additional excess of •OH produced 339 340 under the 6 W UVA radiation that facilitates their lysing, along with its photolytic action over 341 the nucleic acids (DNA and RNA) of the cells [54]. Despite the PEF post-treatment produces faster disinfection and larger TOC abatement of the dairy wastewaters, the high energy spent 342 by the UVA lamp prevents their use in practice and the alternative EF step seems more useful 343 344 for such purposes.

345 *3.5. EF treatment at natural pH*

Last experiments were made to assess the disinfection performance of EF over the dairy wastewater. To do this, 0.25 mM Fe^{2+} were added to 150 mL of sample at natural pH for further electrolysis in stirred BDD/air-diffusion and RuO₂-based/air-diffusion cells at 100 mA for 120 min. No substantial change of the initial conductivity of 2.8 mS cm⁻¹ was found for these trials, whereas the initial pH of 5.8 rose slightly up to 6.6 at the end of electrolysis, regardless the anode used. A slight decay of the initial TOC of 10% for BDD and 13% for RuO₂-based was determined as well, corroborating the very low ability of the oxidizing agents generated to mineralize the complex organic molecules of the dairy wastewater.

Fig. 5a and b depict the change of log N of HT and LA bacteria, *E.coli* and enterococci 354 355 with time for EF with BDD and RuO₂-based anodes, respectively. As can be seen, the complex group of heterotrophs were the most resistant at inactivation. Its concentration profile showed 356 a quicker removal within the first 30 min of electrolysis, with reductions of 2.7 log units for 357 358 BDD and greater of 5.7 log units for RuO₂-based. The loss of efficiency at longer time was due to the lower bacterial concentration. After 120 min of EF treatment, 131 and 9.5 CFU mL⁻¹ of 359 these bacteria using BDD and RuO₂-based still survived. The faster inactivation achieved by 360 361 RuO₂-based suggests that active chlorine, formed to greater extent from this anode than from BDD, plays a more relevant role to remove the bacteria than hydroxyl radicals. However, the 362 contribution of [•]OH formed from Fenton's reaction (4) was confirmed by performing electro-363 oxidation trials where the air-diffusion cathode was replaced by a stainless steel plate, leading 364 365 to a slower removal by 1 log unit.

A similar disinfection trend for both anodes can be observed in Fig. 5a and b for the other bacteria, which were more quickly inactivated. In the case of LA bacteria, the concentration diminished 2.14 log units for BDD and 5.5 log units for RuO₂-based at 30 min, disappearing after 120 and 60 min of electrolysis, respectively. The inactivation of *E. coli* and enterococci was even much faster, since they were completely removed at 60 and 30 min using BDD and RuO₂-based, respectively.

The above results are similar to the large disinfection reported in earlier work for the EF treatment with BDD anode of primary and secondary effluents at neutral pH [24]. They are also

consistent with the removal of 99.95% coliform bacteria from landfill leachate achieved using 374 this technology [43]. Although EF is optimal at pH near 3 where more [•]OH is generated from 375 Fenton's reaction (4), the combined oxidation ability of this radical and active chlorine to 376 inactivate the microorganisms not only makes feasible its application at natural pH, but also 377 favors the use of a RuO₂-based anode, much cheaper than the BDD. The EF with RuO₂-based 378 can then be envisaged as more useful in practice than any sequential EC/EF process to largely 379 380 disinfect dairy wastewater since it avoids the sludge produced in the EC step, which needs further treatment to prevent infections from the active bacteria retained in it. 381

382 **4.** Conclusions

383 The iron hydroxide flocs formed during EC with an Fe|Fe cell were able to remove only small TOC contents (up to 18%) and HT and LA bacteria concentrations (< 1.0 log units) from 384 raw dairy wastewater. Furthermore, it was shown that the sludge retained active bacteria. A 385 poor abatement of the organic matter was also found in single EF and PEF with BDD or RuO₂-386 based anodes, as well as in sequential treatments, indicating the low oxidation ability of 387 hydroxyl radicals and active chlorine to attack the complex molecules of such wastewater. In 388 contrast, the application of these EAOPs yielded a large inactivation of all bacteria. 389 Heterotrophs were the most hardly inactivated microorganisms, whereas LA bacteria, E.coli 390 391 and enterococci were more rapidly removed and even completely inactivated. In the sequential process involving the EF step with BDD, a quick inactivation of LA bacteria was found at 392 circumneutral pH, revealing the pre-eminent oxidation role of active chlorine over the 393 394 molecules of the cell walls. This was corroborated by the quick inactivation of both bacteria using a RuO₂-based anode at pH 3.0, since this material promoted the active chlorine 395 production. With PEF as post-treatment, total disinfection was rapidly achieved due to the 396 additional bacterial inactivation induced by UVA light. Direct EF treatment of dairy wastewater 397

at natural pH also led to faster inactivation of all bacteria using the RuO₂-anode, which was
complete for LA bacteria, *E. coli* and enterococci. This method is thus preferred for dairy
wastewater disinfection because it avoids the need of sludge management from EC, although it
is more energy-intensive than EC.

402 Acknowledgements

The authors are grateful for financial support under projects CTQ2013-48897-C2-1-R and
CTQ2016-78616-R (AEI/FEDER, EU) and from the "Grups de recerca reconeguts"
2014SGR83 and 2014SGR914 (Generalitat de Catalunya). The microscopic analysis of samples
by Prof. Humbert Salvadó is also acknowledged.

407 **References**

- 408 [1] B. Balannec, M. Vourch, M. Rabiller-Baudry, B. Chaufer, Comparative study of different
 409 nanofiltration and reverse osmosis membranes for dairy effluent treatment by dead-end
 410 filtration, Sep. Purif. Technol. 42 (2005) 195-200.
- 411 [2] A. García-García, V. Martínez-Miranda, I.G. Martínez-Cienfuegos, P.T. Almazán412 Sánchez, M. Castañeda-Juárez, I. Linares-Hernández, Industrial wastewater treatment by
 413 electrocoagulation-electrooxidation processes powered by solar cells, Fuel 149 (2015)
 414 46-54.
- U.T. Un, A. Kandemir, N. Erginel, S.E. Ocal, Continuous electrocoagulation of cheese
 whey wastewater: An application of response surface methodology, J. Environ. Manage.
 146 (2014) 245-250.
- 418 [4] F. Carvalho, A.R. Prazeres, J. Rivas, Cheese whey wastewater: characterization and
 419 treatment, Sci. Total Environ. 445-446 (2013) 385-396.

- 420 [5] A.R. Prazeres, F. Carvalho, J. Rivas, Fenton-like application to pretreated cheese whey
 421 wastewater, J. Environ. Manage. 129 (2013) 199-205.
- 422 [6] D. Ghernaout, B. Ghernaout, From chemical disinfection to electrodisinfection: the
 423 obligatory itinerary?, Desalin. Water Treat. 16 (2010) 156-175.
- 424 [7] C.E. Barrera-Díaz, G. Roa-Morales, P. Balderas-Hernández, P.M. Fernandez-Marchante,
- M.A. Rodrigo, Enhanced electrocoagulation: new approaches to improve the
 electrochemical process, J. Electrochem. Sci. Eng. 4 (2014) 285-296.
- 427 [8] E. Brillas, C.A. Martínez-Huitle, Decontamination of wastewater containing synthetic
 428 organic dyes by electrochemical methods. An updated review, Appl. Catal. B: Environ.
- 429 166-167 (2015) 603-643.
- 430 [9] A. Pirkarami, M.E. Olya, S. Tabibian, Treatment of colored and real industrial effluents
 431 through electrocoagulation using solar energy, J. Environ. Sci. Health A: Toxicol.
 432 Hazard. Subst. Environ. Eng. 48 (2013) 1243-1252.
- [10] A. Pirkarami, M.E. Olya, Removal of dye from industrial wastewater with an emphasis
 on improving economic efficiency and degradation mechanism, J. Saudi Chem. Soc. 21
 (2017) \$179-\$186.
- [11] J.N. Hakizimana, B. Gourich, M. Chafi, Y. Stiriba, C. Vial, P. Drogui, J. Naja,
 Electrocoagulation process in water treatment: a review of electrocoagulation modeling
 approaches, Desalination 404 (2017) 1-21.
- 439 [12] D. Ghernaout, B. Ghernaout, Sweep flocculation as a second form of change
 440 neutralization a review, Desalin. Water Treat. 44 (2012) 15-28.
- [13] M. Kobya, O.T. Can, M. Bayramoglu, Treatment of textile wastewaters by
 electrocoagulation using iron and aluminum electrodes, J. Hazard. Mater. 100 (2003)
 163-178.

- 444 [14] S. Cotillas, J. Llanos, P. Cañizares, S. Mateo, M.A. Rodrigo, Optimization of an
 445 integrated electrodisinfection/electrocoagulation process with Al bipolar electrodes for
 446 urban wastewater reclamation, Water Res. 47 (2013) 1741-1750.
- [15] C. Delaire, C.M. van Genuchten, S.E. Amrose, A.J. Gadgil AJ, Bacteria attenuation by
 iron electrocoagulation governed by interactions between bacterial phosphate groups and
 Fe(III) precipitates, Water Res. 103 (2016) 74-82.
- [16] J. Llanos, S. Cotillas, P. Cañizares, M.A. Rodrigo, Electrocoagulation as a key technique
 in the integrated urban water cycle- a case study in the centre of Spain, Urban Water J.
 14 (2017) 650-654.
- [17] M. Elazzouri, Kh. Haboubi, M.S. Elyoubi, Electrocoagulation-flocculation as a low-cost
 process for pollutants removal from urban wastewater, Chem. Eng. Res. Des. 117 (2017)
 614-626.
- [18] A.R. Makwana, M.M. Ahammed, Electrocoagulation process for the post-treatment of
 anaerobically treated urban wastewater, Sep. Purif. Technol. 52 (2017) 1412-1422.
- [19] P. Valero, M. Verbel, J. Silva-Agredo, R. Mosteo, M.P. Ormad, R.A. Torres-Palma,
 Electrochemical advanced oxidation processes for *Staphylococcus aureus* disinfection in
 municipal WWTP effluents, J. Environ. Manage. 198 (2017) 256-265.
- 461 [20] A. Dalvand, M. Gholami, A. Joneidi, N.M. Mahmoodi, Dye removal, energy
 462 consumption and operating cost of electrocoagulation of textile wastewater as a clean
 463 process. Clean-Soil, Air, Water 39 (2011) 665-672.
- 464 [21] V. Khandegar, A.K. Saroha, Electrocoagulation for the treatment of textile industry
 465 effluent: a review, J. Environ. Manage. 128 (2013) 949-963.
- 466 [22] A. Thiam, M. Zhou. E. Brillas, I. Sirés, Two-step mineralization of Tartrazine solutions:
 467 study of parameters and by-products during the coupling of electrocoagulation with

468 electrochemical advanced oxidation processes, Appl. Catal. B: Environ. 150-151 (2014)
469 116-125.

- [23] N.M.A. Ghalwa, A.M. Saqer, N.B. Farhat, Removal of reactive red 24 dye by clean
 electrocoagulation process using iron and aluminum electrodes, J. Appl. Chem. Res. 10
 (2016) 117-132.
- E. Anfruns-Estrada, C. Bruguera-Casamada, H. Salvadó, E. Brillas, I. Sirés, R.M. Araujo,
 Inactivation of microbiota from urban wastewater by single and sequential
 electrocoagulation and electro-Fenton treatments, Water Res. 126 (2017) 450-459.
- 476 [25] N. Flores, E. Brillas, F. Centellas, R.M. Rodríguez, P.L. Cabot, J.A. Garrido, I. Sirés,
- Treatment of olive oil mill wastewater by single electrocoagulation with different
 electrodes and sequential electrocoagulation/electrochemical Fenton-based processes, J.
 Hazard. Mater. 347 (2018) 58-66.
- 480 [26] G. Guven, A. Perendeci, A. Tanylac, Electrochemical treatment of deproteinated whey
 481 wastewater and optimization of treatment conditions with response surface methodology,
 482 J. Hazard. Mater. 15 (2008) 69-78.
- [27] S. Tchamango, C.P. Nanseu-Njiki, E. Ngameni, D. Hadjiev, A. Darchen, Treatment of
 dairy effluents by electrocoagulation using aluminum electrodes, Sci. Total Environ. 408
 (2010) 947-952.
- [28] N.A. Fayad, T. Yehyta, F. Audonnet, Ch. Vial, Elimination of whey proteins by electrocoagulation: Investigation of some key operational parameters and modeling. Desalin.
 Water Treat. 68 (2017) 143-152.
- [29] U.T. Un, A. Kandemir, Treatment of whey wastewater by electrocoagulation and electroFenton methods in batch mode, Desalin. Water Treat. 95 (2017) 88-95.
- 491 [30] E. Brillas, I. Sirés I, M.A. Oturan, Electro-Fenton process and related electrochemical
 492 technologies based on Fenton's reaction chemistry, Chem. Rev. 109 (2009) 6570-6631.

21

- 493 [31] I. Sirés, E. Brillas, Remediation of water pollution caused by pharmaceutical residues
 494 based on electrochemical separation and degradation technologies: a review, Environ. Int.
 495 40 (2012) 212-229.
- I. Sirés, E. Brillas, M.A. Oturan, M.A. Rodrigo, M. Panizza, Electrochemical advanced
 oxidation processes: today and tomorrow. A review, Environ. Sci. Pollut. Res. 21 (2014)
 8336-8367.
- [33] C.A. Martínez-Huitle, M.A. Rodrigo, I. Sirés, O. Scialdone, Single and coupled
 electrochemical processes and reactors for the abatement of organic water pollutants: a
 critical review, Chem. Rev. 115 (2015) 13362-13407.
- 502 [34] A. Dirany, I. Sirés, N. Oturan, A. Özcan, M.A. Oturan, Electrochemical treatment of the
 503 antibiotic sulfachloropyridazine: Kinetics, reaction pathways, and toxicity evolution,
 504 Environ. Sci. Technol. 46 (2012) 4074-4082.
- [35] A. El-Ghenymy, R.M. Rodríguez, E. Brillas, N. Oturan, M.A. Oturan, Electro-Fenton
 degradation of the antibiotic sulfanilamide with Pt/carbon-felt and BDD/carbon-felt cells.
 Kinetics, reaction intermediates, and toxicity assessment, Environ. Sci. Pollut. Res. 21
 (2014) 8368-8378.
- [36] A. Abdessalem, N. Oturan, N. Bellakhal, M.A. Oturan, M. Dachraoui, M. Remediation
 of water contaminated with pesticides by indirect electrochemical oxidation process
 electro-Fenton, J. Adv. Oxid. Technol. 11 (2016) 276-282.
- 512 [37] O. Ganzenko, N. Oturan, I. Sirés, D. Huguenot, E.D. van Hullebusch, G. Esposito, M.A.
 513 Oturan, Fast and complete removal of the 5-fluorouracil drug from water by electro514 Fenton oxidation, Environ. Chem. Lett. 16 (2018) 281-286.
- 515 [38] A. El-Ghenymy, N. Oturan, M.A. Oturan, J.A. Garrido, P.L. Cabot, F. Centellas, R.M.
- 516 Rodríguez, E. Brillas, Comparative electro-Fenton and UVA photoelectro-Fenton

517 degradation of the antibiotic sulfanilamide using a stirred BDD/air-diffusion tank reactor,

518 Chem. Eng. J. 234 (2013) 115-123.

- [39] A. El-Ghenymy, F. Centellas, R.M. Rodríguez, P.L. Cabot, J.A. Garrido, I. Sirés, E.
 Brillas, Comparative use of anodic oxidation, electro-Fenton and photoelectro-Fenton
 with Pt or boron-doped diamond anode to decolorize and mineralize Malachite Green
 oxalate dye, Electrochim. Acta 182 (2015) 247-256.
- [40] A. Thiam, E. Brillas, F. Centellas, P.L. Cabot, I. Sirés, Electrochemical reactivity of
 Ponceau 4R (food additive E124) in different electrolytes and batch cells, Electrochim.
 Acta 173 (2015) 523-533.
- [41] S. Lanzalaco, I. Sirés, M.A. Sabatino, C. Dispenza, O. Scialdone, A. Galia, Synthesis of
 polymer nanogels by electro-Fenton process: investigation of the effect of main operation
 parameters, Electrochim. Acta 246 (2017) 812-822.
- [42] A. Duran Moreno, B.A. Frontana-Uribe, R.M. Ramírez Zamora, Electro-Fenton as a
 feasible advanced treatment process to produce reclaimed water, Water Sci. Technol. 50
 (2004) 83-90.
- [43] H.A. Aziz, O.M. Othman, S.S.A. Amr, The performance of Electro-Fenton oxidation in
 the removal of coliform bacteria from landfill leachate, Waste Manage. 33 (2013) 396400.
- 535 [44] A.L.F. Cavallieri, A.P. Costa-Netto, M. Menossi, R.L. Da Cunha, Whey protein
 536 interactions in acidic cold-set gels at different pH values, Lait 87 (2007) 535-554.
- 537 [45] F.J. Carr, D. Chill, N. Maida, The lactic acid bacteria: a literature survey, Crit. Rev.
 538 Microbiol. 28 (2002) 281-370.
- [46] R. Crittender, Incorporating probiotics into foods, in: Y.K. Lee, S. Salminen (eds),
 Handbook of probiotics and prebiotics, 2nd ed. 2009, NJ, USA, pp. 58-75.

- 541 [47] A. Vásquez, T.C. Olofsson, The lactic acid bacteria involved in the production of bee
 542 pollen and bee bread, J. Apic. Res. 48 (2009) 189-195.
- 543 [48] A. Berstad, J. Raa, T. Midtvedt, J. Valeur, Probiotic lactic acid bacteria- the fledgling
 544 cuckoos of the gut?, Microb. Ecol. Health Dis. 27 (2016) 10.3402/mehd.v27.31557.
- [49] A. Di Cerbo, B. Palmieri, M. Aponte, J.C. Morales-Medina, T. Iannitti, Mechanisms and
 therapeutic effectiveness of lactobacilli, J. Clin. Pathol. Mar. 69 (2016) 187-203.
- 547 [50] J.R. Steter, E. Brillas, I. Sirés, On the selection of the anode material for the
 548 electrochemical removal of methylparaben from different aqueous media, Electrochim.
 549 Acta 222 (2016) 1464-1474.
- [51] Z.G. Aguilar, E. Brillas, M. Salazar, J.L. Nava, I. Sirés, Evidence of Fenton-like reaction
 with active chlorine during the electrocatalytic oxidation of Acid Yellow 36 azo dye with
 Ir-Sn-Sb oxide anode in the presence of iron ion, Appl. Catal. B: Environ. 206 (2017) 44-
- 553 52.
- 554 [52] D. Aguayo, N. Pacheco, E.H. Morales, B. Collao, R. Luraschi, C. Cabezas, P. Calderon,
- F. González-Nilo, F. Gil, I.L. Calderón, Hydrogen peroxide and hypochlorous acid influx
 through the major S. typhimurium porin OmpD is affected by substitution of key residues
 of the channel, Arch. Biochem. Biophys. 568 (2015) 38-45.
- [53] M.J. Watts, K.G. Linden, Chlorine photolysis and subsequent OH radical production
 during UV treatment of chlorinated water, Water Res. 41 (2007) 2871-2878.
- [54] A.M. Zyara, E. Torvinen, A.M. Veijalainen, H. Heinonen-Tanski, The effect of UV and
 combined chlorine/UV treatment on coliphages in drinking water disinfection, Water 130
 (2016), doi:10.3390/w8040130.

563

564 **Figure captions**

Fig. 1. Variation of logarithm of the concentration of heterotrophic (HT) and lactic acid (LA)
bacteria with electrolysis time upon electrocoagulation (EC) of 175 mL of dairy wastewater at
natural pH using an undivided Fe|Fe cell (10 cm² electrode area) at a current of 100 or 200 mA
and 25 °C.

Fig. 2. Change of the logarithm of the concentration of heterotrophic and lactic acid bacteria with time for a sequential EC/EF treatment performed for 60 and 120 min, respectively. In the EC step, 175 mL of dairy wastewater at natural pH were treated in an undivided Fe|Fe cell at 200 mA. The following EF step was carried out with 120 mL of the supernatant solution adjusted to pH 3.0 using a BDD/air-diffusion cell (3 cm² electrode area) at 100 mA. Temperature: 25 °C.

Fig. 3. Variation of the logarithm of the concentration of heterotrophic and lactic acid bacteria
in a sequential EC/EF treatment performed for 30 and 60 min, respectively. The EC and EF
steps were made under the same conditions as in Fig. 2, but the initial pH of the supernatant
liquid in EF was ca. 7.5, the value obtained at the end of EC.

Fig. 4. Change of the logarithm of the concentration of heterotrophic and lactic acid bacteria with time in sequential (a) EC/EF and (b) EC/PEF treatments. In both cases, the first process (EC) was performed with 175 mL of dairy wastewater at natural pH in an undivided Fe|Fe cell at 200 mA for 45 min. The subsequent EF or PEF treatment was made with 120 mL of the supernatant solution at pH 3.0 using a BDD/air-diffusion or RuO₂-based/air diffusion cell at 100 mA for 120 min. In PEF, the solution was irradiated with a 6 W UVA lamp. Temperature: 25 °C.

Fig. 5. Variation of logarithm of the concentration of heterotrophic and lactic acid bacteria, *E. coli* and enterococci along 120 min of EF treatment of 150 mL of dairy wastewater at natural
pH with 0.25 mM Fe²⁺ using (a) BDD/air-diffusion and (b) RuO₂-based/air-diffusion cells at
100 mA and 25 °C.



Fig. 1



Fig. 2



Fig. 3



Fig. 4



0

HT

■ 0 min EF

LA

30 min EF

E. coli

60 min EF **9**0 min EF

Enterococci

□ 120 min EF