



Article Alkali-Activated Binders Using Bottom Ash from Waste-to-Energy Plants and Aluminium Recycling Waste

Alex Maldonado-Alameda ^(D), Jofre Mañosa ^(D), Jessica Giro-Paloma ^(D), Joan Formosa ^(D) and Josep Maria Chimenos *^(D)

Departament de Ciència de Materials i Química Física, Universitat de Barcelona, C/Martí i Franquès, 108028 Barcelona, Spain; alex.maldonado@ub.edu (A.M.-A.); jofremanosa@ub.edu (J.M.); jessicagiro@ub.edu (J.G.-P.); joanformosa@ub.edu (J.F.)

* Correspondence: chimenos@ub.edu; Tel.: +34-93-402-1316

Abstract: Alkali-activated binders (AABs) stand out as a promising alternative to replace ordinary Portland cement (OPC) due to the possibility of using by-products and wastes in their manufacturing. This paper assessed the potential of weathered bottom ash (WBA) from waste-to-energy plants and PAVAL[®] (PV), a secondary aluminium recycling process by-product, as precursors of AABs. WBA and PV were mixed at weight ratios of 98/2, 95/5, and 90/10. A mixture of waterglass (WG) and NaOH at different concentrations (4 and 6 M) was used as the alkaline activator solution. The effects of increasing NaOH concentration and PV content were evaluated. Alkali-activated WBA/PV (AA-WBA/PV) binders were obtained. Selective chemical extractions and physicochemical characterization revealed the formation of C-S-H, C-A-S-H, and (N,C)-A-S-H gels. Increasing the NaOH concentration and PV content increased porosity and reduced compressive strength (25.63 to 12.07 MPa). The leaching potential of As and Sb from AA-WBA/PV exceeded the threshold for acceptance in landfills for non-hazardous waste.

Keywords: MSWI; weathered bottom ash; aluminium salt slag; alkali-activated materials; waste valorization; by-product

1. Introduction

The importance of waste management is increasing every year due to the large amount of residues generated as a result of the increasing population, urbanization, and rising living standards [1]. European Union (EU) countries are channelling their efforts into implementing innovative strategies and policies based on the recycling, re-use, and reduction of residues [2]. The European Waste Framework Directive (2008/98/EC) promotes the search for viable alternatives for waste management and efficient resource use. It also promotes zero-waste policies to mitigate waste management problems. The zero-waste concept is based on an infrastructural change in waste management involving all the manufacturing stages and aiming to transform residues into resources [3]. The goal is to move toward low-carbon zero-waste manufacturing through developing new secondary materials by turning residues into raw materials [4].

Municipal solid waste (MSW) represented around 10% of the 2.54 billion tonnes of waste generated in the European Union (EU) in 2018 [5,6]. Around 30% of the MSW is incinerated in waste-to-energy (WtE) plants [5]. MSW incineration (MSWI) can recover energy and reduce landfilling, as well as decrease the mass (70%) and volume (90%) of the MSW [7]. Approximately 20% of the MSWI becomes a product known as incinerator bottom ash (IBA), which is mainly composed of a mineral fraction (80–85 wt. %), ferrous metals (10–12 wt. %, mainly steel), and non-ferrous metals (2–5 wt. %, two-thirds of which is aluminium) [8,9]. IBA is highly heterogeneous and contains potentially leachable soluble salts and heavy metalloids [10]. A natural weathering process that involves storing the IBA outdoors (2–3 months) is necessary to immobilize the heavy metalloids and stabilize pH



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Copyright: © 2021 by the authors. Licensee MDPI, Basel, Switzerland. This article is an open access article distributed under the terms and conditions of the Creative Commons Attribution (CC BY) license (https:// creativecommons.org/licenses/by/ 4.0/). through the carbonation of the fresh IBA [11]. The resulting material after the weathering process is known as weathered bottom ash (WBA). The particle size distribution and a composition rich in glass, ceramics, stones, bricks, and melting products [12] make the WBA suitable for cement production [13], as aggregates in road construction, concrete, or mortars [14,15], or for the manufacture of ceramic-based products [16]. However, the use of WBA in engineering is limited due to its environmental risks and inferior properties compared to natural aggregates and products. Research on the potential applications of WBA must therefore be focused on those that minimize the leaching potential of heavy metalloids [10]. In this sense, WBA can be used as an aluminosilicate precursor in alkali activation technology, since a cementitious matrix can immobilize heavy metalloids. Some recent studies have demonstrated the potential of WBA as a precursor in the synthesis of alkali-activated cements (AACs) [17–19].

AACs are high-strength binders obtained from the reaction between an aluminosilicaterich solid precursor and an alkaline activator [20]. One of their main advantages is that they can be formulated from aluminosilicate-rich urban, industrial, agro-industrial, and mining wastes [21,22]. AACs are an excellent alternative to mitigating the CO₂ emissions and energy consumption associated with the production of ordinary Portland cement (OPC) [23]. Hence, the production of AACs can promote suitable waste management and sustainable cement production. Additionally, the properties of the AACs are very promising and comparable to those of OPC [24]. These properties vary depending on the curing temperature [25], the alkaline activator used [26], the SiO₂/Al₂O₃ ratio, and the calcium content [27]. The aluminium content plays an essential role in the alkali activation, which affects the nature of the formed products and the strength of the AACs [28,29]. Therefore, the use of aluminium correctors is necessary when the AACs are obtained from the alkali activation of precursors that have a substantial lack of reactive aluminium compared to reactive silica, as is the case with WBA [17,30].

In this study, new sustainable alkali-activated binders (AABs) were obtained from the alkali activation of municipal and industrial waste. The least polluted fraction of WBA (8 to 30 mm) was used, given that it has the lowest concentrations of heavy metalloids and the highest SiO_2 availability [17,31]. Additionally, this fraction allows enhancing the mechanical properties of alkali-activated WBA binders as reported elsewhere by the authors [32]. PAVAL[®] (PV) was also used as a source of reactive aluminium. PV is an industrial waste generated from the salt slag recovery phase of the secondary aluminium recycling process [33]. This aluminium salt slag is processed to separate PV (mainly composed of aluminium oxides) from metallic aluminium and flux, as well as from scarified salts (NaCl and KCl) [34]. Recent studies have shown the potential applications of PV in the cement, ceramic, refractory, and building industries [33,35]. The main goal of this study was to formulate AABs using the coarser and least polluted fraction of WBA and PV (AA-WBA/PV) to enhance the mechanical properties of the alkali-activated WBA binders (AA-WBA) obtained previously [36]. The valorization of WBA and PV contributes to the zero-waste principle and low-carbon manufacturing and gives an added value to the final material. Several AA-WBA/PV formulations were developed by mixing WBA and PV at different weight ratios and using a mixture of sodium silicate (Na_2SiO_3) and sodium hydroxide (NaOH) as the alkaline activator solution. The effects of PV and the alkaline activator concentration on the AA-WBA/PV binders were also evaluated.

2. Materials and Methods

2.1. Materials

WBA and PV were used as precursors to prepare the AA-WBA/PV formulations. The WBA was supplied by the VECSA company and collected from a WtE plant located in Tarragona (Spain), which produces $32 \text{ kt} \cdot \text{y}^{-1}$. PV was provided by the BEFESA company from its salt slag treatment plant located in Valladolid (Spain), which generates around 90 kt·y⁻¹ of this aluminium salt slag [35]. Na₂SiO₃ was supplied by Scharlab, S.L. (Barcelona, Spain),

while the NaOH solutions were prepared by dissolving NaOH pearls (Labbox Labware S.L. (Barcelona, Spain); purity > 98%) in deionized water.

The WBA and PV were first dried for 24 h in a stove at 105 °C. Both materials were then sieved through standard sieves to determine the particle size distribution (PSD) (shown in Figure 1). The shaded area of the WBA in Figure 1 shows the least polluted fraction (8 to 30 mm), which was used to formulate the AA-WBA/PV binders. Finally, the WBA and PV were crushed and milled separately until a particle size below 80 μ m was obtained.



Figure 1. Particle size distribution (PSD) of weathered bottom ash (WBA) and PAVAL® (PV).

Table 1 shows the chemical compositions of the WBA and PV determined by X-ray fluorescence (XRF) using the Panalytical Philips PW2400 Sequential X-ray spectrophotometer (Malvern Panalytical, Malvern, United Kingdom) equipped with the UniQuant[®] version 5.0 software. The main oxide compounds identified in the WBA were SiO₂, Al₂O₃, and CaO from the high levels of glass cullet and fired ceramics in the least polluted fraction [31]. The main oxides found in PV were SiO₂ and Al₂O₃. Therefore, the WBA and PV were considered potential AABs precursors due to their calcium aluminosilicate-rich nature. Furthermore, these elemental oxides have reactive phases (amorphous SiO₂ and Al₂O₃) to form AABs, as well as unreactive or less reactive phases (SiO₂ and Al₂O₃ crystalline phases) that probably remain inert in the alkali-activation process.

	WBA (wt. %)											
-	SiO₂ 52.08	CaO 20.72	Al ₂ O ₃ 6.35	Na₂O 3.38	Na2OK2OFe2O33.382.094.12		MgO 2.43	TiO₂ LOI 0.65 6.1				
	PV (wt. %)											
-	SiO₂ 7.93	CaO 2.24	Al ₂ O ₃ 61.02	Na₂O 3.22	K₂O 0.68	Fe₂O₃ 2.65	MgO 4.73	TiO₂ 0.80	LOI ¹ 15.71			
- 3												

Table 1. Major and minor elements composition of weathered bottom ash (WBA) and PAVAL[®] (PV) powders.

¹ Loss on ignition at 1100 °C.

The availability of the reactive phases of the WBA and PV was assessed using different concentrations of NaOH solution (4, 6, or 8 M) [17,37]. These experimental trials consisted of mixing 1 g of WBA and PV with 100 mL of the NaOH solution in a Teflon beaker and stirring for 5 h at 80 °C. Afterwards, the leached Si and Al concentrations were determined by analyzing the resulting filtered solution with inductively coupled plasma optical emission spectrometry (ICP-OES) using the PerkinElmer Optima 3200 RL spectrometer (PerkinElmer Inc., Waltham, MA, USA). The percentages of available SiO₂ and Al₂O₃ in both the WBA and PV are plotted in Figure 2. Around 20% of SiO₂ and 3% of Al₂O₃ were available in the WBA, while approximately 2.5–5% of SiO₂ and 35% of Al₂O₃ were available in PV. These



results indicate that the WBA and PV have the potential to be secondary silica-rich and alumina-rich sources, respectively.

Figure 2. SiO₂ and Al₂O₃ availability percentage in (a) WBA and (b) PV samples.

X-ray diffraction (XRD) analysis of the WBA and PV was conducted with a Bragg–Brentano Siemens D-500 powder diffractometer (Siemens, Munich, Germany) with CuK α radiation. The main crystalline phases detected in the WBA were quartz (SiO₂; PDF# 01-079-1910) and calcite (CaCO₃; PDF# 01-083-1762), as shown in Figure 3a. Other minor phases such as dolomite (CaMg(CO₃)₂; PDF# 01-075-1759), akermanite (Ca₂Mg(Si₂O₇); PDF# 01-079-2424), anhydrite (CaSO₄; PDF# 01-072-0503), albite calcian-ordered ((Na,Ca)Al(Si,Al)₃O₈; PDF# 020-0548), microcline (KAlSi₃O₈; PDF# 01-076-0918), and muscovite (KAl₂(AlSi₃O₁₀)(OH)₂; PDF# 01-077-2255) were also identified.



Figure 3. XRD patterns of (a) WBA and (b) PV.

Gibbsite (Al(OH)₃; PDF# 01-070-2038), bayerite (Al(OH)₃; PDF# 01-077-0114), nordstrandite (Al(OH)₃; PDF# 01-072-0623), corundum (Al₂O₃; PDF# 01-071-1123), and spinel (MgAl₂O₄; PDF# 01-077-0435) were detected as the major crystalline phases in PV (Figure 3b). Minor phases such as aluminium nitride (AlN; PDF# 01-075-1620), potassium sodium aluminium silicate (Al(K,Na)O₆Si₂; PDF# 01-070-1260), potassium aluminium oxide (AlKO₂; PDF# 01-084-0380), calcium fluoride (CaF₂; PDF# 01-077-0245), cryolite (Na₃AlF₆; PDF# 25-0772), and quartz (SiO₂; PDF# 01-079-1910) were also identified. The XRD results were consistent with those of the XRF analysis, demonstrating the calcium aluminosilicate-rich composition of the WBA and PV.

2.2. AA-WBA/PV Preparation

Table 2 shows the mixture proportion of the AA-WBA/PV formulations, the silicate modulus (Ms) of the alkaline activator solution, and the alkali dosage (Na₂O wt. %). The weight percentages of the WBA and PV (referred to as solid (S)) varied, while the weight percentage of the alkaline activator (referred to as liquid (L)) was fixed. A mixture of Na₂SiO₃ (26.44% of SiO₂ and 8.21% of Na₂O; $\rho = 1.37$ g·cm⁻³) and NaOH solution (4 or 6 M) was prepared as the alkaline activator solution. The liquid-to-solid (L/S) mass ratio was fixed (0.6) to maintain good workability of the pastes during the mixing and casting process. The use of 8 M NaOH solution and the addition of more than 10% of PV were discarded, since both excessively increased porosity through the reaction between the aluminium nitride in PV and NaOH, generating ammonia gas [38].

	S			L				
Reference	WRA 1	PV 1	NaOH ²		Na ₂ SiO ₂ 2	Na ₂ O ¹	SiO ₂ /Na ₂ O ³	
	WDA	1 V	4 M	6 M				
W98-PV2-4M	98	2	20		80	5.2	2.5	
W95-PV5-4M	95	5	20		80	5.2	2.5	
W90-PV10-4M	90	10	20		80	5.2	2.5	
W98-PV2-6M	98	2		20	80	5.8	2.3	
W95-PV5-6M	95	5		20	80	5.8	2.3	
W90-PV10-6M	90	10		20	80	5.8	2.3	

Table 2. AA-WBA/PV mix proportion.

¹ wt. % respect to the total solid; ² wt. % respect to the total liquid; ³ Ms of alkali-activator solution (molar ratio).

The preparation of the pastes started by mechanically stirring the Na₂SiO₃ and NaOH solution (mass ratio of 4:1) in a plastic beaker. The mixed precursors were then added gradually into the alkali-activated solution for 2 min at 568 rpm to promote the dissolution of the reactive phases in the alkali media. Afterwards, the mixture was mixed for 3 min at 760 rpm. The pastes were poured into 25-mm³ moulds that were sealed in plastic bags for three days in a climate chamber at 25 ± 1 °C and with a relative humidity of $95 \pm 5\%$. Finally, the specimens were demoulded after three days and kept in a climate chamber with the same conditions until the experiments (28 days). Nine cubic specimens were prepared for each formulation.

2.3. Test Methods

The hydrolytic stability of AA-WBA/PV was evaluated by using the boiling water test [18], which evaluates the resistance of the binders to degradation in water. One specimen for each formulation was first dried in a desiccator with silica gel to constant weight. The specimen was then placed in boiling water for 20 min, before being dried again in a desiccator to constant weight. Later, visual analysis was conducted to verify the cohesion of the sample. Finally, the sample was weighed to calculate the weight loss percentage.

A selective chemical extraction was carried out to determine the main reaction products formed. The formation of calcium silicate hydrate (C-S-H), calcium aluminosilicate hydrate (C-A-S-H), and sodium aluminosilicate hydrate (N-A-S-H) gels after the alkali activation can be estimated from the calcium and aluminium contents of the precursors [39]. Salicylic acid/methanol (SAM) extraction can be used to determine the formation of the C-S-H and C-A-S-H phases [40]. SAM extraction consisted of mixing 1 g of the binder sample with salicylic acid (6 g) and methanol (40 mL) for 1 h. The resulting solution was then filtered (Whatman filter paper with a 20-µm pore size), and the residual fraction (RF) was washed and dried to constant weight in a desiccator with silica gel. The RF was weighed to calculate the mass dissolved percentage. Another selective chemical extraction test with HCl was performed to determine the formation of the C-S-H, C-A-S-H, and N-A-S-H gels [39]. The extraction process consisted of stirring 1 g of the binder sample with 250 mL of the HCl solution (1:20) for 3 h. Afterwards, the solution was filtered (Whatman filter paper with a 20- μ m pore size), and the weight loss percentage of the washed and dried RF was determined.

XRD analysis of the AA-WBA/PV formulations was performed using a Bragg–Brentano Siemens D-500 powder diffractometer (Siemens, Munich, Germany) with CuKα radiation to identify the main crystalline phases. Fourier transform infrared spectroscopy (FT-IR) spectra of the AA-WBA/PV binders in the attenuated total reflectance (ATR) mode were obtained with a Spectrum Two[™] FT-IR spectrometer from PerkinElmer (PerkinElmer Inc., Waltham, MA, USA). Measurements were performed in the 4000–400 cm⁻¹ range with a 32-scan average and a 4-cm⁻¹ resolution. FT-IR spectra deconvolution of the most representative samples in the 1200–800 cm⁻¹ range was also performed. This range is associated with the symmetric and asymmetric stretching vibrations of the Si-O bonds [41]. The computer software Origin Pro 9 (OriginLab Corporation, Northampton, MA, USA) was used to fit and adjust the shape of the spectra with Gaussian functions, following some of the criteria from the literature [41]. Scanning electron microscopy with energy-dispersive X-ray spectroscopy (SEM-EDS) was used to evaluate the microstructure of the samples using an ESEM FEI Quanta 200 equipment (Thermo Fisher Scientific, Waltham, MA, USA). The samples were cut with a diamond disc cutter and coated with graphite.

Bulk density and open porosity tests were performed following the EN 1936:2006 standard. The compressive strength of the AA-WBA/PV formulations was determined following the UNE-EN 196-1 standard and using an Incotecnic MULTI-R1 device (Matest S.P.A., Bergamo, Italy) equipped with a 20-kN load cell. Three cubic specimens were used in the physical and mechanical tests.

The WBA, PV, and AA-WBA/PV formulations were assessed to determine the leaching of heavy metalloids (As, Ba, Cd, Cr, Cu, Hg, Mo, Pb, Ni, Sb, and Zn) using an ELAN-6000 inductively coupled plasma mass spectrometer (ICP-MS) from PerkinElmer (PerkinElmer Inc., Waltham, MA, USA). Three replicates per sample (WBA, PV, and AA-WBA/PV) were used following the European EN 12457-2 standard. In the case of the AA-WBA/PV binders, the crushed specimens (smaller than 4 mm) obtained after the compressive strength test were used.

3. Results and Discussion

3.1. Hydrolitic Stability Test

The boiling water test demonstrated that all the formulations of the AA-WBA/PV tested were resistant to degradation in water (Figure 4). Although some negligible defects were observed at the edges of the specimens, the visual analysis revealed that all the samples remained dimensionally unaltered. As shown in Figure 4a, a layer of sodium carbonate efflorescence formed on the surface of the AA-WBA/PV specimens, which was removed after the test (Figure 4b). The weight loss percentage (below 1.5% in all cases) also confirmed the hydrolytic stability of the AA-WBA/PV binders, revealing the structural integrity of the samples, probably due to the formation of new reaction products.

3.2. SAM and HCl Extraction

The results from the selective chemical extractions are given in Table 3. The SAM extraction results demonstrated that the OPC paste was mainly composed of the C-S-H gel, as expected, while all the formulations of AA-WBA/PV contained C-S-H and C-A-S-H gels. The concentration of the alkaline activator solution had an effect, since AA-WBA/PV activated with 6 M NaOH solution showed a higher percentage of mass dissolved by the SAM extraction method. This was due to the higher pH of the alkaline activator solution, which increased the Ca content of the formed gel [42]. The SAM extraction results were not conclusive in determining the effect of varying the PV content, since there was no appreciable change in the percentage of mass dissolved by the SAM extraction method among the formulations activated with the same NaOH concentration.



Figure 4. AA-WBA/PV specimens (a) before and (b) after the boiling test.

Table 3. S	Selective	chemical	extraction	results.

Samples	Mass Dissolved by SAM (wt. %)	Mass Dissolved by HCl (wt. %)
OPC paste	89.8	-
WBA powder	5.5	27.1
PV powder	6.5	30.4
W98-PV2-4M	20.5	38.5
W95-PV5-4M	20.2	37.9
W90-PV10-4M	20.4	38.1
W98-PV2-6M	22.8	39.1
W95-PV5-6M	23.3	39.6
W90-PV10-6M	23.1	39.0

The HCl extraction results showed a slight increase in the percentage of mass dissolved for the formulations activated with 6 M NaOH. There was no appreciable difference when varying the PV content, similar to that observed with the SAM extraction. The results on the percentages of mass dissolved for the WBA and PV regarding AA-WBA/PV demonstrated the formation of new reaction products in all the formulations of AA-WBA/PV. However, it is important to highlight that HCl extraction dissolves the main reaction products of AABs (C-S-H, C-A-S-H, and N-A-S-H gels) [39] and the other mineral phases (i.e., carbonate phases) of the precursors and the AA-WBA/PV binders [43]. Therefore, physicochemical characterization is necessary to confirm the formation of these new reaction products.

3.3. Physicochemical Charaterization

The crystalline phases found in the AA-WBA/PV binders are summarized in Table 4. The presence of calcite, cristobalite, corundum, dolomite, gibbsite, and quartz was due to the unreacted WBA and PV. Calcium silicate hydrate as the main C-S-H phase and gismondine [44] and gehlenite [45] as the C-A-S-H phases were detected in all the AA-WBA/PV formulations. The presence of anorthite in the W98PV2 formulations and albite in all the formulations indicated the formation of (C,N)-A-S-H [46] and N-A-S-H [47] gels, respectively. Sodalite, which is associated with a zeolitic product [48,49], was also detected in all the XRD patterns. Kanemite, another typical phase of alkali-silica reaction products [50,51], was identified in the formulations activated with 6 M NaOH. The XRD results are consistent with the SAM and HCl extraction results (Section 3.2) in demonstrating the formation of new reaction products (C-S-H, C-A-S-H, and (C,N)-A-S-H gels).

		Formulations								
Identified Phase	PDF		NaOH 4 M		NaOH 6 M					
		W98PV2	W95PV5	W90PV10	W98PV2	W95PV5	W90PV10			
Albite	01-083-1609	Y	Y	Y	Y	Y	Y			
Calcite	01-072-1937	Y	Y	Y	Y	Y	Y			
Calcium Silicate Hydrate	014-0035	Y	Ν	Ν	Ν	Y	Ν			
Calcium Silicate Hydrate	011-0507		Y	Y	Y	Ν	Y			
Cristobalite	01-082-1479	Y	Y	Y	Y	Y	Y			
Corundum	01-071-1123		Y	Y	Ν	Y	Y			
Diopside	01-071-1067		Y	Ν	Y	Y	Ν			
Dolomite	01-079-1342	Y		Ν	Ν	Ν	Ν			
Gehlenite	01-079-2422	Y	Y	Y	Y	Y	Y			
Gibbsite	01-076-1782	Y	Y	Y	Y	Y	Y			
Gismondine	020-0452	Y	Y	Y	Y	Y	Y			
Kanemite	025-1309		Ν	Ν	Y	Y	Y			
Quartz	01-083-0539	Y	Y	Y	Y	Y	Y			
Sodalite	01-082-1811	Y	Y	Y	Y	Y	Y			

Table 4. Crystalline phases in AA-WBA/PV binders.

Figure 5 shows the results of the FT-IR analysis of the WBA and AA-WBA/PV formulations in the range of 1650–600 cm⁻¹. There is a broad band (1200–900 cm⁻¹) in all the spectra that is associated with the asymmetric T–O (T = Si or Al) stretching mode [41]. The change in the position and shape of this broad band in the AA-WBA/PV spectra regarding that of the WBA indicates alkali activation and the formation of new phases. The displacement of the broad band to higher frequencies in the AA-WBA/PV spectra, when compared to the WBA spectrum, demonstrates the formation of the C-S-H and C-A-S-H phases [52]. The broad band shifts to lower frequencies with increasing NaOH concentration and aluminium in the AA-WBA/PV spectra. This is probably due to the formation of the N-A-S-H phases [53] and the inclusion of aluminium in the C-S-H gel [54]. This agrees with the results from the selective chemical extractions (Section 3.2) and XRD analysis. There is a band at 785 cm⁻¹ in all the spectra corresponding to the quartz contained in the WBA [53]. The other observed peaks are attributed to the stretching vibrations (1405, 1436, and 1483 cm⁻¹) and bending vibrations (875 and 713 cm⁻¹) of calcium carbonates [55].

The deconvoluted FT-IR spectra in the range of 1200–800 cm⁻¹ are shown in Figure 6. The W98PV2-4M and W90PV10-6M samples were selected as they had the lowest and highest NaOH concentration and aluminium content, respectively. The spectra present the same peaks that have slightly displaced to lower frequencies due to increases in the NaOH concentration and PV content. The main narrow band at 1016–1013 cm⁻¹ and the band at 1144–1153 cm⁻¹ are ascribed to the v_3 (Si-O) bridging bond stretching vibrations [56]. The displacement of these bands to lower frequencies for the W90PV10-6M sample indicates a lower degree of polymerization of the silicate chains [41]. The two bands at \approx 900 and \approx 866 cm⁻¹ correspond to Si-O terminal bonds, indicating an incomplete polymerization of the gel [56]. Finally, the narrow peak at 875 cm⁻¹ corresponds to calcium carbonate stretching vibrations (C-O).

Figure 7 depicts the FT-IR spectra of the W98PV2-4M and W90PV10-6M samples before and after the selective chemical extractions. The shift and displacement of the broad band (1009–1013 cm⁻¹) towards a higher frequency (1064 cm⁻¹) indicates the dissolution of the C-S-H, C-A-S-H, and (C,N)-A-S-H phases. The dissolution of these phases produced three characteristic peaks that indicate the presence of silica gel (790, 945, and 1064 cm⁻¹) [57]. HCl extraction completely dissolved the calcium carbonate peaks associated with the stretching vibrations (1405 and 1448 cm⁻¹) and bending vibrations (875 and 713 cm⁻¹). In the case of SAM extraction, some peaks in the spectra are diffused (713 and 1448 cm⁻¹) or remain equal (875 cm⁻¹).



Figure 5. FT-IR spectra of WBA and AA-WBA/PV.



Figure 6. FT-IR deconvoluted spectra of (a) the W98PV2-4M sample and (b) W90PV10-6M sample.



Figure 7. FT-IR spectra after selective chemical extractions: (a) W98PV2-4M sample and (b) W90PV10-6M sample.

SEM micrographs obtained in the backscattered electron (BSE) mode of the W98PV2-4M and W90PV10-6M samples are depicted in Figure 8. There was a substantial difference in the compactness of the samples. The W98PV2-4M sample presented a homogeneous dark greyish compact matrix with some small spherical pores (darkest zones) and unreacted particles. Microcracks could also be observed throughout the sample, indicating drying shrinkage during the curing process [58]. The W90PV10-6M sample presented higher porosity than the W98PV2-4M sample. Increasing the PV content and NaOH concentration in the W90PV10-6M formulation increased the aluminium nitride (AlN) content and alkaline activator concentration, respectively. As mentioned before, the reaction between AlN and NaOH produces ammonia gas, which is mainly responsible for generating the porosity of AA-WBA/PV [38].







Figure 8. SEM images of (a) W98PV2-4M sample and (b) W90PV10-6M sample.

3.4. Physical and Mechanical Properties

The bulk density and open porosity of the AA-WBA/PV binders are shown in Figure 9, which demonstrates the influence of the PV content and NaOH concentration on these properties. As mentioned in Section 3.3, increasing the PV content and NaOH concentration promotes porosity, which implies a decrease in the bulk density. The open porosity curves in Figure 9 also show the porosity-enhancing effect of the PV content and NaOH concentration

when increased, as demonstrated by the pronounced slope for the samples formulated with 6 M NaOH.



Figure 9. Bulk density and open porosity of AA-WBA/PV binders.

Compressive strength (Figure 10) decreased with increasing PV content and NaOH concentration, which agrees with the physical properties of the samples. The substantial difference between the W98PV2-4M and W90PV10-6M samples demonstrated the negative effect of increased porosity on the mechanical properties of the AA-WBA/PV binders.



Figure 10. Compressive strength of AA-WBA/PV binders.

3.5. Environmental Characterization

Leaching tests in deionized water were conducted following the EN 12457-2 standard to simulate the environmental impact of the AA-WBA/PV binders when they are demolished at the end of their useful life. The concentrations of the heavy metals and metalloids leaching from the WBA, PV, and AA-WBA/PV binders, as well as the limits for acceptance in waste landfills [59], are summarized in Table 5. For the WBA, only the Sb concentration exceeded the limit for inert waste. For the PV powder, Mo and Sb concentrations exceeded the limits for inert waste and non-hazardous waste, respectively. The results for the AA-WBA/PV binders varied substantially depending on the heavy metals and metalloids. Mo and Pb concentrations were above the limit for non-hazardous waste. However, the main issue was the high activation of metalloids (As and Sb) in the AA-WBA/PV binders regarding the WBA and PV. Indeed, the leaching concentrations of As and Sb exceeded the limits for acceptance at landfills for non-hazardous waste. The immobilization of these two metalloids is hampered by the high pH environment during the alkali activation process, which contributes to their anionic formation [60]. However, an increase in immobilization efficiency after 18 months of curing has been reported in the literature [61]. Therefore, the immobilization of As and Sb in the AA-WBA/PV matrix is expected to improve with longer curing times comparable to the lifecycle of these materials. The primary and secondary glass contents of the WBA are the main contributors of the metalloids in AA-WBA/PV [31]. Sb and As oxides are used in the glass industry as refining and coloring agents [62] and are mainly found in the coarse fraction of WBA [17]. Furthermore, Sb is also found in PV, because this metal is used in the aluminum industry as a modifier of the eutectic structure and as a grain refiner [63]. Increasing the NaOH concentration affected the leaching of the metalloids from the AA-WBA/PV formulations. The higher the concentration of the alkaline activator solution, the higher the concentration of the alkaline activator solution, the higher the concentration of the leaching metalloids. However, the effect of increasing the PV content was negligible.

Table 5. Leaching concentrations ($mg \cdot kg^{-1}$) in WBA, PV, and AA-WBA/PV binders after leaching tests (EN 12457-2) and limits for acceptance at landfills.

Sample	As	Ba	Cd	Cr	Cu	Hg	Мо	Ni	Pb	Sb	Zn	pН
WBA	0.02	0.25	< 0.01	0.17	0.69	0.01	0.33	0.11	0.01	0.27	0.12	9.54
PV	0.10	0.06	< 0.01	0.01	0.15	< 0.01	2.90	< 0.20	0.01	1.38	0.10	10.03
W98-PV2-4M	2.44	0.14	< 0.01	0.12	0.54	0.04	0.42	< 0.20	0.44	2.82	0.76	11.61
W95-PV5-4M	2.45	0.16	< 0.01	0.14	0.50	0.02	0.50	< 0.20	0.54	2.86	0.71	11.59
W90-PV10-4M	2.34	0.31	< 0.01	0.14	0.55	0.01	0.72	< 0.20	0.49	2.86	0.51	11.48
W98-PV2-6M	2.78	0.15	< 0.01	0.05	0.53	0.01	0.52	< 0.20	0.55	3.15	0.54	11.63
W95-PV5-6M	2.77	0.19	< 0.01	0.18	0.81	0.06	0.50	< 0.20	0.52	3.22	0.68	11.57
W90-PV10-6M	2.68	0.22	< 0.01	0.24	0.34	0.02	0.70	< 0.20	0.50	3.18	0.80	11.57
¹ Inert waste (mg·kg ⁻¹)	0.5	20	0.04	0.5	2	0.01	0.5	0.4	0.5	0.06	4	
¹ Non-hazardous waste (mg∙kg ⁻¹)	2	100	1	10	50	0.2	10	10	10	0.7	50	
¹ Hazardous waste (mg∙kg ⁻¹)	25	300	5	70	100	2	30	40	50	5	200	

¹ limit for acceptance in landfills [59].

4. Conclusions

The use of WBA and PV in the formulation of AABs can lead to a low-carbon and zero-waste manufacturing of cement. This study demonstrated the potential of the coarse fraction of WBA and PV as silica-rich and alumina-rich precursors, respectively. The AA-WBA/PV binders remain stable after immersion in boiling water due to the formation of new phases. Selective chemical extractions, XRD analysis, and FT-IR analysis revealed the presence of C-S-H, C-A-S-H, and/or (N,C)-A-S-H gels as the main reaction products formed in the AA-WBA/PV binders. The NaOH concentration and PV content influenced the mechanical and physical properties of the binders. Increasing the NaOH concentration and the PV content increased the formation of the reaction products as well as porosity. Increasing the PV content, however, reduced the compressive strength of the binders. These results reflect the versatility of PV when applied to enhance mechanical properties or used as an aerating agent to improve thermal conductivity. Finally, the environmental impact of the binders was assessed with leaching tests, which revealed that a high pH of the alkaline activator solution increased the leaching of metalloids from AA-WBA/PV. Considering that the main goal of this study was to obtain AABs with good mechanical properties, W98PV2-4M is the optimal formulation, with the lowest metalloid leaching potential.

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