# 1 Mineralization of Methyl Orange azo dye by processes based

# on H<sub>2</sub>O<sub>2</sub> electrogeneration at a 3D-like air-diffusion cathode

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#### **Abstract**

- 19 This work addresses the mineralization of the widely used Methyl Orange (MO) azo dye by technologies based on H<sub>2</sub>O<sub>2</sub> electrogeneration at a 3D-like air-diffusion cathode. These 20 include two Fe2+-catalyzed processes such as electro-Fenton (EF) and photoelectro-21 Fenton (PEF). Bulk electrolyses were performed in a recirculation flow plant, in which 22 23 the Eco-Cell filter-press electrochemical reactor was connected in series with a UVA photoreactor. The former reactor was equipped with a Ti|Ir-Sn-Sb oxide plate anode 24 alongside a 3D-like air-diffusion cathode made from graphite felt and hydrophobized 25 26 carbon cloth, aimed at electrogenerating H<sub>2</sub>O<sub>2</sub> on site. The influence of current density (i), volumetric flow rate (O) and initial MO concentration was examined. The greatest 27 oxidation power corresponded to PEF process. The best operation conditions to treat 30 28 mg L<sup>-1</sup> of total organic carbon of MO in a 50 mM Na<sub>2</sub>SO<sub>4</sub> solution by PEF were found at 29  $0.50 \text{ mM Fe}^{2+}$ , pH 3.0,  $i = 20 \text{ mA cm}^{-2}$  and  $Q = 2.0 \text{ L min}^{-1}$ , obtaining 100% and 94% of 30 color and TOC removals at 240-300 min, respectively. This accounted for 35% of 31 mineralization current efficiency and 0.12 kWh (g TOC)<sup>-1</sup> of energy consumption at the 32 end of the electrolysis. The oxidation power of EF and PEF was compared with that of 33 anodic oxidation (AO), and the sequence obtained was: PEF > EF > AO. The dye was 34 gradually degraded, yielding non-toxic short carboxylic acids, like maleic, fumaric, 35 formic, oxalic and oxamic, whose Fe(III) complexes were rapidly photolyzed. 36
- 37 Keywords: Azo dye; Gas-diffusion electrode; Hydrogen peroxide; Photoelectro-Fenton;
- Water treatment

#### 1. Introduction

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40 The incessant growth of industrial and urban activities has led to a progressive increase 41 in the clean water demand. The resulting large volumes of wastewater are quite difficult 42 to adequately manage through currently available technologies (McDonald et al., 2014; Cosgrove and Loucks, 2015). Many industries, from textile and leather to cosmetics or 43 44 food employ synthetic dyes in their production chains, becoming a major source of contaminated aqueous effluents (Tkaczyk et al., 2020). The synthetic dyestuffs are 45 categorized as persistent organic pollutant (POPs) because they tend to be designed with 46 47 structural characteristics that confer them a high stability against hydrolysis, natural photolysis or biodegradation (Routoula and Patwardhan, 2020). For this reason, these 48 dyes and some of their by-products are accumulated in water reservoirs, being ubiquitous 49 in surface water in some countries (Bhatia et al., 2018), representing a huge risk to 50 humans and the aquatic life (Khan and Malik, 2018). 51 The textile industry employs more than 30 million workers all over the world and the total 52 production of synthetic dyes approaches  $7 \times 10^5$  tons (Brillas and Martínez-Huitle, 2015; 53 Desore and Narula, 2018). Azo dyes, characterized by the presence of at least one -N=N-54 functional group as chromophore linked to aromatic rings, constitute the main category 55 56 with more than 70% of the produced dyestuffs (Rawat et al., 2016). Methyl Orange (MO) 57 is an anionic monoazo dye (see characteristics in Table SM-1) widely used in the textile, printing and photographic industries (Guo et al., 2011). Although its impact on humans 58 and animals has been scarcely reported, the genetic effects of azo dyes are well 59 60 established (Chung, 2016). Therefore, a range of technologies has been investigated to remove MO from water. They include physical methods like adsorption (Arshadi et al., 61 2014) and chemical ones such as heterogeneous Fenton (Omri et al., 2020), heterogeneous 62

photocatalysis (Saravanan et al., 2018), anodic oxidation (AO) with various anodes (Zhou 63 et al., 2011; Chaiyont et al., 2013; Isarain-Chávez et al., 2017) and electro-Fenton (EF) 64 (Sirés et al., 2010; Jiang et al., 2016). In contrast, the photoelectro-Fenton (PEF) treatment 65 of MO solutions has not been investigated yet, which is a significant finding because this 66 67 is considered the most promising electrochemical advanced oxidation process (EAOP) (Brillas, 2020). 68 69 Fenton-based EAOPs like EF and PEF processes have become increasingly popular for the fast degradation of organic pollutants in water (Brillas and Martínez-Huitle, 2015; 70 Brillas and Sirés, 2015; Zhou et al., 2018; Brillas, 2020). The common feature of these 71 72 methods is the in-situ H<sub>2</sub>O<sub>2</sub> electrogeneration from the cathodic reduction of O<sub>2</sub>, according to reaction (1) (Coria et al., 2015; Le et al., 2015; Scialdone et al., 2015; Zhou 73 et al., 2018; Salmerón et al., 2019), which is highly efficient at carbon-based materials 74 like carbon black (Lanzalaco et al., 2017; Lima et al., 2020), carbon nanotubes (Gendel 75 et al., 2014; Alcaide et al., 2020), graphene (Le et al., 2015; Yang et al., 2019), carbon 76 felt / graphite felt (El-Ghenymy et al., 2013; Lin et al., 2017; Pérez et al., 2018) or vitreous 77 carbon (González-Pérez and Bisang, 2014; Zhou et al., 2018). Some of these materials 78 have been implemented as cathodes that are simultaneously in contact with the conductive 79 80 solution and an air chamber fed with O<sub>2</sub> or air, in the so-called gas-diffusion electrodes (GDE) conformation, which is the most suitable to produce H<sub>2</sub>O<sub>2</sub> (El-Ghenymy et al., 81 2013; Barazesh et al., 2015; Yu et al., 2015; Lanzalaco et al., 2017; Coria et al., 2018; 82

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$$O_2 + 2H^+ + 2e^- \rightarrow H_2O_2$$
 (1)

Salmerón et al., 2019; Lima et al., 2020).

If the production of H<sub>2</sub>O<sub>2</sub> takes place in the presence of dissolved Fe<sup>2+</sup> (i.e., EF conditions), hydroxyl radicals (\*OH) and Fe<sup>3+</sup> are generated in the bulk via Fenton's reaction (2), whose optimum pH is ~3.0 (Brillas, 2020). Fe<sup>3+</sup> can be reduced at the cathode to yield Fe<sup>2+</sup> from reaction (3), which sustains the catalytic cycle (Brillas and Sirés, 2015). The organics present in such an oxidizing environment can be partially mineralized by OH in a non-selective manner, according to general reaction (4) (Martinez-Huitle et al., 2015).

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$$Fe^{2+} + H_2O_2 \rightarrow Fe^{3+} + {}^{\bullet}OH + OH^-$$
 (2)

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$$Fe^{3+} + e^{-} \rightarrow Fe^{2+}$$
 (3)

$$94 R + {}^{\bullet}OH \rightarrow CO_2 + H_2O (4)$$

However, total mineralization is not feasible in EF, since very stable complexes between 95 Fe(III) and some organic by-products are formed upon cleavage of the aromatic or cyclic 96 97 structures (Zhou et al., 2018). The PEF process was developed to overcome that drawback thanks to the high photosensitivity of those complexes under UVA irradiation (Brillas, 98 2020). UVA photons cause the photolysis of main dissolved Fe(III) species, such as 99 Fe(OH)<sup>2+</sup> via reaction (5) and metal-organic complexes from reaction (6) (El-Ghenymy 100 et al., 2013; Alcaide et al., 2020). Note that both reactions involve the photoregeneration 101 of Fe<sup>2+</sup>, which feeds reaction (2) to enhance the \*OH production. 102

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$$[Fe(OH)]^{2+} + hv \rightarrow Fe^{2+} + {}^{\bullet}OH$$
 (5)

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$$[Fe(OOCR)]^{2+} + hv \rightarrow Fe^{2+} + CO_2 + R^{\bullet}$$
 (6)

On most occasions, EF and PEF treatments are carried out in undivided reactors, which is advantageous because the POPs can be additionally degraded by AO promoted by the adsorbed radicals formed on the anode surface (M) from water discharge via reaction (7) (Martinez-Huitle et al., 2015). Boron-doped diamond (BDD) (Cornejo et al., 2020) and

dimensionally stable anodes (DSA) (Lanzalaco et al., 2018) are typically employed for this purpose.

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$$M + H_2O \rightarrow M(^{\bullet}OH) + H^+ + e^-$$
 (7)

This work discusses the performance of an electrochemical reactor equipped with inhouse-made 3D-like GDE as the cathode and Ir-Sn-Sb oxide as the anode, referred to the color removal and mineralization of MO solutions by PEF process as compared to AO and EF. The 3D-like GDE was used to guarantee the efficient formation of H<sub>2</sub>O<sub>2</sub> and to improve the mass transport (Pérez et al., 2018). The filter-press Eco-Cell was combined in series with a UVA photoreactor, and 2 L of solution were treated under recirculation mode in each trial. The characterization of the reaction environment along the oxidation of MO in the presence of 50 mM Na<sub>2</sub>SO<sub>4</sub> and 0.50 mM Fe<sup>2+</sup> at pH 3.0 was systematically addressed in terms of the operation variables such as current density (*j*), volumetric flow rate (*Q*) and initial dye concentration. Carboxylic acids generated were monitored chromatographically during the PEF treatment.

#### 2. Experimental

*2.1. Chemicals* 

Analytical grade chemicals have been employed. Methyl Orange ( $C_{14}H_{14}N_3NaO_3S$ , dye content 85%, Sigma-Aldrich) played a role as model contaminant, whereas sodium sulfate (Karal) was added to ensure a high conductivity. Ferrous sulfate heptahydrate added as catalyst in EF and PEF was supplied by Fermont. All synthetic solutions were prepared with three-distilled water at room temperature (298  $\pm$  2 K). The pH of the solutions was adjusted with diluted NaOH and  $H_2SO_4$  solutions, both reagents acquired

from Fermont. Carboxylic acids used as standards were from Sigma-Aldrich. The solvents used for high-performance liquid chromatography (HPLC) analysis were of chromatographic grade from Karal.

## 2.2. Description of the flow plant

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An Eco-Cell was employed as the electrochemical reactor (Fig. 1). It was equipped with a Ti|Ir-Sn-Sb oxide anode, manufactured following the Pechini method according to our recently reported procedure (Aguilar et al., 2017, 2018). Its dimensions of breadth (3.0 cm) and length (8.0 cm) conferred a total area of 24 cm<sup>2</sup> that contacted with the liquid phase. A 3D-like air-diffusion cathode was prepared by placing a commercial carbon cloth (ROOE Group) of 24 cm<sup>2</sup>, previously hydrophobized with polytetrafluorethylene (PTFE) (Coria et al., 2018; Pérez et al., 2018), below a graphite felt (ROOE Group) piece  $(3.0 \text{ cm breadth} \times 8.0 \text{ cm length} \times 0.25 \text{ cm thickness}, 651 \text{ cm}^2 \text{ cm}^{-3} \text{ volumetric area, } 10$  $100 \times 10^{-3} \ \Omega^{-1} \ cm^{-1}$  electrical conductivity). The assembly was made by direct contact, without using any adhesive. A stainless-steel frame with a window of 3.0 cm breadth × 8.0 cm length  $\times 0.23 \text{ cm}$  thickness was used as current collector for the cathode. The back side of the carbon cloth was in contact with an air chamber (3.0 cm breadth × 8.0 cm length  $\times$  0.55 cm thickness) fed with atmospheric air pumped with a DeWalt compressor model D55168, regulating the pressure at 3 psi to electrogenerate H<sub>2</sub>O<sub>2</sub>. The front side of the carbon cloth and the graphite felt piece were in contact with the solution. A polypropylene separator was used in the anode side to act as flow distributor, whereas a plastic mesh (promoter type D) (Rivera et al., 2015) was placed between the anode and cathode as well as into the air chamber. An acrylic tank with capacity of 2 L was connected in series with the Eco-Cell. This reservoir was covered with a black box that contained a 15 W UVA lamp with  $\lambda_{max} = 365$  nm, being turned on in PEF trials and off 155 in AO and EF. In AO process, the setup was the same but the GDE was replaced by a Ti|RuO<sub>2</sub> plate as the cathode to avoid the H<sub>2</sub>O<sub>2</sub> electrogeneration. The electrochemical 156 reactor and the reservoir were connected by hydraulic PVC pipes of 1.27 cm in diameter. 157 The solution was recirculated by a magnetic pump (Little Giant, model 4-MD-HC) and 158 the flow rate was adjusted by means of a PVC valve and measured with a Cole Palmer 159 flow meter in the range of 0.5-4.0 L min<sup>-1</sup>. A BK precision power supply model 1621A 160 was used to work under galvanostatic conditions. The cell voltage was monitored with 161 the same equipment. Fig. SM-1 depicts a sketch of the flow plant. 162

# 163 2.3. Methodology

To evaluate the performance of the three advanced processes, 2 L of acidic (pH 3.0) 164 solutions containing a given concentration of MO with 50 mM Na<sub>2</sub>SO<sub>4</sub>, in the absence or 165 presence of  $0.50 \,\mathrm{mM}\,\mathrm{Fe^{2+}}$ , were electrolyzed in duplicate at constant *j*, *Q* and temperature. 166 167 Further, the operation parameters evaluated to characterize the PEF process were *j* (10-25 mA cm<sup>-2</sup>), Q (0.5-2.0 L min<sup>-1</sup>) and the initial dye concentration (20-50 mg L<sup>-1</sup> total 168 organic carbon (TOC)). The values of catalyst concentration and pH were fixed because 169 these have been conveniently optimized in previous works for the EF and PEF treatments 170 of various POPs (El-Ghenymy et al., 2013; Alcaide et al., 2020). 171

#### 172 2.4. Analytical methods

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The solution pH was measured with a HANNA HI991300 pH-meter and adjusted to 3.0 with an  $H_2SO_4$  solution (10 vol.%). The decolorization of MO solutions was monitored from the decrease of absorbance measured at the maximum ( $\lambda_{max} = 464$  nm) employing a Perkin Elmer Lambda 35 UV/Vis spectrophotometer, at 298 K. The decolorization

percentage was determined from the starting absorbance ( $A_0$ ) and its value at time t ( $A_t$ ), as follows:

$$\% \text{ Color removal} = \frac{A_t - A_0}{A_0} x 100 \tag{8}$$

Before the analysis of samples treated by EF and PEF, the pH was adjusted to ~8.0 with an NaOH solution (0.25 M) to stop the Fenton's reaction thanks to the precipitation of the dissolved iron. TOC was determined using a Torch combustion analyzer, from Teledyne Tekmar. All samples were previously filtered using 0.45 µm cellulose nitrate syringe filters supplied from Whatman. The results discussed throughout the article are the average of duplicate trials and thus, the data shown in figures are accompanied by their corresponding error bars.

The time profiles of linear carboxylic acids were assessed via ion-exclusion HPLC technique, employing a Perkin Elmer Flexar liquid chromatograph (Murrieta et al., 2020).

The chromatograms exhibited very good peaks related to oxalic, maleic, oxamic, formic and fumaric acids at retention times of 7.5, 9.4, 10.5, 14.7 and 19.3 min, respectively. The electrolytic energy consumption (EC) and mineralization current efficiency (MCE) were also determined (see below).

## 3. Results and discussion

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194 3.1. Comparative ability of AO, EF and PEF processes to degrade MO

A first series of AO, EF and PEF trials was carried out to assess their oxidation power during the degradation of the MO azo dye. The study of the AO degradation of solutions containing MO at a TOC concentration of 30 mg L<sup>-1</sup> and 50 mM Na<sub>2</sub>SO<sub>4</sub> as supporting

electrolyte at pH 3.0 was carried out in the Eco-Cell equipped with the Ti|Ir-Sn-Sb oxide anode and a Ti|RuO<sub>2</sub> cathode. The study of the EF and PEF processes was carried out upon replacement of the Ti|RuO<sub>2</sub> by the 3D-like air-diffusion cathode, supplied with O<sub>2</sub> that is reduced at the cathode to form  $H_2O_2$  via reaction (1). The same electrolyte was used, but in the presence of 0.50 mM Fe<sup>2+</sup>.

Fig. 2a shows the results obtained for the decolorization analysis at j=20 mA cm<sup>-2</sup> and Q=2.0 L min<sup>-1</sup>. The color removal followed the order: AO < EF < PEF, and agreed with a pseudo-first-order reaction kinetics (see inset of Fig. 2a) that yielded increasing values of apparent rate constants  $(k_1)$ . The constant was  $0.35 \times 10^{-2}$  min<sup>-1</sup> (with  $R^2=0.98$ ),  $13.45 \times 10^{-2}$  min<sup>-1</sup> ( $R^2=0.92$ ) and  $18.04 \times 10^{-2}$  min<sup>-1</sup> ( $R^2=0.99$ ) for AO, EF, PEF processes, respectively. A slow color loss of the MO solution can be observed in AO, meaning that the radical M(\*OH) formed from reaction (7) did not completely destroy the chromophore group (-N=N-). Worth mentioning, during the water discharge, the oxygen evolution reaction via the overall reaction (9) took place to a large extent and generated M(\*OH) was partially converted into a weak metal oxide (Martinez-Huitle et al., 2015). This behavior drastically reduced the ability of the anode to produce large quantities of reactive M(\*OH) and, as a result, only about 80% of color removal was reached at the end of the AO process. Meanwhile, in EF and PEF, the homogeneous \*OH radicals produced by Fenton's reaction (2) and/or photolytic reaction (5) broke rapidly the azo bond of the chromophore group, yielding more than 99% decolorization after 30 min of electrolysis.

$$218 2H_2O \rightarrow 4H^+ + O_2 + 4e^- (9)$$

Fig. 2b depicts the decrease of TOC related to MO mineralization. The AO process only destroyed a 19% of TOC, whereas the EF process improved the mineralization up to a

- 221 66%. Complete MO mineralization was not achieved in the latter treatment, owing to the
- production of hardly oxidizable Fe(III) complexes with organic by-products. Meanwhile,
- in the PEF process, the mineralization was significantly upgraded thanks to the effect of
- UVA radiation, which accelerated the regeneration of Fe<sup>2+</sup> ion from reaction (5) and
- 225 quickly photodecomposed the Fe(III)-carboxylate complexes from reaction (6). Thus,
- TOC was reduced to 1.8 mg L<sup>-1</sup>, yielding an almost total mineralization of 94%.
- From the above TOC measurements, two important parameters like the mineralization
- 228 current efficiency (MCE) and the energy consumption (EC) were estimated to
- characterize the processes. The MCE was determined according to Eq. (10), and the
- included parameters have been defined elsewhere (Isarain-Chávez et al., 2017; Coria et
- 231 al., 2018).

232 %MCE = 
$$\frac{nFV_s\Delta(TOC)_{exp}}{4.32x10^7 mlt} \times 100$$
 (10)

- In particular, the number of carbon atoms of the initial MO was m = 14, whereas the
- constant number of electrons (n = 86) involved in the dye mineralization came from Eq.
- 235 (11), assuming overall conversion of heteroatoms into  $NO_3^-$  and  $SO_4^{2-}$  ions:

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$$C_{14}H_{14}N_3NaO_3S + 38H_2O \rightarrow 14CO_2 + 3NO_3^- + SO_4^{2-} + Na^+ + 90H^+ + 86e^-(11)$$

- The EC values were calculated from Eq. (12), with  $E_{cell}$  accounting for the average cell
- voltage (in V) (Martinez-Huitle et al., 2015; Coria et al., 2018):

239 EC (kWh (g TOC)<sup>-1</sup>) = 
$$\frac{E_{\text{cell}}It}{V_{\text{S}}\Delta(TOC)_{\text{exp}}}$$
 (12)

- 240 Fig. 2c presents the percentage of current efficiency for the assays of Fig. 2b. The highest
- MCE values were verified for the PEF process, with a maximal of 54% at 150 min,

242 whereupon it decayed to 23% at 420 min. This decrease of MCE is indicative of the formation of more recalcitrant by-products with the simultaneous loss of organic load 243 (Brillas and Martinez-Huitle, 2015; Martínez-Huitle et al., 2015; Isarain-Chávez et al., 244 2017). The superiority of PEF over EF is primordially due to the additional photolysis of 245 Fe(III) complexes, since in both methods, the main oxidizing agent is \*OH formed from 246 Fenton's reaction (2). In contrast, much smaller MCE values varying between 5-15% 247 were determined in AO, as expected from the low oxidizing ability of M(\*OH). The above 248 behavior is also reflected in the corresponding EC values given in Fig. 2d. In all cases, 249 EC increased over electrolysis time and the lowest values were obtained in the most 250 efficient process, i.e., PEF, finally obtaining 0.18 kWh (g TOC)<sup>-1</sup>. 251 From the above results, one can establish that the PEF process was the most powerful for 252 the decolorization and mineralization of MO. The influence of current density, volumetric 253 flow rate and initial MO concentration on its performance was then systematically 254 analyzed with the purpose of finding the best operation conditions for PEF. 255 3.2. Influence of operating parameters on PEF performance 256 The percentage of color removal profiles with respect to electrolysis time at *i* values 257 between 10 and 25 mA cm<sup>-2</sup>, at  $Q = 2.0 \text{ L min}^{-1}$  and MO at TOC content of 30 mg L<sup>-1</sup>, 258 are depicted in Fig. 3a. A similar decolorization rate can be observed and more than 98% 259

color decay was always achieved at about 30 min of electrolysis. The color removal followed a pseudo-first order reaction kinetics (see inset of Fig. 3a), highlighting that  $k_1$  increased slightly with current density in the interval 10-20 mA cm<sup>-2</sup> and then, at 25 mA cm<sup>-2</sup>,  $k_1$  decreased (Table 1). From this, it can be deduced that the amount of M( $^{\bullet}$ OH) and

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 $^{ullet}$ OH produced at the lowest j (10 mA cm $^{-2}$ ) was already sufficient to attack the target

pollutant and all its colored by-products. In contrast, Fig. 3b shows that TOC was more rapidly abated at 20 mA cm<sup>-2</sup>, reaching a maximum mineralization of 94% at 240-300 min. A similar TOC abatement was achieved at 15 mA cm<sup>-2</sup>, although much more slowly since about 420 min of electrolysis were required. The enhancement observed when j was increased from 10 to 20 mA cm<sup>-2</sup> can be pre-eminently attributed to the higher production of H<sub>2</sub>O<sub>2</sub> that caused a larger formation of •OH from Fenton's reaction (2) and photolytic reaction (5). The quantity of Fe(III) complexes, originated more quickly, was then photolyzed earlier via reaction (6), enhancing the mineralization. However, this trend was not accomplished at 25 mA cm<sup>-2</sup>, causing a quick deceleration of TOC removal. This can be associated to a faster increase in rate of the parasitic reactions involving M(OH) and OH, diminishing their attack over organics. Examples of these unwanted reactions are the anodic oxidation of the former radical to O<sub>2</sub> from reaction (13), or the dimerization of the second one to H<sub>2</sub>O<sub>2</sub> via reaction (14). Free OH can also react with the latter oxidant to form the weaker hydroperoxyl radical (HO $_2$  $^{\bullet}$ ) from reaction (15), or oxidize Fe $^{2+}$  to Fe<sup>3+</sup> via reaction (16) (Brillas and Martínez-Huitle, 2015; Ye et al., 2019; Alcaide et al., 2020).

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$$281 2M(^{\bullet}OH) \rightarrow 2M + O_2 + 2H^{+} + 2e^{-} (13)$$

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$$2^{\circ}OH \rightarrow H_2O_2$$
 (14)

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$$H_2O_2 + {}^{\bullet}OH \rightarrow HO_2{}^{\bullet} + H_2O$$
 (15)

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$$Fe^{2+} + {}^{\bullet}OH \rightarrow Fe^{3+} + OH^{-}$$
 (16)

Fig. 3c illustrates a larger decay of MCE as j became higher, which is more evident at long electrolysis time, as expected from the inverse relationship of this parameter with

current from Eq. (10). The highest MCE (95%) was found at the lowest j (10 mA cm<sup>-2</sup>), 287 dropping down to 42% at the end of the treatment. The opposite tendency can be observed 288 in Fig. 3d for the EC values, which were gradually raised at increasing j since this was 289 also accompanied by the concomitant increase in  $E_{cell}$ . Final values of 0.10, 0.14, 0.18 290 and 0.26 kWh (g TOC)<sup>-1</sup> at growing j of 10, 15, 20 and 25 mA cm<sup>-2</sup>, respectively, were 291 obtained. All these findings allow inferring that 20 mA cm<sup>-2</sup> was the optimum current 292 density for the MO treatment under the experimental conditions tested. 293 In a flow cell, the volumetric flow rate is a key operation parameter since the 294 hydrodynamics regulates the mass transport of species toward the electrodes. An 295 enhancement of the reaction rate of all electrode reactions, with generation of more 296 quantities of H<sub>2</sub>O<sub>2</sub> from reaction (1), could be expected as Q was increased, thereby 297 yielding more OH (Pérez et al., 2018). This would upgrade the attack of M(OH) and 298 OH over organics and the earlier photodecomposition of photoactive by-products under 299 UVA light irradiation. To clarify this behavior, the PEF treatment of MO at TOC 300 concentration of 30 mg L<sup>-1</sup> was investigated at the optimum j = 20 mA cm<sup>-2</sup> and Q values 301 ranging between 0.5 and 2.0 L min<sup>-1</sup>. 302 It is clear from Fig. 4a that the lowest Q (0.5 L min<sup>-1</sup>) caused the poorest decolorization 303 rate since total color removal was reached after more than 300 min of electrolysis. In 304 contrast, Q values  $\geq 1.0 \text{ L min}^{-1}$  needed less than 60 min for total color loss. It is worth 305 mentioning that the decolorization kinetics, was very similar at  $Q \ge 1.0 \text{ L min}^{-1}$  (see inset 306 of Fig. 4a), giving relatively close values of  $k_1$  (Table 1). This points to consider that 307 under the latter conditions, sufficient amounts of oxidizing agents were formed and 308 rapidly transported to destroy the target pollutant, whereas at lower Q values the mass 309

transport of reactants toward the electrode became insufficient and the electrode reactions became slower. Fig. 4b clearly highlights the enhancement of TOC abatement at higher Q, in agreement with the greater generation of M(OH) and OH alongside the quicker photolysis of intermediates. At the end of the treatment, TOC was reduced by 60%, 75% and 80% at 0.5, 1.0 and 1.5 L min<sup>-1</sup>, much lower than 94% obtained at 2.0 L min<sup>-1</sup>. The same tendency can be seen for MCE in Fig. 4c, whose final values increased from 17% at 0.5 L min<sup>-1</sup> to 23% at 2.0 L min<sup>-1</sup>, whereas Fig. 4d evidences the progressive rise of EC up to a value of 0.28 kWh (g TOC)<sup>-1</sup> at the lowest Q. Hence,  $2.0 \text{ L min}^{-1}$  can be considered an optimum Q in PEF process. The ability of PEF process to destroy the organic pollutants formed in MO solutions was examined at initial concentrations within the TOC range of 20-50 mg L<sup>-1</sup> using the optimal j = 20 mA cm<sup>-2</sup> and Q = 2.0 L min<sup>-1</sup>. At all these contents, total decolorization was quickly achieved in 30-60 min of electrolysis (see Fig. 5a). Overall, the decolorization kinetics became slower as the initial TOC concentration was increased from 20 to 50 mg L<sup>-1</sup> (see inset of Fig. 5a and  $k_1$  values in Table 1). However, Fig. 5b shows that the mineralization was accelerated when initial TOC was increased from 20 to 30 mg L<sup>-1</sup>, whereupon it was gradually decelerated, although a similar 79% of mineralization was attained at TOC of 20, 40 and 50 mg L<sup>-1</sup>. This allows inferring a continuous rise in the quantity of TOC removed, which can be accounted for by a progressive increase of the amounts of M(OH) and OH that effectively reacted with MO and its by-products. Since the same quantity of these oxidizing agents is always expected in the electrolytic system because the same i was applied, this phenomenon can be related to the gradual decrease in reaction rate of their parasitic reactions, like reactions (13)-(16), as result of their favored attack over the larger number of organic molecules. This

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behavior presupposes a concomitant growing of MCE with decreasing of EC, as can be confirmed in Fig. 5c and d, respectively. At the greatest MO concentration (TOC of 50 mg L<sup>-1</sup>), these parameters reached values of 32% and 0.14 kWh (g TOC)<sup>-1</sup>, respectively. Despite this, the most favorable mineralization occurred at TOC of 30 mg L<sup>-1</sup>, when the maximum overall destruction of by-products was reached thanks to the combined action of M(\*OH), \*OH and UVA radiation.

3.3. Time course of final carboxylic acids

- The final carboxylic acids were detected and quantified by ion-exclusion HPLC analysis of the MO solution at TOC of 30 mg L<sup>-1</sup> treated by PEF under the best operation conditions, i.e., j = 20 mA cm<sup>-2</sup> and Q = 2.0 L min<sup>-1</sup>. Maleic, fumaric, formic, oxalic and oxamic acids were identified. Maleic and fumaric acids were generated from the cleavage of the aromatic moiety, being subsequently oxidized to formic and oxalic acids that were converted into CO<sub>2</sub> (Martinez-Huitle et al., 2015; Isarain-Chávez et al., 2017; Brillas, 2020). In contrast, the other final acid (oxamic) was expected from the progressive destruction of *N*-intermediates. Under the PEF conditions tested, all these acids were largely present in solution as Fe(III)-carboxylate complexes.
- Fig. 6 highlights that maleic, fumaric, formic and oxamic acids were accumulated up to  $0.6 \text{ mg L}^{-1}$  as maximal, disappearing after 180 min of electrolysis. Oxalic acid was much largely accumulated, reaching 15.9 mg L<sup>-1</sup> at 90 min. Then, it was rapidly removed and only a residual amount of  $0.5 \text{ mg L}^{-1}$  was detected because of the effective photolysis of Fe(III)-oxalate complexes via reaction (6). This means that the final solution with TOC of  $1.8 \text{ mg L}^{-1}$  contained TOC <  $0.2 \text{ mg L}^{-1}$  related to this acid, suggesting the formation of a small proportion (about 5.3% of initial TOC) of more recalcitrant final by-products.

#### **Conclusions**

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358 The EF treatment of MO solutions in a flow plant led was more effective than AO, as 359 result of the larger production of \*OH in the bulk. This was feasible by the great ability of the 3D-like air-diffusion cathode to electrogenerate H<sub>2</sub>O<sub>2</sub>. The low oxidation power of 360 M(\*OH) generated at the Ti|Ir-Sn-Sb oxide anode explained the lower oxidation ability 361 of AO. The PEF process was superior thanks to the continuous regeneration of Fe<sup>2+</sup> 362 catalyst induced by UVA photons. The progressive transformation of the target pollutant 363 allowed reaching total color removal and 94% TOC abatement under optimum conditions 364  $(j = 20 \text{ mA cm}^{-2} \text{ and } Q = 2.0 \text{ L min}^{-1})$ . This resulted in an MCE and EC of 35% and 0.12 365 kWh (g TOC)<sup>-1</sup>, respectively. Small contents of maleic, fumaric, formic and oxamic acids 366 were formed, being oxalic acid the prevailing short-chain carboxylic acid. However, it 367 was very rapidly reduced to trace amounts (TOC < 0.2 mg L<sup>-1</sup>) due to the effective 368 photolysis of Fe(III)-oxalate species. These results confirm that the oxidation power of 369 the PEF process with a 3D-like GDE is enough to treat azo dyes in water. 370

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### Figure captions

- Figure 1. Diagram of the electrochemical reactor showing the labelled components.
- Figure 2. Change of (a) color removal, (b) normalized TOC content, (c) mineralization
- current efficiency and (d) electrolytic energy consumption with electrolysis time during
- different treatments: ( $\Diamond$ ) AO, ( $\circ$ ) EF and ( $\Delta$ ) PEF. Conditions: 2 L of a solution with MO
- at a concentration of 30 mg L<sup>-1</sup> of TOC, 50 mM Na<sub>2</sub>SO<sub>4</sub> and 0.50 mM Fe<sup>2+</sup> at pH 3.0,
- treated at  $Q = 2.0 \text{ L min}^{-1}$  and  $j = 20 \text{ mA cm}^{-2}$ . The inset in plot (a) shows the pseudo-
- 553 first-order kinetic analysis for MO decolorization.
- Figure 3. Change of (a) color removal (see kinetic analysis in the inset), (b) TOC, (c)
- 555 mineralization current efficiency and (d) electrolytic energy consumption with
- electrolysis time for PEF treatments at different j: ( $\Diamond$ ) 10, ( $\circ$ ) 15, ( $\Delta$ ) 20 and ( $\nabla$ ) 25 mA
- 557 cm<sup>-2</sup>. Same conditions as described in Fig. 2.
- Figure 4. Effect of the volumetric flow rate under the same conditions described in Fig.
- 3, at 20 mA cm<sup>-2</sup>. Q: ( $\Diamond$ ) 0.5, ( $\circ$ ) 1.0, ( $\Delta$ ) 1.5 and ( $\nabla$ ) 2.0 L min<sup>-1</sup>. The inset in plot (a)
- shows the pseudo-first-order kinetic analysis for MO decolorization.
- Figure 5. Effect of the initial dye concentration under the same conditions described in
- Fig. 3, at 20 mA cm<sup>-2</sup>. [MO]: ( $\lozenge$ ) 20, ( $\circ$ ) 30, ( $\triangle$ ) 40 and ( $\nabla$ ) 50 mg L<sup>-1</sup> of TOC. See the
- kinetic analysis in the inset of plot (a).
- Figure 6. Time course of the concentration of (■) oxalic, (●) maleic, (▲) oxamic, (▼)
- formic and (•) fumaric acids during the mineralization of the MO solution by PEF under
- the conditions described in Fig. 2. The inset shows a magnification of the same profiles.

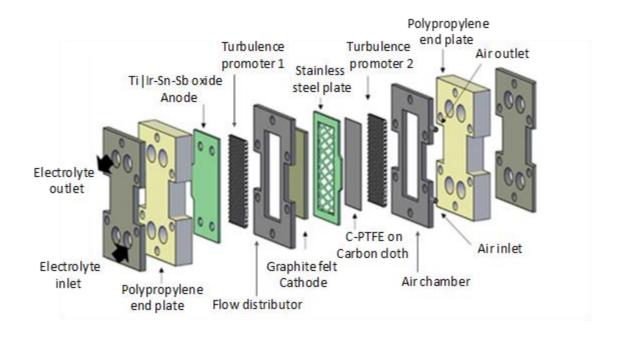


Figure 1

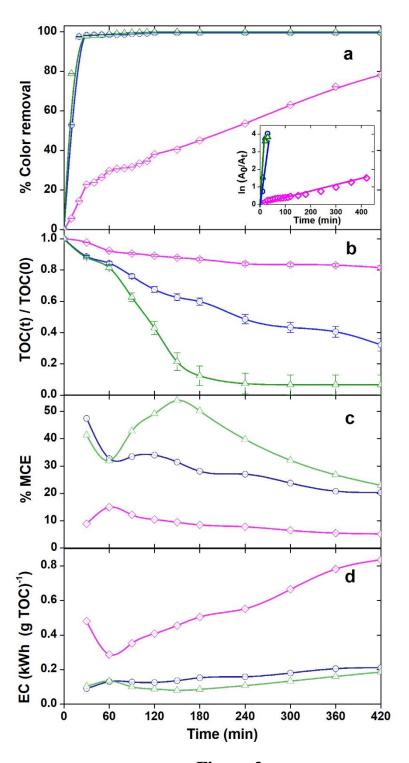


Figure 2

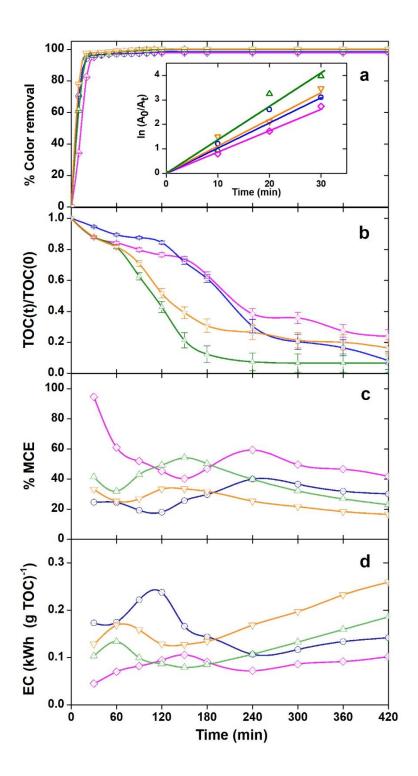


Figure 3

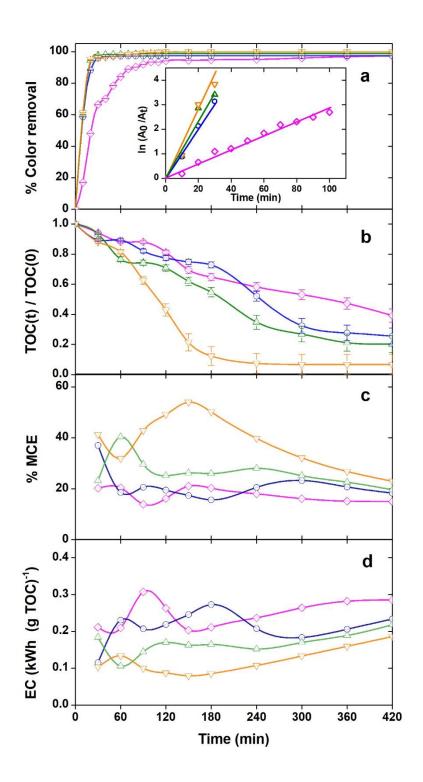


Figure 4

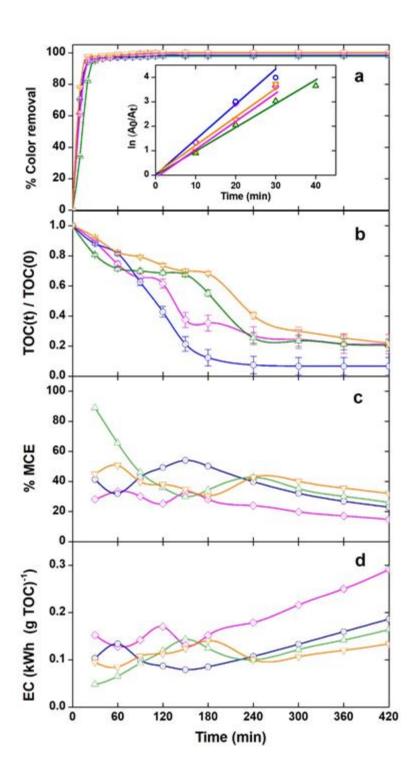


Figure 5

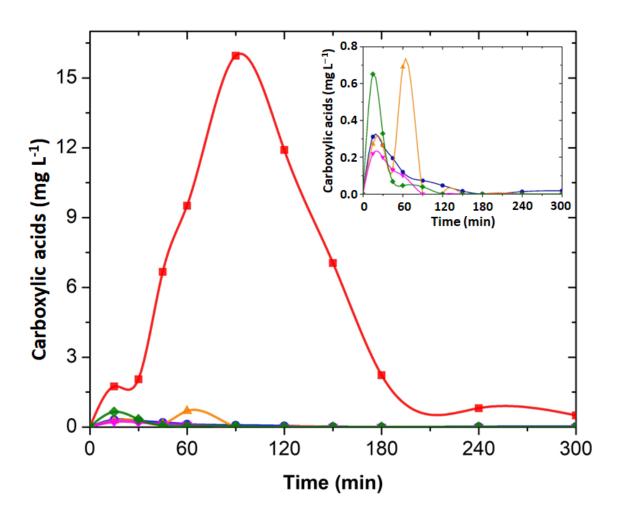


Figure 6

**Table 1.** Pseudo-first-order rate constants and *R*-squared values, along with the percentage of TOC removal and energy consumption per unit TOC mass for the PEF treatment of 2 L of MO solutions in the presence of 0.5 mM Fe<sup>2+</sup> at pH 3.0 and 298  $\pm$  2 K, using the ECO-cell with an Ir-Sn-Ru oxide anode and a 3D-like air-diffusion cathode.

j	TOC(0)	Q	$k_1$	$R^2$	% TOC	EC
(mA cm <sup>-2</sup> )	$(mg L^{-1})$	(L min <sup>-1</sup> )	(10 <sup>-2</sup> min <sup>-1</sup> )		removal	(kWh (gTOC) <sup>-1</sup> )
10	30	2.0	8.22	0.96	76.2	0.84
15	30	2.0	11.01	0.97	91.9	1.62
20	20	2.0	10.95	0.95	78.7	1.81
	30	0.5	2.70	0.98	60.9	2.47
		1.0	10.45	0.99	74.5	2.12
		1.5	12.48	0.97	79.8	1.65
		2.0	18.04	0.99	93.5	1.17
	40	2.0	9.13	0.90	79.6	1.12
	50	2.0	12.07	0.95	78.1	1.12
25	30	2.0	12.87	0.93	83.7	1.70