

Asymptotic analysis of the Gunn effect with realistic boundary conditions

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A general asymptotic analysis of the Gunn effect in n -type GaAs under general boundary conditions for metal-semiconductor contacts is presented. Depending on the parameter values in the boundary condition of the injecting contact, different types of waves mediate the Gunn effect. The periodic current oscillation typical of the Gunn effect may be caused by moving charge-monopole accumulation or depletion layers, or by low- or high-field charge-dipole solitary waves. A new instability caused by multiple shedding of (low-field) dipole waves is found. In all cases the shape of the current oscillation is described in detail: we show the direct relationship between its major features (maxima, minima, plateaus, etc.) and several critical currents (which depend on the values of the contact parameters). Our results open the possibility of measuring contact parameters from the analysis of the shape of the current oscillation. [S1063-651X(97)04708-9]

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I. INTRODUCTION

The Gunn effect appears in many semiconductor samples presenting negative differential resistance and subject to voltage bias conditions [1–7]. It consists of a periodic shedding of pulses of the electric-field at the injecting contact, which then progress and are annihilated at the receiving contact. As a result there appears a periodic oscillation of the current through a passive external circuit attached to the semiconductor. Under different conditions, the current self-sustained oscillation may be caused by the motion of charge accumulation layers (charge monopoles) [2], not by the usual electric-field pulses which are charge dipoles. Most of the experiments on the Gunn effect in different materials take place in samples with attached planar contacts, so that the wave motion may be safely assumed to be one dimensional. Despite the vast literature on the Gunn effect, it is surprising that many basic questions remain poorly understood. For example, given a description of the charge transport in the bulk semiconductor (say at the level of drift-diffusion and rate equations), which are the proper boundary conditions for given contacts and how they affect the self-sustained current oscillations. The first question has been addressed in a companion paper, Ref. [8], while the second will be answered here.

Until recently, when confronted with the Gunn effect, theorists resorted to computer simulations of more or less complicated models (which were supposed to reflect the physics of a given semiconductor), and would then explain qualitatively their numerics. Special solutions valid for infinite semiconductors at constant current bias conditions [3], or extrapolations of Kroemer's nonlinear (NL) criterion [9] were often used to interpret the simulation results. This left the processes of generation and annihilation of domains at the contacts (and in fact it also left out the dynamics of wave

fronts and pulses) outside theoretical considerations. Concerning asymptotic descriptions of the Gunn effect which delve deeper than just numerical simulations of drift-diffusion models, some progress has been made recently [10–13]. These works propose asymptotic descriptions of the Gunn effect, exploiting the fact that this effect is seen most clearly in semiconductors having a large value of the product of sample length times doping (basically a dimensionless length). The role of the NL product in the analysis of the Gunn instability was already discovered by Kroemer [2], and exploited to study the linear stability (small signal analysis) of stationary solutions by many authors [3]. It was recognized only much later that in the limit of large dimensionless length (NL product) it is possible to describe asymptotically both the onset [16] and the fully developed Gunn instability [10]. In this asymptotic limit the processes of repeatedly generating a new wave (a charge monopole or dipole domain) at the injecting contact, the motion of the wave and its annihilation at the receiving contact may be well separated. Then they can be analyzed and combined to fully describe the Gunn effect. In particular, the effect of contacts on these processes and in determining the shape of the current oscillation can be clearly stated. In this paper we use our asymptotic theory to study Kroemer's model for n -type GaAs under boundary conditions (BC's) corresponding to ideal metal-semiconductor (MS) contacts. We find that these BC's give rise to a multivalued control current-field characteristic at the injecting contact. The asymptotic analysis shows that the Gunn effect can be mediated by both charge monopole or dipole domains according to the values of the contact parameters. Shedding of new charge dipole waves from the injecting contact is adiabatic, in clear distinction with what happens if the control characteristic of the contact is single valued [12,13]. In the latter case (analyzed for a p -type Ge model in Ref. [12]) the charge dipole pulses

are created very rapidly at the injecting contact, and they advance and grow simultaneously (see also [10]), whereas for multivalued control characteristic the boundary layer at the injecting contact grows adiabatically to a much greater size before a new pulse can be shed. These facts may appreciably determine the shape of the current oscillations. Our analysis could be extended to more complex models also displaying the Gunn effect [12–14]. Depending on the values of the parameters characterizing the injecting contact and of the dc voltage bias, we find Gunn oscillations mediated by charge accumulation and depletion monopole wave fronts, and high- and low-field charge dipole domains. We also find narrow regions in the parameter space where multiple shedding of dipole domains at the injecting contact occurs. We have thus found a characterization of all possible dynamic behaviors which an ideal metal-semiconductor contact would give rise to in the Kroemer model for the Gunn effect. This opens the possibility of extracting information about the contacts from the analysis of the Gunn oscillations themselves, a subject of considerable interest for applied researchers.

The rest of the paper is as follows. In Sec. II we present Kroemer's model and the boundary conditions for metal-semiconductor contacts discussed in the companion paper [8]. In Sec. III we present our asymptotic analysis of Kroemer's model, and find that different types of Gunn effect are possible according to the values of the bias and of certain dimensionless parameters appearing in the BC's, i_0 and α_0 : charge monopoles (moving charge depletion and accumulation layers), high- and low-field solitary waves (charge dipoles), and multiple (low-field) charge dipoles are predicted and confirmed by numerical simulations. Section V contains our conclusions whereas the Appendixes are devoted to different technical matters related to the main text.

II. KROEMER'S MODEL AND BC'S FOR METAL-SEMICONDUCTOR CONTACTS

The unipolar drift-diffusion model for the Gunn effect proposed by Kroemer [2,15] is generally accepted to provide a rather complete description of the main features of this effect. In the dimensionless units described in Ref. [8], Kroemer's model is

$$\frac{\partial E}{\partial t} + v(E) \left(\frac{\partial E}{\partial x} + 1 \right) - \delta \frac{\partial^2 E}{\partial x^2} = J, \quad (1)$$

$$\frac{1}{L} \int_0^L E(x,t) dx = \phi. \quad (2)$$

Equation (1) is Ampère's law, which says that the sum of the displacement current and drift-diffusion current is equal to the total current density $J(t)$. It can be obtained by differentiating the Poisson equation $\partial E/\partial x = n - 1$, with respect to time, substituting the charge continuity equation $\partial n/\partial t + \partial j(x,t)/\partial x = 0$ [the electron current density is of the drift-diffusion type: $j(x,t) = nv(E) - \delta \partial n/\partial x$], and then integrating the result with respect to x . The electron velocity is assumed to be N shaped. For specific numerical calculations we shall use Kroemer's curve [15]

$$v(E) = E \frac{1 + BE^4}{1 + E^4} \quad (3)$$

(it has a maximum $v_M > 0$ at $E_M > 0$ followed by a minimum $0 < v_m < v_M$ at $E_m > E_M$), and assume that the electron diffusivity δ is constant. The dc bias ϕ is the average electric field on the semiconductor sample. Equations (1) and (2) need to be solved with an appropriate initial field profile $E(x,0)$ and subject to the corresponding b.c.'s. For an ideal MS, the following mixed boundary conditions were derived in Ref. [8]:

$$\frac{\partial E}{\partial x}(0,t) = \alpha_0 \left(i_0 - J(t) + \frac{\partial E}{\partial t}(0,t) \right), \quad (4)$$

$$\frac{\partial E}{\partial x}(L,t) = \alpha_L \left(i_L + J(t) - \frac{\partial E}{\partial t}(L,t) \right), \quad (5)$$

where i_i and α_i ($i=0,L$) are dimensionless parameters which are a combination of the semiconductor effective density of states, contact barrier height, Richardson's constant, doping, and temperature (see Ref. [8]). In what follows, i_i will be assumed to be positive because physically interesting phenomena (including the usual Gunn effect mediated by high-field domains) are observed for these values of i_i (see the phase diagram in Ref. [8]).

For typical n -type GaAs data, $\delta \ll 1$ and $L \gg 1$ [10]. In this limit, we shall find approximate solutions to the initial boundary value problem Eqs. (1)–(5) for $E(x,t)$ and $J(t)$. Strictly speaking, the simple asymptotic description that follows holds in the limit $L \rightarrow \infty$, even when $\delta = O(1)$ [13]. Assuming $\delta \ll 1$ just simplifies the description of the traveling waves of the electric field in the semiconductor through the use of characteristic equations and shock waves [10,17,18]. For example, it is shown in Appendix A (by using the method of characteristics) that the boundary condition Eq. (4) implies that the electric field at the injecting contact, $E(0,t) = E_0(t)$, obeys the following equation:

$$\frac{dE_0}{dt} = J - j_c(E_0), \quad (6)$$

$$j_c(E) = \frac{(1 + \alpha_0 i_0)v(E)}{1 + \alpha_0 v(E)}. \quad (7)$$

These expressions constitute a Dirichlet boundary condition for the electric field which contains the same information as the mixed condition Eq. (4). The contact curve, $j_c(E)$, presents two extrema, a minimum $j_{cm} = j_c(E_m)$ and a maximum $j_{cM} = j_c(E_M)$, at the same field values as the electron velocity curve $v(E)$. $j_c(E)$ tends to $j_0^{\text{sat}} = \alpha_0^{-1} + i_0$ for high electric fields. As we shall see below, during most of an oscillation period, $j_c(E_0) \sim J$, and this expression yields a multivalued contact-characteristic curve relating the field at the injecting contact to the actual value of the current density.

To take advantage of the large-length limit, we will use the following rescaled time and length,

$$\epsilon = \frac{1}{L}, \quad s = \frac{t}{L}, \quad y = \frac{x}{L}. \quad (8)$$

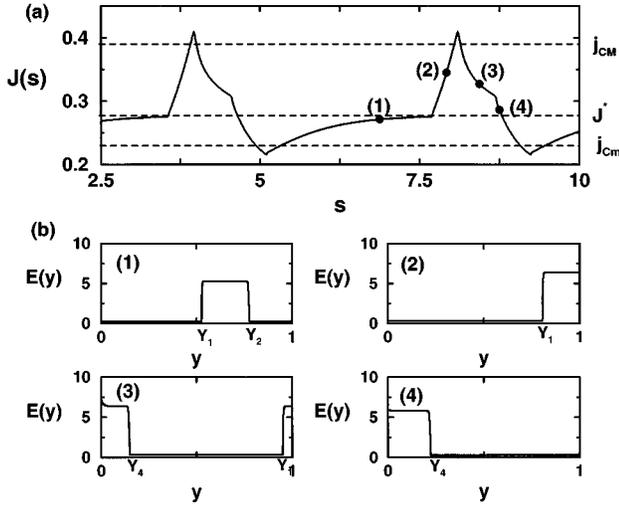


FIG. 1. Gunn effect mediated by dipole solitary waves. (a) Dimensionless current density $J(s)$. Parameter values are $L=800$, $i_0=0.3$, $\alpha_0=3.6$, and $\phi=1.5$, for which $v_m < j_{cm} < J^* < j_{cm} < v_M$. The minimum and maximum values of $J(s)$ correspond to $j_{cm}=0.23$ and $j_{cm}=0.31$, respectively, whereas the plateau at intermediate values of $J(s)$ corresponds to the solution of $c_+(J)=c_-(J)$ and $J^*=0.28$. (b) The corresponding electric-field profiles $E(y,s)$ evaluated at the times marked in (a) of this figure.

Then Eqs. (1) and (2) become

$$J - v(E) = \epsilon \left(\frac{\partial E}{\partial s} + v(E) \frac{\partial E}{\partial y} \right) - \delta \epsilon^2 \frac{\partial^2 E}{\partial y^2}, \quad (9)$$

$$\int_0^1 E(y,s) dy = \phi. \quad (10)$$

Notice that the boundary condition (6) becomes

$$J - j_c(E) = \epsilon \frac{dE_0}{ds} \quad (11)$$

in the limit $\delta \ll 1$.

III. ASYMPTOTICS OF THE GUNN EFFECT

In a previous paper [8] we analyzed the stationary solutions of Kroemer's model with metal-semiconductor contacts, and discussed their stability. No stable stationary solution is expected for certain ranges of bias and the cathode contact parameters i_0 and α_0 . In these circumstances, the Gunn effect mediated by either moving charge monopoles or dipoles might appear. A rich phenomenology of propagating waves and current oscillations has been numerically observed for these parameter ranges. Among them, we have observed both high- (Figs. 1 and 2) and low- (Fig. 3) field solitary waves (moving charge dipoles), multiple low-field dipoles (Fig. 4), moving charge accumulation (Fig. 5) and charge depletion monopoles (Fig. 6). In Ref. [8], we identified the critical currents determining which type of waves mediate the current oscillation (in the limit $\delta \ll 1$). They are related to the boundary conditions in the following way:

(i) If $j_{cm} > v_M$, the Gunn effect is mediated by moving

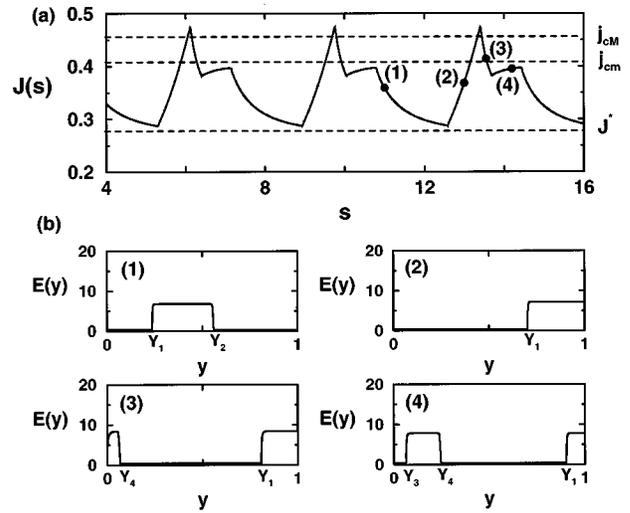


FIG. 2. Gunn effect mediated by dipole solitary waves. (a) Dimensionless current density $J(s)$. Parameter values are $L=1000$, $i_0=0.45$, $\alpha_0=30$, and $\phi=2.4$, for which $v_m < J^* < j_{cm} < j_{cm} < v_M$. The maximum value of $J(s)$ corresponds to $j_{cm}=0.46$, whereas the plateau at bottom of $J(s)$ corresponds to the solution of $c_+(J)=c_-(J)$ and $J^*=0.28$. The value of j_{cm} is 0.41. (b) The corresponding electric-field profiles $E(y,s)$ evaluated at the times marked in (a) of this figure.

charge accumulation monopoles (j_{cm} and v_M are the local maxima of the contact current and electron velocity curves, both reached at $E=E_M$).

(ii) If $j_{cm} < v_m$, and $j_0^{\text{sat}} > v_m$, the Gunn effect is mediated by moving charge depletion monopoles [j_{cm} and v_m are the local minima of the contact current and electron velocity curves, both reached at $E=E_m$, and $j_0^{\text{sat}} = \alpha_0^{-1} + i_0$ is the value at which $j_c(E)$ saturates at high electric fields].

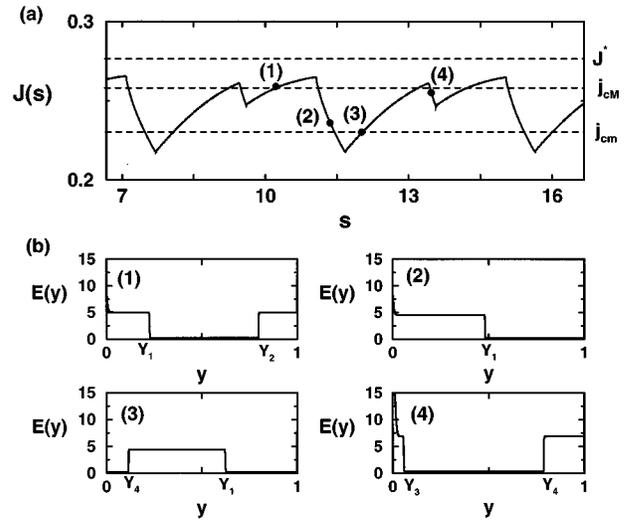


FIG. 3. Gunn effect mediated by low-field dipole solitary waves. (a) Dimensionless current density $J(s)$. Parameter values are $L=1500$, $i_0=0.24$, $\alpha_0=30$, and $\phi=2.3$, for which $v_m < j_{cm} < j_{cm} < J^* < v_M$, where $J^*=0.28$ corresponds to the solution of $c_+(J)=c_-(J)$. The values of $j_{cm}=0.26$ and $j_{cm}=0.23$. (b) The corresponding electric-field profiles $E(y,s)$ evaluated at the times marked in (a) of this figure.

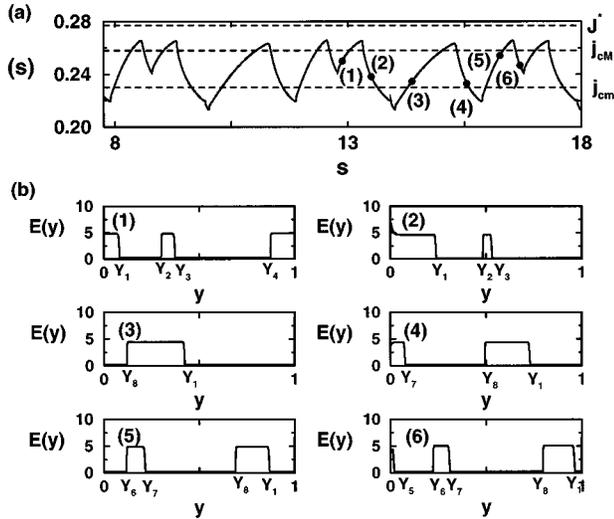


FIG. 4. Multiple shedding of low-field domains. The parameter values are $L=800$, $i_0=0.24$, $\alpha_0=30$, and $\phi=1.5$. The critical currents are $J^*=0.28$, $j_{cM}=0.26$, and $j_{cm}=0.23$. (a) Dimensionless current density $J(s)$. (b) The corresponding electric-field profiles $E(y,s)$ evaluated at the times marked in (a) of this figure. Two pulses are formed during each period. The second shed pulse reaches and overtakes the first one.

(iii) If $v_m < j_{cm} < j_{cM} < v_M$, moving charge dipoles mediate the Gunn effect (see Ref. [8] for more details).

As shown in the figures, there are several stages in each period of the current oscillation corresponding to the processes of generation, propagation, and annihilation of electric-field domains. Each stage has its own time and space scales, and hence the oscillation can be suitably described by

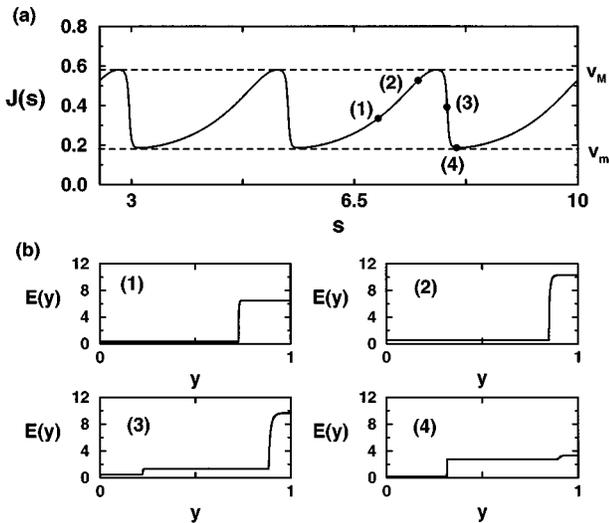


FIG. 5. Gunn effect mediated by monopole wave fronts (moving accumulation charge monopoles). (a) Dimensionless current density $J(s)$. Parameter values are $L=800$, $i_0=1.35$, $\alpha_0=0.8$, and $\phi=2$, for which $j_{cm} < v_m$ and $j_0^{\text{sat}} > v_m$, where j_0^{sat} corresponds to the saturation current $j_0^{\text{sat}} = \alpha^{-1} + i_0$. The maximum and minimum values of the oscillation correspond to the maximum and minimum values of the $v(E)$ curve, $v_M=0.58$ and $v_m=0.18$, respectively. (b) The corresponding electric field profiles $E(y,s)$ evaluated at the times marked in (a) of this figure.

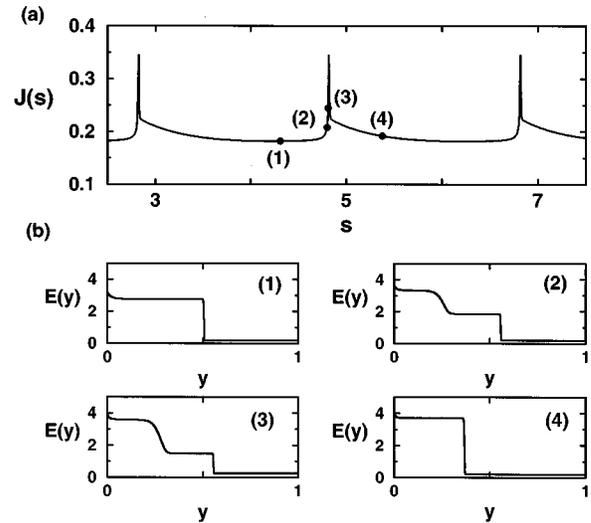


FIG. 6. Gunn effect mediated by monopole wave fronts (moving depletion charge monopoles). (a) Dimensionless current density $J(s)$. Parameter values are $L=800$, $i_0=0.135$, $\alpha_0=0.8$, and $\phi=1.5$, for which $j_{cM} > v_M$. (b) The corresponding electric field profiles $E(y,s)$ evaluated at the times marked in (a) of this figure.

means of a matched asymptotic analysis. For instance, the annihilation of wave fronts takes place on a fast time scale compared to that governing wave-front propagation. Thus on the time scale of wave-front propagation, the annihilation of wave fronts is a quasi-instantaneous process during which the time derivative of the current density changes appreciably while the current itself, $J(s)$, does not change. On the other hand, the generation of fronts takes place adiabatically on a much slower time scale comparable to wave-front propagation. In this stage both $J(s)$ and its derivative change appreciably. This is quite different from the fast generation of fronts and pulses observed for other types of boundary conditions [12].

As long as these different processes take place on different time and space scales, there are different stages of the oscillation which can be analyzed separately. This happens for certain bias ranges. We shall then construct the approximate electric field and current density solutions by means of matched asymptotic expansions. A detailed description of a period of the current oscillation will then be obtained. For other bias values, several processes occur almost simultaneously (e.g., the annihilation of a wave front may occur during the process of detachment of another wave front from the injecting boundary layer for low bias values). This complicates the asymptotic description without adding much to our physical understanding, so that we will omit the details.

Note that in the limit $\epsilon = 1/L \ll 1$, the solutions of Eqs. (9) and (10) are piecewise constant: on most of the y interval, E is equal to one or another of the zeros of $v(E) - J$ (notice that this equation may have three zeros which we denote by $E_1 < E_2 < E_3$), separated by transition layers that connect them. At $y=0$ and 1 there are boundary layers (quasistationary most of the time), which we call *injecting and receiving layers*, respectively. It can be seen that the propagation of fronts turns out to be a quasistationary process, while the generation is not. Thus two different asymptotic approaches will be used: one for the description of the quasistationary

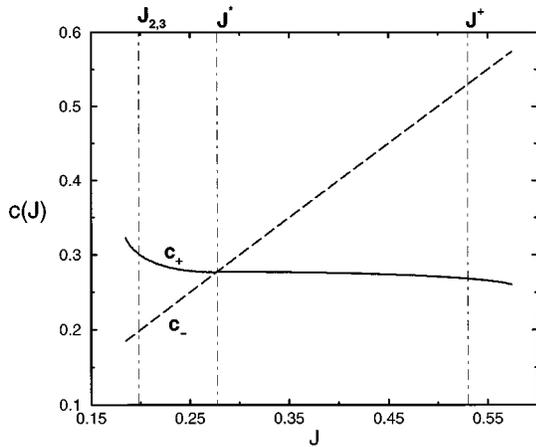


FIG. 7. Velocities c_+ and c_- of the heteroclinic wave fronts as functions of the current density. Notice that the lines intersect at $J^* = 0.28$. We have also marked the currents $J^{\dagger} = J_{2,1} = 0.53$ at which $2c_+ = c_-$ and $J_{2,3} = 0.20$ at which $2c_+ = 3c_-$.

propagation of fronts, and the other for their (nonquasistationary) generation.

A. Quasistationary propagation of wave fronts

In this section we will present the asymptotics of the quasistationary propagation of wave fronts, and of the corresponding time evolution of the density current. Wave fronts are moving transition layers connecting regions of the sample where the electric field is spatially uniform. In order to describe their quasistationary propagation we will proceed as follows. We assume that $E(y,s)$ is either $E_1(J)$ or $E_3(J)$ outside boundary layers and wave fronts. Let the wave front located at $y = Y(s)$ move with velocity $c = dY/ds$. For each value of J , the wave front advances with speed $c = c_+(J)$, if it connects $E = E_1(J)$ [$y < Y(s)$] to $E_3(J)$ [$y > Y(s)$], or with speed $c = c_-(J)$, if it connects $E = E_3(J)$ [$y < Y(s)$] to $E_1(J)$ [$y > Y(s)$]. To find the inner structure of a wave front and its speed, we introduce a coordinate $\xi = \epsilon^{-1}[y - Y_i(s)]$ moving with the wave front. Then we need to solve the following problem for the equation,

$$\frac{dE}{d\xi} = F, \quad \frac{dF}{d\xi} = \frac{[v(E) - c]F + v(E) - J}{\delta}, \quad (12)$$

obtained from Eq. (9): Find the unique value $c = c_+(J)$ [$c_-(J)$] such that there is a solution of (12) with $E(-\infty) = E_1(J)$ and $E(\infty) = E_3(J)$ [$E(-\infty) = E_3(J)$ and $E(\infty) = E_1(J)$]. The solution of this problem will provide both the speed and inner structure of the wave front. In terms of the phase plane (12), the previous problem is equivalent to find $c = c_+(J)$, so that there is a heteroclinic orbit connecting the saddle point $(E_1, 0)$ to the saddle point $(E_3, 0)$ with $F > 0$. Similarly $c = c_-(J)$ corresponds to a heteroclinic orbit connecting $(E_3, 0)$ to $(E_1, 0)$ with $F < 0$. The functions $c_{\pm}(J)$ for our model are depicted in Fig. 7. Note that they intersect when $J = J^*$, given by

$$J^* = \frac{1}{E_3 - E_1} \int_{E_1}^{E_3} v(E) dE, \quad c_{\pm} = J^*, \quad (13)$$

the so-called equal-areas rule [4].

In the limit $\delta \ll 1$, we can obtain explicit expressions for $c_{\pm}(J)$ and for the corresponding wave fronts, as we now recall [10,18]. The wave front (moving depletion layer) joining $(E_3(J), 0)$ and $(E_1(J), 0)$ may be approximated by the exact solution of Eq. (12),

$$E(\xi) = -\xi, \quad F(\xi) = -1, \quad c_-(J) = J, \quad (14)$$

which holds for any value of δ plus two corner layers of width $O(\sqrt{\delta})$ (on the ξ scale) at $\xi = \pm(E_3 - E_1)/2$. See Ref. [18] for an explicit calculation. The width of this wave front on the ξ length scale is $(E_3 - E_1) + O(\sqrt{\delta})$, which yields $y - Y_i(s) = O(\epsilon)$ on the large length scale. The velocity of this wave front is $c_-(J) = J$.

The other wave fronts (moving accumulation layers) can be constructed by matched asymptotic expansions in the limit $\delta \ll 1$, and their velocities $c_+(J)$ and shapes depend on whether J is larger or smaller than J^* . These wave fronts are composed of a shock wave joining two field values E_- and E_+ (at least one of them should be equal to E_i , $i = 1$ and 3) plus a tail region which moves rigidly with the same velocity as the shock [10]. The inner structure of the shock wave (for very small but not zero δ) can be a quite complicated triple-deck set of boundary layers [18]. Let $V(E_+, E_-)$ be the velocity of the shock wave given by the equal-areas rule [10,17,18]

$$V(E_+, E_-) = \frac{1}{E_+ - E_-} \int_{E_-}^{E_+} v(E) dE. \quad (15)$$

We now have the following [10]:

(1) If $J \in (v_m, J^*)$, $E_+ = E_3(J)$, whereas E_- is calculated as a function of J by imposing the condition that the tail region to the left of the shock wave moves rigidly with it:

$$V(E_3, E_-) = v(E_-). \quad (16)$$

Solving Eqs. (15) and (16) simultaneously (with $E_+ = E_3$), we find both E_- and $c_+ = v(E_-) > J$ as functions of J . To the left of the shock wave (in the tail region) the field satisfies the (approximate) boundary value problem

$$[v(E) - c_+(J)] \frac{dE}{d\xi} = J - v(E), \quad \xi < 0,$$

$$E(-\infty) = E_1(J), \quad E(0) = E_-(J). \quad (17)$$

(2) If $J \in (J^*, v_M)$, $E_- = E_1(J)$, whereas E_+ is calculated as a function of J by imposing the condition that the tail region to the right of the shock wave moves rigidly with it:

$$V(E_+, E_1) = v(E_+). \quad (18)$$

Simultaneously solving Eqs. (15) and (18) (with $E_- = E_1$), we find both E_+ and $c_+ = v(E_+) < J$ as functions of J . To the right of the shock wave (in the tail region) the field satisfies the (approximate) boundary value problem

$$[v(E) - c_+(J)] \frac{dE}{d\xi} = J - v(E), \quad \xi > 0,$$

$$E(0) = E_+(J), \quad E(\infty) = E_3(J). \quad (19)$$

At $J = J^*$ we have $E_- = E_1$, $E_+ = E_3$, and $c_+ = J^*$. It is not hard to prove that $c_+(J)$ is a decreasing function. The functions $c_{\pm}(J)$ are depicted in Fig. 7.

Notice that the inner structure of the shock wave has width $O(\sqrt{\delta})$ on the ξ scale, while the total width of the wave front is $O(1)$ on the ξ scale and $O(\epsilon)$ on the y scale. In the limit $\delta \ll 1$, the structure of the wave fronts is thus one sided: the wave front is a discontinuity preceded or followed by a tail region.

In conclusion, the propagation of a single wave front can be described by giving the position $Y(s)$ and velocity $c_{\pm}(J(s))$ of the front and the values of the electric field on its left- and right-hand sides, $E_i(J(s))$. When more than a single wave front are comoving inside the sample, the same description applies to each of them. All of the magnitudes involved in this description depend on time s only through the instantaneous value of the current $J(s)$. This fact, together with the fact that the voltage must remain constant all the time, can be used to derive a simple closed equation describing the time evolution of the current density during the propagation stages. As an example of this result, let us consider the case a single propagating dipole (two fronts) [see Fig. 1(b1)]. In this case, neglecting transition and boundary layers, we have $E(y, s) = E_1(J(s))$ for $0 < y < Y_1(s)$ and $Y_2(s) < y < 1$ and $E(y, s) = E_3(J(s))$ for $Y_1 > y > Y_2(s)$. For the voltage we have

$$\phi = E_1(J(s)) + [E_3(J(s)) - E_1(J(s))][Y_2(s) - Y_1(s)] + O(\epsilon). \quad (20)$$

By using the fact that the voltage is fixed, we can obtain an equation for $J(s)$ by differentiating the bias condition (20) with respect to s . By noting that

$$v(E_i) = J \Rightarrow \frac{dE_i}{dJ} = \frac{1}{v'(E_i(J))},$$

$$\frac{dY_1}{ds} = c_+(J), \quad \frac{dY_2}{ds} = c_-(J), \quad (21)$$

the following simple closed equations for the current are obtained:

$$\frac{dJ}{ds} = A(J) [c_+(J) - c_-(J)], \quad (22)$$

$$A(J) = \frac{(E_3 - E_1)^2}{\frac{\phi - E_1}{v'_3} + \frac{E_3 - \phi}{v'_1}} > 0, \quad (23)$$

where $v'_i \equiv v'(E_i(J))$ ($i = 1$ and 3). This equation for J holds as long as the electric-field profile consists of a single propagating dipole. A simple analysis of Eq. (22) demonstrates that J tends to J^* [for which $c_+(J) = c_-(J)$] exponentially fast, starting from a certain value of the current $J(0)$. This

result explains, in particular, why the solitary wave responsible for the Gunn effect moves at an approximately constant velocity $c_{\pm} = J^*$ and a constant current far from the contacts.

A similar procedure can be applied to derive the corresponding closed equation for the current when different types of propagating domains are present. In general we will have n_+ fronts moving at velocity c_+ and n_- moving at c_- , with $|n_+ - n_-| = 0, 1$. For these cases the current evolves following the equation

$$\frac{dJ}{ds} = A(J)[n_+ c_+(J) - n_- c_-(J)]. \quad (24)$$

As before, this equation holds as long as the propagating profile consists of n_+ fronts propagating at c_+ and n_- at c_- . Two typical cases can be considered in analyzing Eq. (24): (i) either n_+ or n_- are equal to zero; and (ii) $n_{\pm} \neq 0$, and both numbers are different from zero. In the first case, we have either

$$\frac{dJ}{ds} = A(J)c_+(J), \quad n_+ = 1, n_- = 0, \quad (25)$$

or

$$\frac{dJ}{ds} = -A(J)c_-(J), \quad n_+ = 0, n_- = 1, \quad (26)$$

and the current will either increase [Eq. (25)], or decrease [Eq. (26)], with time. In the second situation, the current follows the general relation Eq. (24) with the corresponding values of n_{\pm} : the current evolves toward the fixed point $J = J_{n_+, n_-}$, satisfying $n_+ c_+(J_{n_+, n_-}) - n_- c_-(J_{n_+, n_-}) = 0$, when such a point exists. A particular example of this behavior was explained above for $J_{1,1} = J^*$.

These results describe the quasistationary propagation of fronts and the corresponding time evolution of the current density during these stages. We will use them to interpret the results of the numerical simulations.

B. Generation of fronts

As mentioned above, for our b.c.'s an appreciable part of a period of the current oscillation may be spent generating new fronts nonadiabatically. Fronts of dipole domains are generated at the cathode, whereas monopole wave fronts appear somewhere in the middle of the sample. In what follows, we will focus on the description of dipole domains. Monopole wave fronts have recently been described in detail elsewhere [11].

A simple rule concerning generation of dipole domains can be formulated: when the current density $J(s)$ crosses the maximum (minimum) of the contact curve j_{cM} (j_{cm}), a front moving with speed c_- (c_+) starts being formed *when its generation is compatible with the field value at the bulk after the injecting contact*.

Let us now show why the previous rule holds. Suppose that the current reaches adiabatically one of the critical values mentioned above, let us say j_{cM} , in the slow time scale s . Then the field at $x = 0$, given by Eq. (6), can no longer be quasistationary, and the injecting layer becomes unstable and starts shedding a new solitary wave. Let s_1 now be the earliest time at which $J = j_{cM}$, and the boundary field $E_0 = E_M$. After this time, the disturbances $J - j_{cM} = O(\epsilon)$ cause E_0 to evolve to the third branch of $j_c(E)$ on a time of

order $s - s_1 = O(\epsilon)$. The field in the injecting layer, in turn, increases until a moving wave front moving with speed c_- is formed. To describe this process, we adapt ideas developed for the analysis of the trap-dominated Gunn effect in p -type Ge [12] to the present situation. An important difference is that the sharp increase in the contact field E_0 helps to create the new wave front, but a new pulse is not shed on the fast time scale $\sigma = (s - s_1)/\epsilon$: after the wave front is created, the contact field varies on the third branch of $j_c(E)$ and the current has to decrease slowly [according to Eq. (24), on the s time scale] until E_0 can jump back to values on the first branch of $j_c(E)$ when $J = j_{cm}$.

To leading order, the field in the injecting layer solves the following semi-infinite problem, whose derivation can be found in Appendix B:

$$\frac{\partial E}{\partial \sigma} + v(E) \left(\frac{\partial E}{\partial x} + 1 \right) = J, \quad x > 0, \quad -\infty < \sigma < +\infty, \quad (27)$$

$$E(0, \sigma) = E_0(\sigma), \quad (28)$$

where E_0 solves Eq. (6) with $J = j_{cm} + \epsilon J^{(1)}(\sigma)$ and $J^{(1)}(\sigma)$ is given by

$$\left(\frac{\partial}{\partial \sigma} + \beta \right) [J^{(1)} - h'(\sigma) - \alpha h] = -\gamma h, \quad (29)$$

where $h(\sigma)$ is

$$\begin{aligned} h(\sigma) = & (E_3 - E_1)c_+ \sigma - \int_0^\infty [E(x, \sigma) - E_1] dx \\ & - \int_{-\infty}^0 [E(\xi) - E_1(j_{cm})] d\xi \\ & - \int_0^\infty [E(\xi) - E_3(j_{cm})] d\xi, \end{aligned} \quad (30)$$

and formulas for the positive constants α , β , and γ may be found below, in Eqs. (B10). The function $h(\sigma)$ is the area lost due to the motion of the old front during the time σ minus the instantaneous excess area under the injecting layer minus the constant excess area under the old wave front at $Y = Y_1(s_1)$ [that is, under the heteroclinic orbit connecting $(E_1(j_{cm}), 0)$ and $(E_3(j_{cm}), 0)$].

As $\sigma \rightarrow -\infty$, we have to impose the following matching condition on an appropriate overlap domain:

$$E(x, \sigma) - E_{\text{stat}}(x; J(s)) \ll 1, \quad (31)$$

as $\sigma \rightarrow -\infty$ and $s \rightarrow s_1 -$. Here $E_{\text{stat}}(x; J(s))$ is the quasistationary injecting layer solution of Eq. (12) with $c = 0$ such that $E_{\text{stat}}(0; J(s))$ satisfies Eq. (4) and $E_{\text{stat}}(\infty; J(s)) = E_1(J(s))$ for $s < s_1$, $J(s_1) = j_{cm}$. Notice that the term $\epsilon J^{(1)}(\sigma)$ is needed so as to avoid that the solution of this problem stay indefinitely in the quasistationary field $E_{\text{stat}}(x; J(s))$.

The solution of the previous semi-infinite problem reveals the growth of the field at the contact and inside the injecting layer until (i) E_0 becomes $E_{c3}(j_{cm})$ [$E_{c1}(J) < E_{c2}(J) < E_{c3}(J)$ are the three possible solutions of $J = j_c(E)$], (ii) $E(x, \sigma)$ increases to $E_3(j_{cm})$ as x increases from $x = 0$, and

then (iii) has the structure of a wave front connecting $E_3(j_{cm})$ to $E_1(j_{cm})$. This wave front advances with velocity $c_-(j_{cm})$. The formation of a front when J crosses j_{cm} can be explained similarly.

C. Putting the pieces together

In the two previous subsections, we presented the basic features of an asymptotic description of the Gunn effect, namely, quasistationary front propagation and the generation of new fronts. Now we are in a position to put all the pieces together, and describe a full period of current oscillation. We shall distinguish three cases: high-field dipoles, low-field dipoles, and monopoles.

1. Dynamics of high-field dipoles

High-field dipole domains have been observed to appear when $v_m < j_{cm}$ and $J^* < j_{cm} < v_M$. Then depending on the value of j_{cm} with respect to J^* , and of j_{cm} with respect to $J^\dagger \equiv J_{2,1}$, different situations may occur.

Let us start by considering the case $v_m < j_{cm} < J^* < j_{cm} < J^\dagger < v_M$. This situation corresponds to the propagation of high-field dipole domains as shown in Fig. 1. We will assume the initial electric-field configuration to correspond to a single propagating high-field domain [Fig. 1(b1)]. This configuration corresponds to $n_+ = 1$ and $n_- = 1$, and hence the current satisfies Eq. (22), evolving from an initial value $J(0) \in (j_{cm}, J^*)$, toward the fixed point $J^* = J_{1,1}$. After a certain time, the wave front located at Y_2 reaches the end of the sample and disappears, producing an abrupt change in the time derivative of the current. We have a new stage with $n_+ = 1$ and $n_- = 0$, Fig. 1(b2), governed by Eq. (25). Its solution increases until it surpasses the value j_{cm} . At this point the injecting layer becomes unstable and starts shedding a new front. The formation dynamics was explained in detail in Sec. II. Then a new slowly varying stage begins. There are two leftover wave fronts: the old one located at $y = Y_1(s)$ [which advances toward $y = 1$ with speed $c_+(J)$]; and a new one located at $y = Y_4(s)$, moving with speed $c_-(J)$, and leaving behind a quasistationary field $E_3(J)$ [see Fig. 1(b3)]. Again, the field configuration corresponds to $n_+ = n_- = 1$, with $J(s)$ following Eq. (22), and decreasing exponentially fast toward J^* . Before J reaches J^* , the front located at Y_1 reaches the end of the sample and disappears, thereby producing a new abrupt change in the time derivative of the current density. Then only the recently formed front [located at $Y_4(s)$] is present on the sample [Fig. 1(b4)], which corresponds to $n_+ = 0$ and $n_- = 1$. $J(s)$ decreases according to Eq. (26) until the minimum of the contact curve, $J = j_{cm}$, is reached. After that, a front moving with speed c_+ is generated. The charge dipole wave thus created evolves adiabatically, and the current density is described again by Eq. (22), Fig. 1(b1). We have come back to the initial situation, and one period of the current oscillation has been completed.

It is worth noting that by means of this analysis some of the most relevant features of the current oscillations, such as the maximum and minimum currents J_{max} and J_{min} , have been identified with quantities related to the contact parameters $J_{\text{max}} \approx j_{cm}$ and $J_{\text{min}} \approx j_{cm}$, then opening the possibility of determining the values of contact parameters from the

analysis of the current oscillations.

Other situations involving dipole domains have been numerically identified. They are described by the same type of analysis. In what follows only the more relevant features of these situations will be considered. Let us now assume $v_m < J^* < j_{cm} < j_{cM} < J^\dagger < v_M$. This case again corresponds to high-field solitary waves (dipole domains, see Fig. 2), but the current oscillations have a different shape. The three first stages of the oscillation, Figs. 2(b1), 2(b2), and 2(b3), correspond to the propagation of a single dipole, annihilation of a front, and generation of new one. They are similar to the stages described above. Now, however, after the new front has been formed, Fig. 2(b3), and the current is decreasing toward J^* , J reaches the critical current, j_{cm} (because $J^* < j_{cm}$). A new front moving with speed c_+ is then created. After the formation process has finished, we have a configuration with two fronts moving at c_+ and one at c_- , that is, with $n_+ = 2$ and $n_- = 1$ [Fig. 2(b4)]. Hence the current satisfies [see Eq. (24)]

$$\frac{dJ}{ds} = A(J) [2c_+(J) - c_-(J)], \quad (32)$$

and it starts increasing again, trying to reach $J_{1,2} = J^\dagger$. Before this value may be attained, the old front, located at Y_1 , arrives at the receiving contact and disappears. We again obtain Eqs. (22) and (23), and recover the initial situation. Thus a full period of the Gunn oscillation is again completed.

There are other possible situations for propagating high-field domains, but we have not found them in our numerical simulations with the curve $v(E)$ considered in the present work. For example, in the second case we have described above, $v_m < J^* < j_{cm} < j_{cM} < J^\dagger < v_M$, after the formation of the new front [Fig. 2(b4)], the current density could have reached the value J^\dagger before the old front located at Y_1 had arrived at the receiving contact. In such a situation, a new front moving at c_- could be formed, giving rise to an electric-field configuration with $n_+ = n_- = 2$. In this configuration the current would decrease again to $J_{2,2} = J_{1,1} = J^*$. We would then have a more complicated situation with two pulses and the dying wave front simultaneously present in the sample. Proceeding in a similar way, we could therefore observe simultaneous coexistence of several pulses for appropriate ranges of parameters. This situation (multiple shedding of high-field domains) has been numerically observed in other models [12,13].

2. Dynamics of low-field dipoles

Low-field dipole domains appear when $v_m < j_{cm} < j_{cM} < J^*$. Depending on the value of the applied bias, single (high-bias values) or multiple (low-bias values) propagating low-field domains are obtained (see Figs. 3 and 4).

Let us start by considering the case of single propagating low-field dipole domains, Fig. 3. We consider an initial field configuration having a low-field domain far from the contacts. Then there is a wave front located at Y_1 , moving with speed c_- , and a wave front located at $Y_2 > Y_1$, moving with speed c_+ , that is, $n_+ = n_- = 1$ [Fig. 3(b1)], and $J(0) \in (j_{cm}, J^*)$. The current increases toward J^* according to Eq. (22), until $Y_2 = 1$. Then J starts satisfying Eq. (26) [cor-

responding to $n_+ = 0$ and $n_- = 1$; see Fig. 3(b2)], and it decreases until the value j_{cm} is reached. After this occurs, a new front (moving at speed c_+) is created, while the old wave front $Y_1 < 1$. We have a stage described by Eq. (22) with $n_+ = n_- = 1$ [see Fig. 3(b3)], during which J increases past j_{cM} ($j_{cM} < J^*$). Then a new front moving with speed c_- starts to be created. At the same time, the old front located at Y_1 reaches the end of the sample, giving rise to a complex stage in which the nonstationary effects cannot be neglected [Fig. 3(b4)]. After that stage, we recover the first situation [Fig. 3(b1)], and a complete period of the oscillation has been described.

Let us now consider an example of multiple propagating low-field dipole domains (Fig. 4). As we mentioned above, these appear for small bias values. The asymptotic analysis of this case is more complicated because there are new stages (fusion of two wave fronts inside the sample) whose detailed description is outside the scope of this paper. Let us start with the configuration shown in Fig. 4(b1), for which two low-field domains coexist. This configuration corresponds to $n_+ = n_- = 2$. Following Eq. (24), the current will evolve according to

$$\frac{dJ}{ds} = A(J) [2c_+(J) - 2c_-(J)], \quad (33)$$

thereby increasing toward $J_{2,2} = J^*$. Before this value can be reached, the front located at Y_4 reaches the end of the sample. The resulting configuration [Fig. 4(b2)] has now $n_+ = 1$ and $n_- = 2$, and the current decreases according to

$$\frac{dJ}{ds} = A(J) [c_+(J) - 2c_-(J)]. \quad (34)$$

If the curve $v(E)$ were such that the fixed point of Eq. (34) existed, the current would tend to such a value. For our choice of $v(E)$, this fixed point does not exist (see Fig. 7), and therefore the current decreases all the time. During this process j_{cm} will be crossed. According to our previous considerations, a new front moving at speed c_+ should then be formed. However, this does not occur because melting of the fronts Y_2 and Y_3 starts after Y_4 reaches $y = 1$. This melting process seems to inhibit the creation of new wave fronts until it is completed, which happens for $J < j_{cm}$. Then a new front moving at speed c_+ is rapidly created, and we have a stage, with $n_+ = n_- = 1$ [Fig. 4(b3)], described by Eq. (22). The current increases until $J = j_{cM}$, at which time a front moving at speed c_- appears at $y = 0$ [Fig. 4(b4)]. Then the current decreases following Eq. (34) until $J = j_{cm}$. Another front moving at speed c_+ is then formed. We have now $n_+ = n_- = 2$ [Fig. 4(b5)], and J increases according to Eq. (22). When $J > j_{cM}$, a front moving with speed c_- is created at $y = 0$, so that $n_+ = 2$, $n_- = 3$; see Fig. 4(b6). Now the current decreases towards $J_{2,3}$ according to the equation

$$\frac{dJ}{ds} = A(J) [2c_+(J) - 3c_-(J)]. \quad (35)$$

This stage lasts until $Y_1 = 1$, at which time we are back at the first stage, Fig. 4(b1), having completed a full period of the

oscillation. More complicated examples of multiple low-field domains exist, and they could be described similarly.

3. Dynamics of charge monopoles

When $j_{cM} > v_M$, or when $j_{cm} < v_m$ and $j_{sat} > v_m$, the Gunn effect is mediated by wave fronts which are charge monopoles. The case $j_{cM} > v_M$, corresponds to moving accumulation layers, (Fig. 5), while moving depletion layers are observed for $j_{cm} < v_m$ and $j_{sat} > v_m$ (Fig. 6). Kroemer [15] discovered numerically the Gunn effect mediated by charge accumulation monopoles for boundary conditions corresponding to the control characteristics, while its asymptotic analysis (for $B \ll 1$) was performed many years later [10]. Recently a Gunn effect mediated by charge accumulation monopoles has been used to describe self-sustained oscillations of the current in GaAs/AlAs superlattices [21] in the limit of weakly coupled, low doped, long superlattices [11].

The complete asymptotic analysis found in Ref. [11] can be used to describe the present situation after a few simple changes are made. First of all, the equal-areas rule in the case of the superlattice refers to $1/v(E)$, not $v(E)$ [22]. The second important change is that of the injecting boundary condition in the description of the birth of a new monopole: instead of a rigid Neumann boundary condition $\partial E(0,t)/\partial x = c$, we should use Eq. (4). These two changes can be implemented without difficulty, and the details will be omitted. An important difference from the Gunn effect mediated by dipole solitary waves is that the amplitude of the current oscillations is larger (its largest value is approximately $v_M - v_m$ for the charge accumulation monopoles, and $j_{cM} - j_{cm}$ for the dipoles). The monopoles “probe” the full region of negative slope of $v(E)$, while the dipoles “probe” a smaller region.

IV. CONCLUSIONS

We have performed an asymptotic and numerical analysis of the Gunn effect in n -type GaAs under general boundary conditions for metal-semiconductor contacts. We have shown that the Gunn effect is mediated by (i) moving depletion charge monopoles, (ii) moving accumulation charge monopoles, (iii) high-field dipole solitary waves, or (iv) low-field dipole solitary waves, according to whether the critical contact currents $j_{cM} = j_c(E_M)$, $j_{cm} = j_c(E_m)$, and j_0^{sat} are (i) $j_{cm} < v_m$ and $j_0^{sat} > v_m$, (ii) $j_{cM} > v_M$, (iii) $v_m < j_{cm}$ and $J^* < j_{cM} < v_M$, or (iv) $v_m < j_{cm} < j_{cM} < J^*$, in dimensionless units [v_m and v_M are the minimum and maximum values of the electron drift velocity $v(E)$, $E > 0$, and J^* is the solution of $c_+(J) = c_-(J)$]. Some of these results are well known for boundary conditions given by Kroemer’s control characteristic. In addition, we have shown that there are new instability mechanisms consisting of multiple generation of (low-field) charge dipole solitary waves in the region near the injecting contact if j_{cM} is close enough to J^* , and the dimensionless length is large enough. In each case we have been able to describe in detail the shape of the current oscillation, identifying some of its main features (maxima, minima, plateaus, etc.) with critical currents appearing in our model, among them the contact currents j_{cm} and j_{cM} . This result opens the possibility of determining contact parameters by

means of the analysis of the shape of the current oscillation. Our results might be of use in the analysis of self-sustained current oscillations in weakly coupled n -doped superlattices [21], once the role of contacts and the boundary conditions they generate are understood in these systems. Besides this, our results are not restricted to the particular model of the Gunn effect studied here, but seem to hold for a general class of models, supporting the idea of the “universality” of the Gunn effect [13].

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APPENDIX A: NONSTATIONARY FIELD AT THE INJECTING CONTACT

We shall now prove that the field $E_0(t)$ at the contact $x=0$ obeys the equation

$$\frac{dE_0}{dt} = J - j_c(E_0). \quad (\text{A1})$$

This can be seen from the method of characteristics applied to Eq. (1) with $\delta=0$ and the boundary condition Eq. (4). The characteristic equations are

$$\frac{dE}{dt} = J - v(E), \quad (\text{A2})$$

$$\frac{dx}{dt} = v(E), \quad (\text{A3})$$

to be solved with the conditions

$$E(\tau; \tau) = E_0(\tau), \quad (\text{A4})$$

$$x(\tau; \tau) = 0. \quad (\text{A5})$$

Clearly,

$$\frac{dE_0}{d\tau} = \frac{\partial E}{\partial t}(\tau; \tau) + \frac{\partial E}{\partial \tau}(\tau; \tau) = J - v(E_0) + \frac{\partial E}{\partial \tau}(\tau; \tau). \quad (\text{A6})$$

The last term in this equation can be obtained from the boundary condition Eq. (4) as follows. From the solution of Eqs. (A3) and (A5), we obtain $(\partial x / \partial \tau)(\tau; \tau) = -v(E_0(\tau))$. Then the boundary condition Eq. (4) yields

$$\begin{aligned} \frac{\partial E}{\partial \tau}(\tau; \tau) &= \frac{\partial E}{\partial x}(0, \tau) \frac{\partial x}{\partial \tau}(\tau; \tau) \\ &= -v(E_0(\tau)) \alpha_0 \left(i_0 - J + \frac{dE_0}{d\tau} \right). \end{aligned} \quad (\text{A7})$$

Insertion of Eq. (A7) into Eq. (A6) yields Eq. (A1) (with $\tau=t$).

**APPENDIX B: CALCULATION OF THE CURRENT
 $J^{(1)}(\sigma)$ DURING THE SHEDDING STAGE**

To obtain the equations governing the shedding stages, we need to keep terms of order ϵ in our calculations, as indicated in Ref. [12]. The outer (bulk) expansion is

$$E = E_i^{(0)}(\sigma) + \epsilon E_i^{(1)}(\sigma) + O(\epsilon^2), \quad (\text{B1})$$

$$J = J^{(0)}(\sigma) + \epsilon J^{(1)}(\sigma) + O(\epsilon^2), \quad (\text{B2})$$

where $i = 1$ if $0 < y < Y_1(s_1)$ and $i = 3$ if $Y_1(s_1) < y < 1$. Then $E_i^{(0)}$ and $J^{(0)}$ solve

$$\frac{\partial E_i^{(0)}}{\partial \sigma} + v(E_i^{(0)}) = J^{(0)}(\sigma), \quad (\text{B3})$$

$$\phi = E_1^{(0)} + [E_3^{(0)} - E_1^{(0)}][1 - Y_1(s_1)]. \quad (\text{B4})$$

We can obtain easily $E_3^{(0)}$ and $J^{(0)}$ from these equations:

$$E_3^{(0)} = \frac{\phi - E_1^{(0)} Y_1(s_1)}{1 - Y_1(s_1)}, \quad (\text{B5})$$

$$J^{(0)}(\sigma) = v(E_1^{(0)}) Y_1(s_1) + v(E_3^{(0)}) [1 - Y_1(s_1)]. \quad (\text{B6})$$

Now $E_1^{(0)}$ follows from Eq. (B3) and these two last equations. These equations should be solved with the matching conditions that $E_i^{(0)} \rightarrow E_i(j_{cM})$ ($i = 1$ and 3) and $J^{(0)} \rightarrow j_{cM}$ as $\sigma \rightarrow -\infty$. These problems have the solutions $J = j_{cM}$ and $E_i^{(0)} = E_i(j_{cM})$. Thus we expect that the current density does not depart substantially from j_{cM} as $\epsilon \rightarrow 0$.

The $O(\epsilon)$ corrections $E_i^{(1)}(\sigma)$ obey the equations

$$\Theta_i E_i^{(1)} \equiv \frac{\partial E_i^{(1)}}{\partial \sigma} + v'(E_i) E_i^{(1)} = J^{(1)}(\sigma), \quad (\text{B7})$$

which immediately follow from Eq. (9). To find $J^{(1)}$ we proceed as follows. First of all, we write the bias condition Eq. (10) including terms of order ϵ in the approximation of the electric field and the current density:

$$\begin{aligned} \phi &= E_1(j_{cM}) + [E_3(j_{cM}) - E_1(j_{cM})][1 - Y_1(s_1)] \\ &+ \epsilon \left\{ E_1^{(1)} + [E_3^{(1)} - E_1^{(1)}][1 - Y_1(s_1)] \right. \\ &- [E_3(j_{cM}) - E_1(j_{cM})]c_+ \sigma + \int_0^\infty [E(x, \sigma) \\ &- E_1(j_{cM})]dx + \int_{-\infty}^0 [E(\xi) - E_1(j_{cM})]d\xi \\ &\left. + \int_0^\infty [E(\xi) - E_3(j_{cM})]d\xi \right\} + O(\epsilon^2). \end{aligned} \quad (\text{B8})$$

Here $E(\xi)$ is the field inside the wave front at Y_1 , and $E(x, \sigma)$ is the field in the injecting layer. Since $\phi = E_1(j_{cM}) + [E_3(j_{cM}) - E_1(j_{cM})][1 - Y_1(s_1)]$, we obtain

$$E_1^{(1)} + [E_3^{(1)} - E_1^{(1)}][1 - Y_1(s_1)] = h(\sigma), \quad (\text{B9})$$

where $h(\sigma)$ is given by Eq. (30).

We now obtain the first-order differential equation (29) for $J^{(1)}(\sigma)$ by applying the operator $\Theta_1 \Theta_3$ to both sides of Eq. (B9) and then using Eq. (B7):

$$\left(\frac{\partial}{\partial \sigma} + \beta \right) [J^{(1)} - h'(\sigma) - \alpha h] = -\gamma h,$$

where the coefficients α , β , and γ are

$$\begin{aligned} \alpha &= v'_1 Y_1(s_1) + [1 - Y_1(s_1)]v'_3, \\ \beta &= v'_3 Y_1(s_1) + [1 - Y_1(s_1)]v'_1, \\ \gamma &= Y_1(s_1)[1 - Y_1(s_1)](v'_1 - v'_3)^2. \end{aligned} \quad (\text{B10})$$

All functions of J in these equations are calculated at $J = j_{cM}$. Solving this equation we obtain the following function:

$$J^{(1)}(\sigma) = h'(\sigma) + \alpha h(\sigma) - \gamma \int_{-\infty}^\sigma e^{-\beta(\sigma-t)} h(t) dt. \quad (\text{B11})$$

The only missing function is the field at the injecting boundary layer. This field profile is the solution of the semi-infinite problem Eqs. (27)–(31), with $J(\sigma; \epsilon) = j_{cM} + \epsilon J^{(1)}(\sigma)$ given by Eq. (B11). We can write Eq. (B11) in another form that suggests a more transparent interpretation:

$$\begin{aligned} J^{(1)}(\sigma) &= \frac{\alpha}{\beta} \left\{ J'(s_1)(\sigma - \sigma_0) - I'(\sigma) - \int_0^\infty [\alpha I'(\sigma - \sigma') \right. \\ &\left. + v'_1 v'_3 I(\sigma - \sigma')] e^{-\beta \sigma'} d\sigma' \right\}, \end{aligned} \quad (\text{B12})$$

$$I(\sigma) = \frac{\beta}{\alpha} \int_0^\infty [E(x, \sigma) - E_1] dx, \quad (\text{B13})$$

$$\begin{aligned} \sigma_0 &= - \frac{v'_3 Y_1(s_1) + v'_1 [1 - Y_1(s_1)]}{v'_1 v'_3 \beta} + \{ [E_3(j_{cM}) \\ &- E_1(j_{cM})]c_+ \}^{-1} \left\{ \int_{-\infty}^0 [E(\xi) - E_1(j_{cM})]d\xi \right. \\ &\left. + \int_0^\infty [E(\xi) - E_3(j_{cM})]d\xi \right\}. \end{aligned} \quad (\text{B14})$$

The terms on the right-hand side of Eq. (B12) clearly display the balance between the area lost by the motion of the old wave front at $Y_1(s)$ and the excess area under the injecting layer. $J^{(1)}(\sigma)$ increases linearly with σ until the excess area under the injecting layer increases with σ at least linearly.

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