

Ti|Ir–Sn–Sb oxide anode: Service life and role of the acid sites content during water oxidation to hydroxyl radicals

Zaira G. Aguilar ^a, Oscar Coreño ^b, Mercedes Salazar ^c, Ignasi Sirés ^d, Enric Brillas ^d, José L. Nava ^{a,*}

^a *Departamento de Ingeniería Geomática e Hidráulica, Universidad de Guanajuato, Av. Juárez 77, Zona Centro, C.P 36000 Guanajuato, Guanajuato, Mexico*

^b *Departamento de Ingeniería Civil, Universidad de Guanajuato, Av. Juárez 77, Zona Centro, C.P 36000 Guanajuato, Guanajuato, Mexico*

^c *Departamento de Ingeniería en Minas, Metalurgia y Geología, Universidad de Guanajuato, ExHacienda San Matías S/N, C.P. 36020, Guanajuato, Guanajuato, Mexico*

^d *Laboratori d'Electroquímica dels Materials i del Medi Ambient, Departament de Química Física, Facultat de Química, Universitat de Barcelona, Martí i Franquès 1-11, 08028 Barcelona, Spain*

* Corresponding author: E-mail address: jlnm@ugto.mx (J.L. Nava)

Abstract

This work describes the preparation of four Ti|Ir–Sn–Sb oxide anodes by the Pechini method under different conditions and the evaluation of their service life, envisaging a future application in electrochemical advanced oxidation processes for water treatment. This was estimated by means of accelerated life tests (1 A cm^{-2} , 1 M HClO_4), which highlighted the dependence of durability on the Ir and Sn content in the mixed metal oxide (MMO) as well as on the required heat treatment time for its preparation. The best MMO anode reached up to 351 h of service life under such extreme conditions. SEM-EDS and XRD analyses were performed before and after the accelerated life tests, evidencing that the failure of the MMO coatings occurred by detachment from the titanium substrate, thus losing the anode electroactivity. Great amounts of acid sites in the range $0.21\text{--}0.26 \text{ meq g}^{-1}$ were determined on the MMO surfaces by Boehm titrations. From the apparent rate constants determined for the decay of *N,N*-dimethyl-4-nitrosoaniline used as spin trap, before and after acid sites neutralization, a higher activity of adsorbed hydroxyl radicals at the MMO surface cannot be correlated with a greater amount of acid sites. The results obtained suggest that other active sites affect the formation of such radicals from water discharge.

Keywords: Accelerated life tests; Mixed metal oxide anode; Acid site; Hydroxyl radical; Anodic oxidation.

1. Introduction

Dimensionally stable anodes (DSA[®]) were developed by Beer in the late 1960s. Although their primary application has been recognized in the chlor-alkali industry [1], they are widely used for the degradation of persistent organic pollutants (POPs) in water [2-15]. These works highlighted that mixed metal oxides (MMO) supported on either titanium or niobium substrates represent one of the most important categories of electrocatalysts [4-11,13-15]. In recent years, electrochemical advanced oxidation processes (EAOPs) using pure metal anodes like Pt, metal oxides (MO) such as PtO, IrO₂, RuO₂, SnO₂ and PbO₂, and MMO like SnO₂-Sb₂O₅, TiO₂-SnO₂ and IrO₂-SnO₂-Sb₂O₅, among others, have been investigated in detail for environmental preservation [13,16]. The high oxidation power of these anodes has been confirmed upon degradation of all kinds of POPs in synthetic and real water effluents.

The anode material plays a fundamental role for the development of effective electro-oxidation (EO) methods, being necessary to prevent typical surface failure and fouling that cause the anode deactivation [17,18]. At present, boron-doped diamond (BDD) anode is considered the best electrode for the EO of POPs [13,16]. Its success is attributed to the large production of physisorbed hydroxyl radicals (BDD(•OH)) via water oxidation, leading to the complete mineralization of the organic matter in most cases. However, the high cost of BDD anodes has limited its use to small devices. Hence, the design and synthesis of much less expensive MMO anodes is now attracting a lot of attention [4,6-10,14,15]. The preparation of an ideal MMO electrode must guarantee its high oxidation ability, chemical and mechanical stability based on an adequate service life, and low cost. Worth mentioning, the use of MMO for POPs degradation has only been performed at small scale due to limitations from short service life and passivation, which has impeded its industrial application so far [3,12,19].

The MMO anodes are composed of a metal substrate coated with an electrocatalytic layer. Ti, Ta, Zr, W, Nb and Bi are typical substrates, being Ti the most common, whereas Pt, Ir, Ru, Sn, Ir and Ru are used as electrocatalysts, either pure or as metal oxides. Other metal oxides such as TiO_2 , Ta_2O_5 , ZrO_2 , Nb_2O_5 and SnO_2 are used as dispersing or stabilizing agents, and Sb is often added as a doping mediator [20]. RuO_2 -based MO anodes are suitable to evolve Cl_2 , but they are stable only at alkaline conditions [20], with modest service life under acidic conditions even when a stabilizer is used [21]. In contrast, IrO_2 -based anodes are typically chosen as optimum electrocatalysts to promote the O_2 evolution reaction, being stable in acid media [20], with moderate service life in alkaline media [22]. SnO_2 possesses interesting properties to produce physisorbed hydroxyl radicals ($\text{M}(\bullet\text{OH})$) but its great drawback is the short service life [3]. MMO electrodes like IrO_2 - SnO_2 - Sb_2O_5 tend to increase the stability and durability, and show higher conductivity [20]. Furthermore, the IrO_2 interlayer enhances the generation of physisorbed hydroxyl radicals ($\text{M}(\bullet\text{OH})$). Thus, IrO_2 acts as catalyst, SnO_2 behaves as dispersing agent and catalyst, while Sb_2O_5 is a dopant.

The performance of the MO and MMO electrodes depends on: (i) the preparation method of the ink to be deposited onto the substrate (sol-gel or polymeric precursor method), (ii) the coating method (immersion, painting, electrophoresis) [23], (iii) the thermal treatment to obtain the MO or MMO crystallographic phases, and (iv) the substrate pre-treatment [9]. In earlier articles, we demonstrated the good performance of a Ti|Ir-Sn-Sb oxide anode for the EO treatment of dyes like Methyl Orange [9], Indigo [11] and Acid Yellow 36 [15]. The oxidation of water to adsorbed $\text{M}(\bullet\text{OH})$ on the Ti|Ir-Sn-Sb oxide surface may be carried out according to a mechanism that relies on the adsorption of the water molecule on the acid sites of MMO (reaction (1)), which arise from the acid nature of the Ir-Sn-Sb oxides. This is followed by water

79 discharge via reaction (2). Therefore, the determination of the surface acid sites content is
80 necessary.



83 The evidence of $\text{M}(\bullet\text{OH})$ production at Ti|Ir-Sn-Sb oxide anode was demonstrated in
84 previous communications of our group, using either spin-trapping with *N,N*-dimethyl-4-
85 nitrosoaniline (RNO) [3,10] or by electron paramagnetic resonance (EPR) [15]. However, the
86 characterization of the acid sites has not been reported yet.

87 The aim of this article is the preparation of Ti|Ir-Sn-Sb oxide anodes by the polymeric
88 precursor method (Pechini method), which show several advantages [10], and the evaluation of
89 their service life, as well as to ascertain the role of the acid sites in the formation of $\text{M}(\bullet\text{OH})$
90 from water discharge. The service life was estimated using accelerated life tests, in strong acidic
91 medium under galvanostatic conditions. The influence of the Ir, Sn and Sb molar percentage on
92 service life was also addressed. The acid sites content was determined by the Boehm titration
93 method, which consists in neutralizing the acid sites with a carbonate or hydroxide [24,25].
94 Scanning electron microscopy (SEM) and X-ray diffraction (XRD) were used to examine the
95 morphological and structural changes of the coating.

96 **2. Experimental**

97 *2.1. Chemicals*

98 All solutions were prepared with deionized water. The chemicals for the MMO preparation
99 were $\text{H}_2\text{IrCl}_6 \times \text{H}_2\text{O}$, SnCl_4 , SbCl_3 , citric acid and ethylene glycol of analytical grade purchased
100 from Sigma-Aldrich. RNO and phosphate buffer used for the $\text{M}(\bullet\text{OH})$ detection were of

analytical grade supplied by Sigma-Aldrich. Perchloric acid used for accelerated life tests and other chemicals employed for the pre-treatment of the Ti surface were of reagent grade also provided by Sigma-Aldrich.

2.2. Preparation of the MMO electrodes

The Ti plates were pre-treated by consecutive immersion in concentrated HCl at 70 °C for 1 h and concentrated HNO₃ at room temperature for 20 min. Then, the plates were rinsed with distilled water and dried at room temperature. This pre-treatment served to increase the surface roughness and improve the coating adhesion. Each plate was 4 cm long, 0.5 cm wide and 0.1 cm thick.

The polymeric precursor solution to perform the Pechini method was prepared by mixing citric acid (CA) and ethylene glycol (EG) at 60-70 °C, according to the molar contents summarized in Table 1. The metallic precursors (H₂IrCl₆×H₂O, SnCl₄ and SbCl₃) were added to the mixture (see Table 1), maintaining the temperature at 60-70 °C for 30 min. The resulting solutions were used to coat the pre-treated Ti substrates on both sides using a brush. To obtain electrodes E1 and E3, the coated Ti was heated at 115 °C for 15 min in a furnace to induce the polymerization of the precursor. The overall procedure was repeated until forming 32 layers and, finally, the electrodes were heated at 550 °C for 1 h. To obtain electrodes E2 and E4, the heating after the application of the solution onto the pre-treated Ti substrate was made at 550 °C for 10 min, and the overall procedure was repeated to form 32 layers. A final heating at 550 °C was performed for 1 h. The temperature was controlled to avoid the formation of TiO₂, which occurs at 600 °C, because it would cause passivation [26].

2.3. Surface characterization of the electrodes

The morphological characteristics and distribution of metal oxides of the Ti|Ir-Sn-Sb oxide electrodes were evaluated by SEM, using a Carl Zeiss EVO HD15 scanning electron microscope, coupled with an integrated energy dispersive X-ray detector. The crystal structure of the MMO was analyzed by XRD using a Rigaku Ultima IV diffractometer. The diffraction patterns were measured in the 2θ range from 20° to 70° , using $\text{Cu K}\alpha_1$ $\lambda=1.5418 \text{ \AA}$.

2.4. Detection of generated hydroxyl radicals

RNO was employed as a spin trap for the detection of low concentrations of $\text{M}(\bullet\text{OH})$ formed at the MMO surfaces. This technique is based on the analysis of the solution bleaching, which is confirmed from the absorbance decay at $\lambda_{\text{max}} = 440 \text{ nm}$ [3,10,17]. More details about its effectiveness are reported in previous work [3,10,27]. The absorption spectra of RNO were recorded using a Perkin Elmer Lambda UV/Vis spectrophotometer coupled to an anode half-cell for the *in-situ* detection of $\text{M}(\bullet\text{OH})$. A divided three-electrode cell was employed in order to avoid cathodic interferences during the detection process. Two quartz cells typically used in UV/Vis spectrophotometry were utilized to construct the two half cells, which were connected through a saline bridge of Pyrex glass (containing phosphate buffer) and with a Pt wire welded at each extreme. An MMO anode of 0.66 cm^2 area in contact with 3 mL of anolyte ($5.2 \times 10^{-5} \text{ M}$ RNO in phosphate buffer at $\text{pH} = 7$) and a carbon rod cathode in contact with the same volume of catholyte (phosphate buffer at $\text{pH} = 7$) were used. The reference electrode was an Ag/AgCl (saturated KCl) electrode immersed in a Luggin capillary, which was carefully inserted into the anodic half-cell. The microelectrolysis tests were performed at 25°C using a BioLogic® SP 150 potentiostat-galvanostat running with EC-Lab® software. All the electrode potentials reported in this work are referred to the standard hydrogen electrode (SHE). The oxidation of water was performed at constant anode potential of 1.3 V|SHE for 2 h, carrying

out the *in-situ* monitoring of RNO bleaching from starting yellow solution. Note that the selection of such anode potential was made on the basis of previous optimization work [10]. The absorption spectra of RNO were recorded in the wavelength range between 375 and 515 nm, every 10 min during the 2-h trials.

2.5. Accelerated life tests

The accelerated life test method allowed estimating the service life of the anodes. This procedure was carried out by applying a constant current density (j) of 1 A cm^{-2} to the cell containing 1 M HClO_4 at 25°C , maintained with a recirculation water bath. A typical undivided three-electrode cell made of Pyrex glass with double jacket containing 70 mL of solution was employed. An MMO of 1 cm^2 and a graphite rod with the same area were used as the anode and cathode, respectively, whereas an Ag/AgCl (saturated KCl) was utilized as the reference electrode. The anode potential was plotted against the electrolysis time until an exponential increase of the signal was observed and thus, the time needed for this drastic change was considered as the service life of the MMO anode. The dramatic increase of the anode potential informs about the anode deactivation due to coating failure. Note that this type of test is usually made in strongly acidic media to mimic chemically corrosive environments [19,20].

2.6. Determination of the acid sites content on the MMO anode

The determination of the surface acid sites content was carried out by the Boehm titration [24,25]. To do this, about 0.40 g of electrode material was added to 40 mL of a 0.01 M NaOH solution and maintained under vigorous stirring for 24 h. After that, the resulting solution was titrated with 0.1 M HCl , under magnetic stirring. The pH of the suspension was measured in continuous until reaching the equilibrium. This allowed identifying the milliequivalents of acid sites content per gram of MMO anode (meq g^{-1}) present on its surface. The relationship between

the acid sites content and the rate of $M(\bullet OH)$ production (known from RNO analyses) from combined reactions (1) and (2) was assessed.

3. Results and discussion

3.1. SEM-EDS and XRD characterization

Fig. 1 shows the SEM micrographs obtained for the surfaces of the four MMO electrodes prepared, namely E1, E2, E3 and E4. The chemical composition, revealing the metal ratio in each coating, was analyzed semi-quantitatively by EDS, as collected in Table 2. The SEM image of electrode E1 shows an irregular surface with high roughness, where some small lumps can be observed. Conversely, micrographs of electrodes E2, E3 and E4 highlight much more flat, regular surfaces with good-looking coatings, as expected from a better integration of Ir, Sn and Sb oxides onto the Ti substrate. Electrode E2 presents the less rough surface, which is attributed to the highest content of Ir and Sn, accounting for up to 24.89 at.%. Note that, in particular, Sn was the most abundant metallic element on E2 surface, reaching 21.02 at.%, whereas Ti was detected at the lowest concentration, i.e., 0.75 at.%. The large accumulation of Sn in E2 is apparently surprising, since its molar ratio in the precursor solution was the same as that used for E1, and much lower than those employed for E3 and E4 (Table 1). This means that the much smaller amounts of polymeric precursors, CA and EG, favor the deposition of Sn. In addition, such low amounts of organic compounds enhance the homogeneity of the E2 coating. The sum of Ir and Sn before the tests in the E1, E3 and E4 electrodes was smaller, with values of 20.06, 8.25 and 17.29 at.%, respectively. Therefore, it seems that a higher Sn content is associated to more homogenous and flat coatings, whereas excessively high Ir contents tend to promote irregularities on the surface (Table 2, anode E1).

The X-ray diffraction patterns of the E1, E2, E3 and E4 coatings are presented in Fig. 2. Peaks that can be assigned to Ti, Ir, Sb, Sn, Sb_2O_5 , $\text{Sb}_{31}\text{Ti}_{43.35}$ and SnO_2 phases were found in the four electrodes, highlighting that neither IrO_x nor TiO_x ones were identified. In all these XRD patterns, a broad peak typically associated to an amorphous phase can be observed between 32° and 42° . Other weak peaks at 55.0° , 56.5° , 61.5° and 66.5° could not be assigned to any phase. Since IrO_x was not detected in the diffractograms, it is reasonable to assign the latter XRD peaks to a highly intermixed Ir-Sn-Sb oxide that formed a solid solution. This might be explained by the kind of synthesis employed, which included a thermal treatment that promotes the solid state diffusion of all metals to form the final MMO [15].

3.2. Influence of acid sites content on the formation of adsorbed hydroxyl radicals

Table 3 summarizes the acid sites content found for the four electrodes prepared, which reached high values varying from 0.21 to 0.26 meq g^{-1} . In order to elucidate whether these acid sites play a fundamental role in the formation of hydroxyl radicals onto the surface of the MMO anodes, the kinetics of RNO removal upon EO treatment was studied by carrying out several microelectrolyses, in the presence and absence of acid sites. UV/Vis spectra of the solutions were recorded and the maximum absorbance values were determined at $\lambda = 440 \text{ nm}$.

Fig. 3 depicts the time course of the absorption spectra of RNO with electrolysis time for the four anodes in the presence of their natural acid sites. A regular decay of the RNO absorbance until 120 min of electrolysis can be observed for all the electrodes, thereby confirming its reaction with adsorbed $\text{M}(\bullet\text{OH})$ in all cases. A similar set of trials was performed after the neutralization of the acid sites onto the MMO electrodes (not shown). Fig. 4a and b shows the decay of the RNO concentration as a function of time in the presence and absence of acid sites, respectively. The corresponding inset panels show the semi-logarithmic plots of these

curves and evidence the good fit. Therefore, the concentration decay follows a pseudo-first-order reaction kinetics in both sets of experiments, which means that a constant concentration of $M(\bullet OH)$ is formed during the EO treatments with these types of anodes, either in the absence or presence of acid sites. This is then a relevant finding, since it suggests that $M(\bullet OH)$ production from water oxidation is not controlled by the amount of acid sites. Table 3 collects the apparent rate constants in the presence (k_{app}) and absence (k_{app}^*) of acid sites, as determined from the slopes of the linear correlations shown in the insets of Fig. 4a and b. These data show that the kinetics of $M(\bullet OH)$ formation is not proportional to the number of acid sites. For example, the concentration of such sites on the MMO electrodes increased in the order: $E2 < E3 < E4 < E1$, whereas k_{app} rose as $E4 \leq E1 < E3 < E2$. In the absence of the acid sites, k_{app}^* slightly decreased as compared to k_{app} , growing in the order $E1 < E4 < E3 < E2$, that is, inversely to the initial concentration of acid sites. Overall, our results suggest that other kinds of active sites seem to catalyze the $M(\bullet OH)$ production.

3.3 Accelerated life tests performed on the MMO electrodes

The results obtained for the accelerated life tests of the four electrodes used as anodes are presented in Fig. 5. As can be seen, the anode potential versus electrolysis time plots were recorded until a drastic potential rise appeared, being this time assumed as the service life of each MMO anode. The service life of the anodes tested decreased according to the following sequence: $E2 \gg E4 > E1 > E3$. It is particularly remarkable the long service life of electrode E2, as long as 351 h, in contrast to the very short ones of E1 (23 h) and E3 (13 h). Although the service life of 37 h of the E4 electrode was superior to those of the two latter ones, it underwent a progressive passivation from the beginning of the accelerated life test, suggesting that the E4 electrode was the less stable MMO of the anodes synthesized. On the other hand, the good

performance of E2 can be related to the regular and uniform surface coverage shown in Fig. 1, which is in turn associated to the large presence of SnO₂ (Table 2). Furthermore, the higher temperature used for E2 and E4 electrodes (consecutive cycles at 550 °C) also seems to contribute favorably to their larger stability as a result of a better adhesion of the MMO coating on the Ti substrate.

The metal content in the coatings after the accelerated life tests is also listed in Table 2. These data evidence a high increase in the percentage of Ti, along with a notable decrease of the percentages of Ir, Sn and Sb, as compared to those measured in the raw electrodes. This behavior confirms that the coatings were detached from the titanium surface during the accelerated life tests. Worth mentioning, when using these anodes for the EO treatment of POPs, the formation of some by-products may lead to the appearance of metal complexes, which could cause a quicker destabilization of the electrodes. Then, the accelerated life test method only allows the estimation of the service life of the MMO anodes.

Finally, just as an example, if we consider the use of the E2 anode in an EO at a $j = 10 \text{ mA cm}^{-2}$ to mineralize POPs, assuming the absence of polymer film formation on the E2 anode surface during the electrolysis, one can infer that this MMO anode would have a service life as long as 1460 days (about 4 years).

4. Conclusions

Ti plates were successfully coated with Ir, Sn and Sb oxides by the polymeric precursor method (Pechini method). SEM-EDS and XRD corroborated that the synthesized electrodes were mainly composed of a mixture of Ir-Sn-Sb oxides. The analysis of service life of four different anodes, estimated from accelerated life tests at 1 A cm^{-2} , highlighted that a high Sn content and high heating temperature are crucial parameters. The best MMO anode reached up to 351 h of service life. EDS analyses proved that the coatings were detached from the substrate during the accelerated life tests. The acid sites content on the surface of the anodes varies between $0.21\text{-}0.26 \text{ meq g}^{-1}$, but it cannot be correlated with a larger or poorer production of $\text{M}(\bullet\text{OH})$ from water discharge.

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Table 1

Molar content of organic chemicals and metals in the polymeric precursor solutions employed for the preparation of different anodes.

Electrode	EG	CA	Ir	Sn	Sb
E1	16	0.12	0.0296	0.0296	0.0004
E2	3.2	0.024	0.0296	0.0296	0.0004
E3	16	12	0.0296	0.2371	0.0296
E4	16	12	0.0296	0.2371	0.0296

Table 2

Atomic percentages of the elements present on the surface of the anodes prepared, namely E1, E2, E3 and E4, as measured by EDS analysis.

Element	E1	E1 [*]	E2	E2 [*]	E3	E3 [*]	E4	E4 [*]
Ti	2.92	38.45	0.75	24.44	2.53	27.18	4.81	24.12
Sn	2.85	0.40	21.02	6.07	5.06	1.55	12.94	0.41
Sb	0.73	0.21	0.77	0.61	2.52	0.81	6.42	0.12
Ir	17.21	0.50	3.87	1.53	3.19	1.40	4.35	0.35
O	76.29	60.44	73.59	67.35	86.70	69.07	71.48	75.00

^{*} After accelerated life test.

Table 3

Acid sites content of the MMO anodes, and apparent rate constants for the decays of the RNO absorbance shown in the semi-logarithmic plots of Fig. 4a,b.

Electrode	Acid sites / meq g ⁻¹	k_{app} (s ⁻¹)	R^2	k_{app}^* (s ⁻¹)	R^2
E ₁	0.26	0.0221	0.995	0.0191	0.991
E ₂	0.21	0.0265	0.983	0.0230	0.979
E ₃	0.22	0.0246	0.994	0.0222	0.989
E ₄	0.23	0.0217	0.990	0.0212	0.985

* After the acid sites content was neutralized.

Figure captions

Fig. 1. Scanning electron micrographs of the MMO anodes E1, E2, E3 and E4.

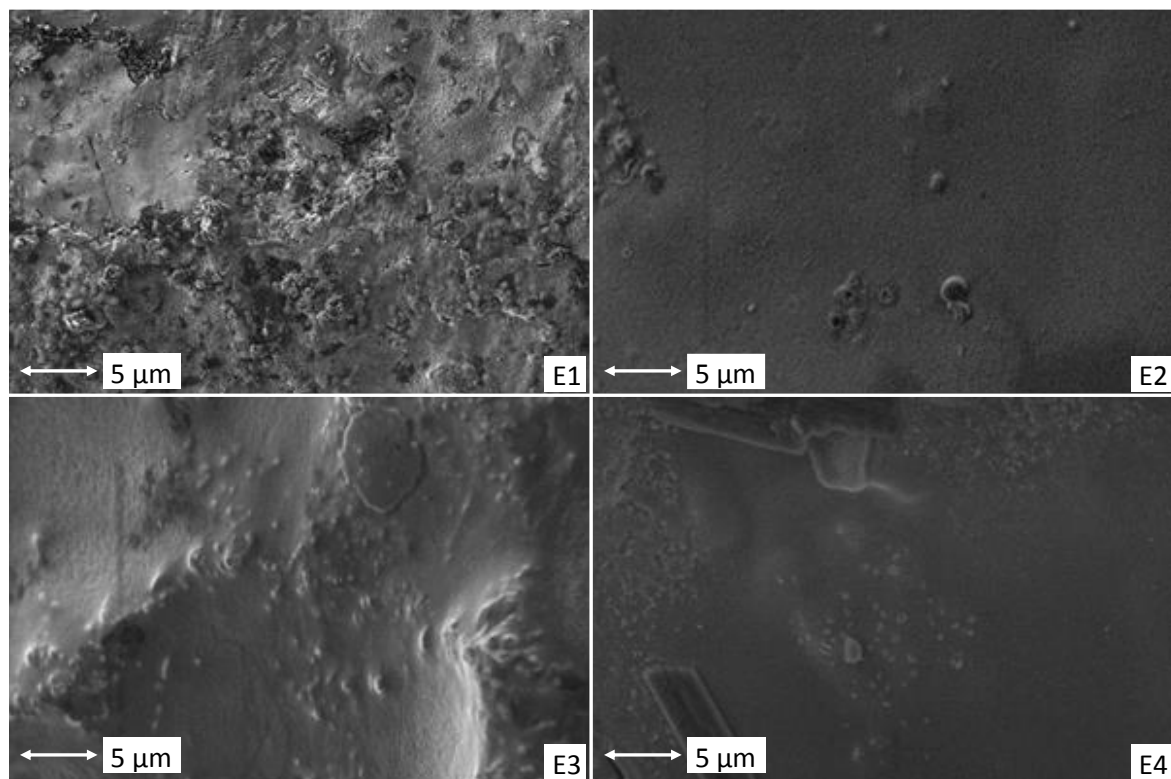
Fig. 2. XRD patterns of the MMO anodes E1, E2, E3 and E4.

Fig. 3. Absorption spectra of RNO solutions obtained at 10 min intervals upon 2-h electrolyses using the MMO anodes E1, E2, E3 and E4, with immersed area of 0.66 cm^2 . The solutions contained 3 mL of $5.2 \times 10^{-5} \text{ M}$ RNO in phosphate buffer solution of $\text{pH} = 7$, at 25°C . Anodic potential: 1.3 V|SHE . Measurements were made under quiescent conditions.

Fig. 4. Change of RNO concentration with electrolysis time using the MMO anodes E1, E2, E3 and E4. (a) Curves obtained from absorbance data shown in Fig. 3. (b) Similar curves, obtained after neutralization of acid sites. The inset panels present the corresponding pseudo-first-order kinetic analysis.

Fig. 5. Service life tests of the MMO anodes E1, E2, E3 and E4. Electrolyses were performed in 1 M HClO_4 , at 1 A cm^{-2} and 25°C , using an immersed electrode area of 1 cm^2 . Measurements were made under quiescent conditions.

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Fig. 1

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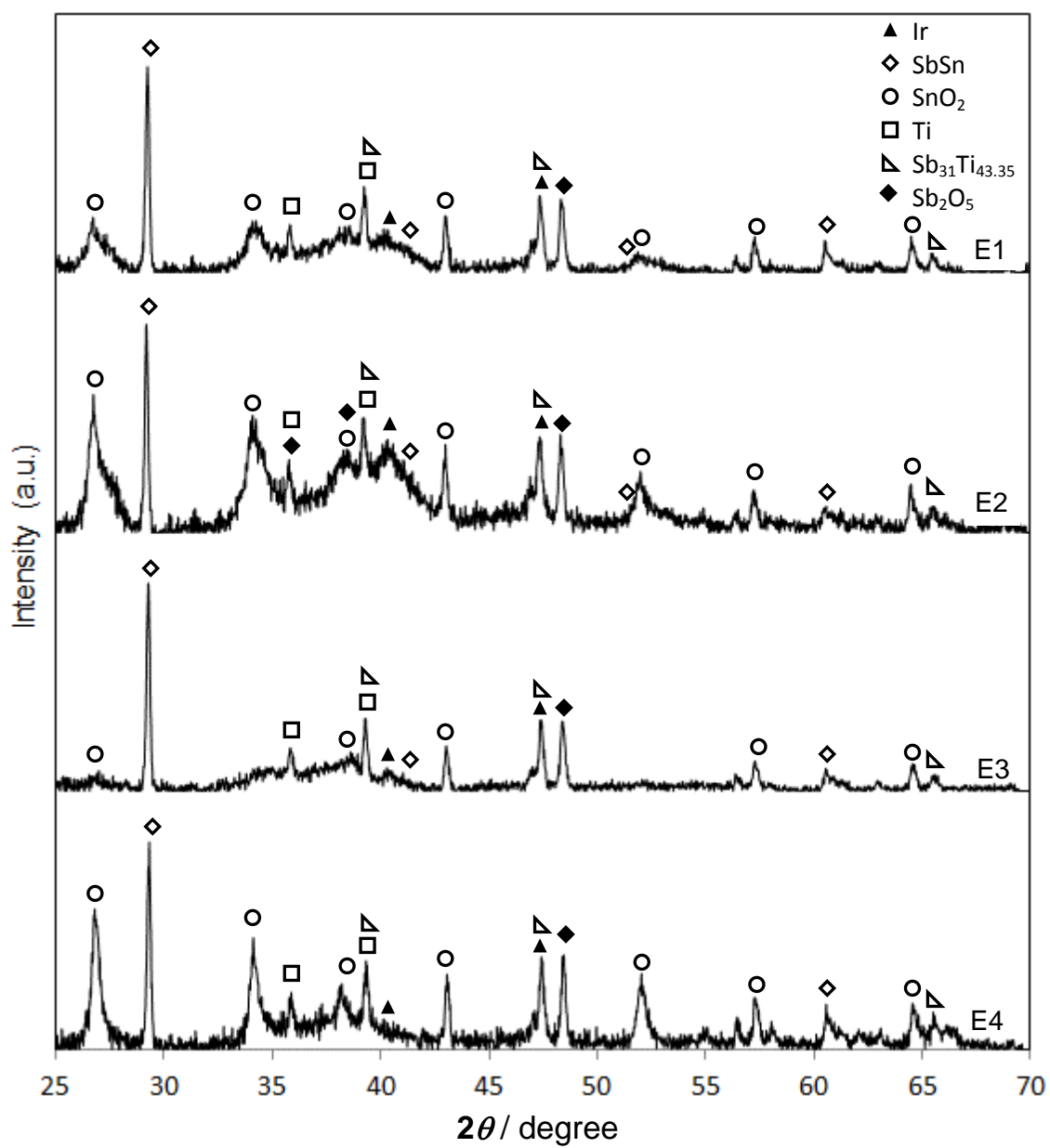
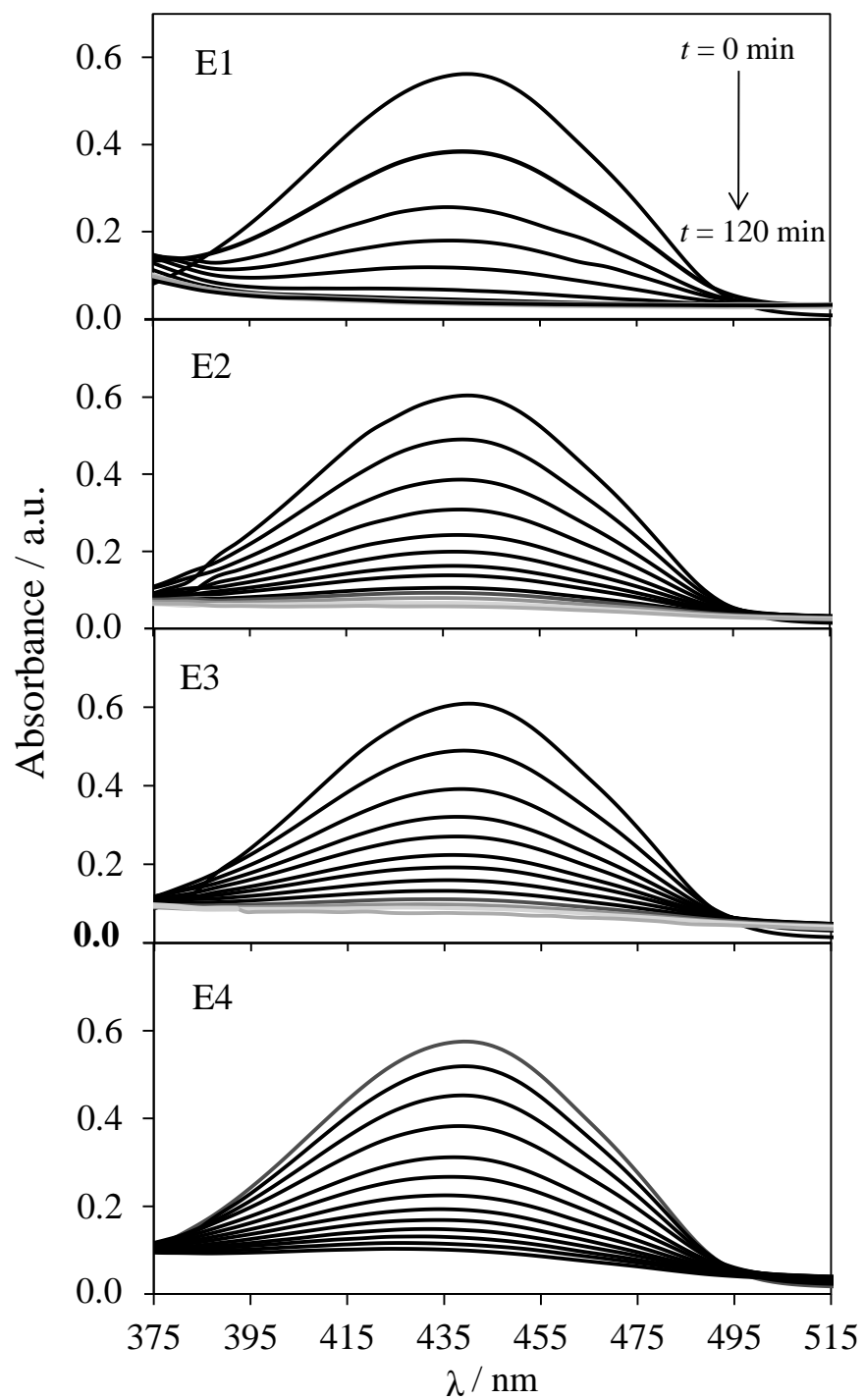


Fig. 2

**Fig. 3**

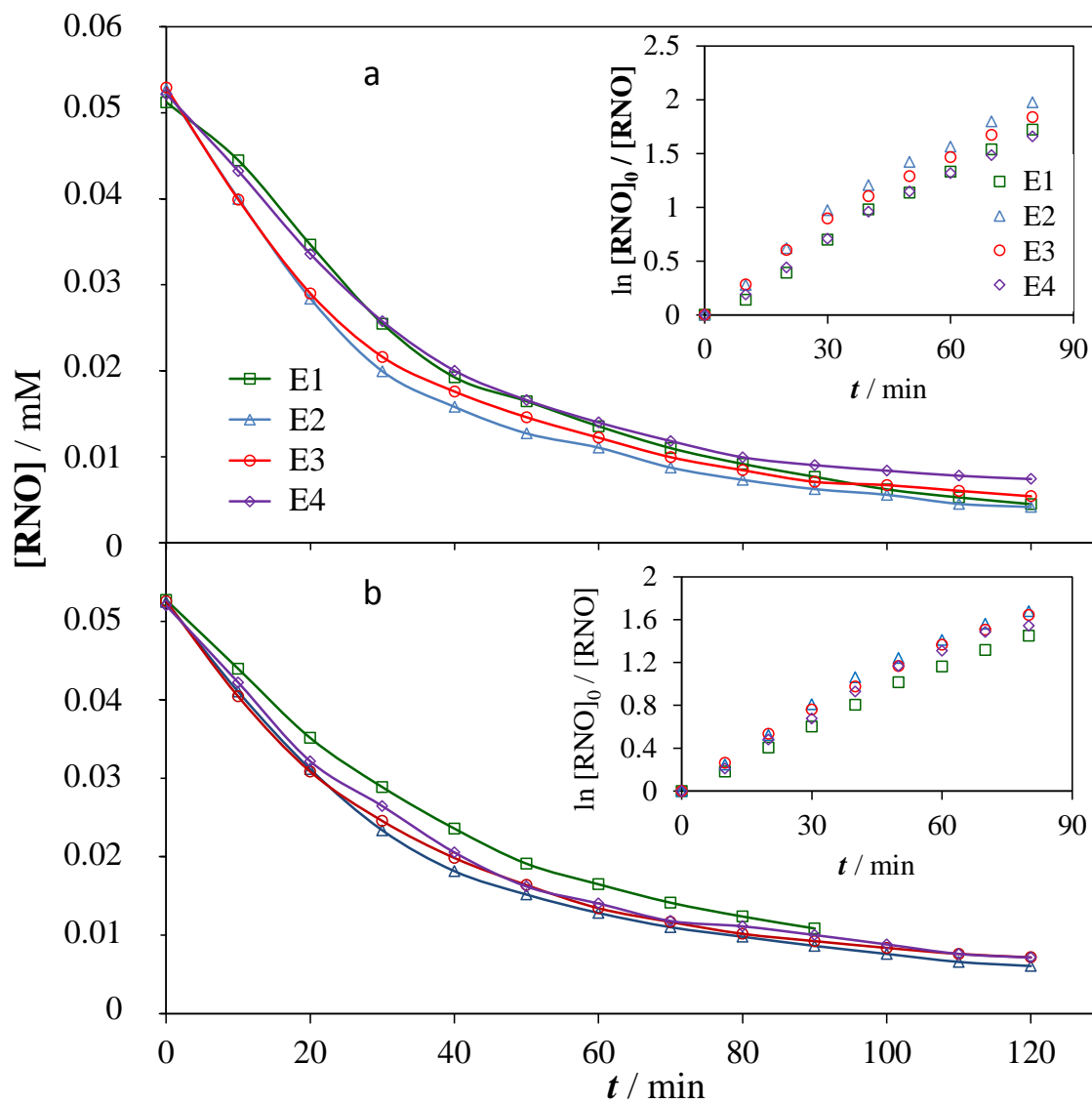
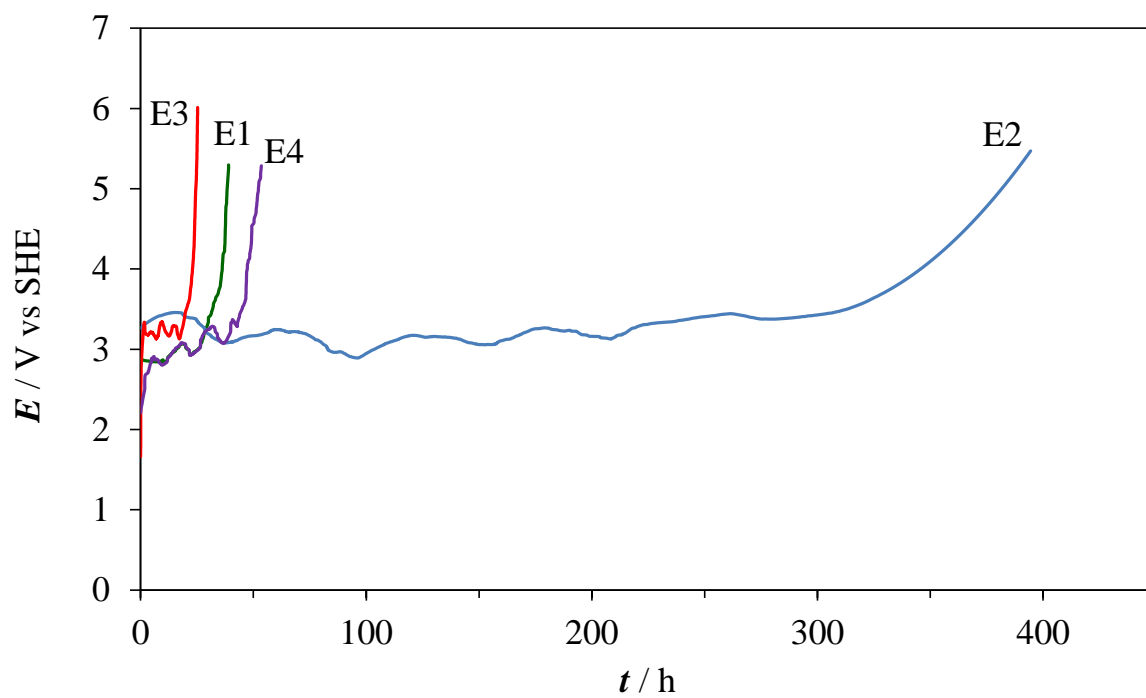


Fig. 4

**Fig. 5**