

1 **Ultra-uniform MIL-88B(Fe)/Fe₃S₄ hybrids engineered by partial**
2 **sulfidation to boost catalysis in electro-Fenton treatment of**
3 **micropollutants: Experimental and mechanistic insights**

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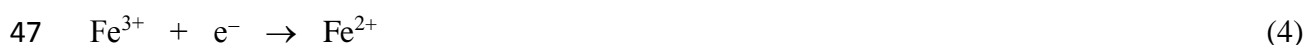
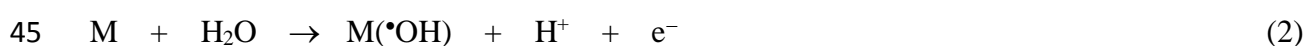
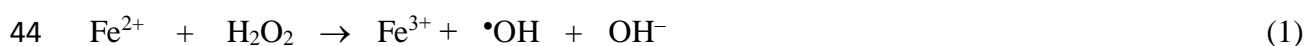
17 **Abstract**

18 Fe-based metal-organic frameworks are promising catalysts for water treatment, although their
19 viability is hampered by the slow regeneration of active Fe(II) sites. A facile sulfidation
20 strategy is proposed to boost the catalytic activity of MIL-88B(Fe) in heterogeneous
21 electro-Fenton (HEF) treatment of organic micropollutants at mild pH. The synthesized
22 MIL-88B(Fe)/Fe₃S₄ hybrids possessed numerous and durable unsaturated iron sites, acting the
23 S²⁻ atoms as electron donors that enhanced the Fe(II) recycling. The sulfidated catalyst
24 outperformed the MIL-88B(Fe), as evidenced by the 7-fold faster degradation of antibiotic
25 trimethoprim by HEF and the fast destruction of micropollutants in urban wastewater. The
26 hybrid catalyst was reused, obtaining >90% drug removal after four runs and, additionally, its
27 inherent magnetism facilitated the post-treatment recovery. Electrochemical tests and DFT
28 calculations provided mechanistic insights to explain the enhanced catalysis, suggesting that the
29 accelerated Fe(III)/Fe(II) cycling and the enhanced mass transport and electron transfer
30 accounted for the efficient trimethoprim degradation.

31 *Keywords:* Heterogeneous electro-Fenton; Metal-organic framework; Fe(II) regeneration;
32 Pharmaceutical pollution; Water treatment

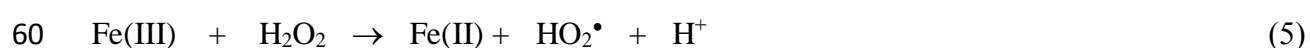
33 1. Introduction

34 In the last decade, electro-Fenton (EF) has become the most popular among the so-called
35 electrochemical advanced oxidation processes (EAOPs) for the remediation of wastewater
36 containing organic micropollutants like pharmaceuticals, owing to the efficient production of
37 free and highly active hydroxyl radicals ($\bullet\text{OH}$, $E^\circ = 2.80 \text{ V/SHE}$) via Fenton's reaction (1) [1-3].
38 In EF, the oxidation is empowered by the simultaneous production of adsorbed $\bullet\text{OH}$ on the
39 anode from reaction (2) [4]. The utilization of carbonaceous cathodes enables massive in-situ
40 generation of H_2O_2 through the 2-electron oxygen reduction reaction (3), a distinct feature as
41 compared to conventional Fenton process that allows minimizing the negative aspects associated
42 to the industrial H_2O_2 supply chain [3,5,6]. Moreover, the continuous Fe^{3+} reduction from
43 reaction (4) at the cathode maintains the catalytic cycle [7,8].



48 Nonetheless, the implementation of conventional homogeneous EF at large scale is
49 currently limited by the need of a strict control of solution pH (optimum at ~ 3) and the gradual
50 deposition of iron mud [9]. The development of heterogeneous electro-Fenton (HEF) process
51 based on the employment of suspended solid catalysts to replace soluble Fe^{2+} salts has mitigate
52 these problems, although new challenges have emerged: (i) irreversible loss of metal active
53 sites due to leaching; (ii) slow regeneration of unsaturated Fe(II) sites because reaction (4)

54 becomes ineffective; (iii) reduced number of exposed active centers towards H₂O₂ and
55 pollutants, since most of them are embedded inside the 3D structure; and (iv) particle
56 aggregation and deactivation, which limits their recyclability [1,4,10]. H₂O₂ may act as an
57 electron donor to regenerate Fe(II) sites via Fenton-like reaction (5), but this is quite inefficient
58 due to the extremely slow reaction kinetics ($k = 0.001-0.01 \text{ M}^{-1} \text{ s}^{-1} \ll k = 63 \text{ M}^{-1} \text{ s}^{-1}$ for reaction
59 (1)), eventually causing a drastic decay in the EF performance [11].



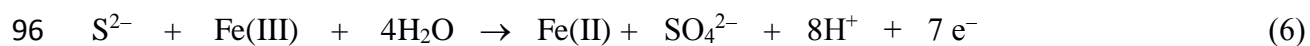
61 The design of highly porous catalysts accelerates the mass transport of H₂O₂ and pollutants,
62 but also raises the risk of deactivation, leading to low recyclability of catalysts [12-14].
63 Therefore, breaking the activity-stability trade-off for high performance HEF is still a
64 conundrum to unravel.

65 Fe-based metal organic frameworks (Fe-MOFs) have been receiving major attention as a
66 new class of catalysts for HEF due to their unique features, arising from a facile synthesis that
67 yields ultraporous and highly tunable structures [15,16]. Among them, MIL-88B(Fe),
68 synthesized by assembling 1,4-benzenedicarboxylic acid ligands and trimeric iron nodes, led to
69 an efficient removal of organic pollutants by HEF, being 10-30-fold quicker than that with
70 simple iron-based catalysts (e.g., iron oxides) [17,18]. The well-developed open pores of
71 MIL-88B(Fe) favor the mass transport of both H₂O₂ and organics to the accessible unsaturated
72 iron active sites, which allows the fast activation of the adsorbed H₂O₂ to yield •OH.
73 Furthermore, the strong coordination of the iron centers minimizes the iron leaching [19,20].
74 However, an excessive binding of iron centers to organic linkers is detrimental, since it reduces

75 the amount of free active sites for H₂O₂ adsorption and activation. It has been shown that the
76 coordinatively unsaturated iron sites in MIL-88B(Fe) are rather scarce [21], which adds to the
77 slow Fe(II) regeneration, negatively affecting the HEF performance [19,22].

78 It is thus evident that accelerating the Fe(III)-to-Fe(II) conversion and multiplying the
79 presence of durable unsaturated iron sites are key tasks to enhance the catalytic performance of
80 Fe-MOFs. For this, a first strategy is based on UV/Vis photoirradiation to create electrons at
81 the conduction band of the catalyst, which can be captured by Fe(III), although the efficiency
82 depends on the quantum yield [23]. Alternatively, bimetallic MOFs with partial substitution of
83 iron nodes by other transition metals promote the Fe(II) regeneration via direct electron transfer
84 [24]. Third, the introduction of electrophilic functionalities (e.g., -NH₂) into MIL-88B(Fe)
85 decreases the electron density of iron centers, favoring their reduced form, although such
86 specific ligands may be too expensive [21]. Vacuum activation of MIL-88B(Fe) at 150-250 °C
87 has also been proposed as an alternative approach [19]. On this basis, the quest for facile and
88 cost-effective routes for the synthesis of improved Fe-MOFs catalysts has drawn attention.

89 Recently, it has been shown that sulfur-doped iron materials accelerate the Fe(III)-to-Fe(II)
90 conversion in non-electrochemical systems [25]. The hybrid molecular orbitals of S-Fe possess
91 larger expansion room, which eases the orbital overlapping between iron sites and H₂O₂,
92 thereby enhancing the electron transfer from H₂O₂ to Fe(III) required for reaction (5) [22].
93 Additionally, the unsaturated S atoms can act as electron donors for efficient Fe(III) reduction;
94 for example, up to 7 moles of electrons can be supplied to Fe(III) upon equimolar conversion of
95 S₂²⁻ into SO₄²⁻ (reaction (6)), being more efficient than Fenton-like reaction (5) [10,12].



97 Iron sulfides as Fenton catalyst experienced a boom in recent years, but they still suffer
98 from low water stability and extremely high iron leaching [10,26]. MIL-100(Fe)-derived Fe₃S₄
99 exhibited superior catalytic activity for photo-Fenton degradation of sulfonamide antibiotics
100 [27]. Du et al. prepared an S-modified MIL-53(Fe) by calcination of a mixture of MIL-53(Fe)
101 with S, proven to be an efficient EF catalyst due to the increased amount of Fe(II) centers.
102 S-doped Fe-MOFs might thus become a suitable choice in EF, although the rational design and
103 the involved mechanistic aspects merit deeper investigation [28].

104 This study constitutes the first attempt to synthesize the ultra-uniform MIL-88B(Fe)/Fe₃S₄
105 hybrids via a facile sulfurization, followed by their application in the HEF treatment of
106 trimethoprim (TMP), selected as target pollutant because it is one of the most commonly
107 prescribed antibiotics for the treatment of bacterial infections. TMP has been frequently
108 detected in surface water, municipal sewage and hospital effluents at ng L⁻¹ - μg L⁻¹ level [29].
109 The effect of sulfidation conditions on the coordination and physicochemical properties of the
110 hybrids, as well as on the catalyst activity was systematically evaluated. Then, the influence of
111 critical factors (e.g., initial pH, catalyst dosage and current density), the viability of various
112 micropollutants degradation in urban wastewater and the catalyst reusability in HEF were
113 studied in detail. Finally, the intrinsic mechanism, including the Fe(III)/Fe(II) redox cycling,
114 the role of S species, and the H₂O₂ adsorption and activation is proposed based on the catalyst
115 characterization and density functional theory (DFT) results.

116 2. Experimental

117 2.1. Chemicals

118 Trimethoprim, naproxen, bisphenol A, ciprofloxacin and 2,4-dichlorophenol were
119 purchased from Sigma-Aldrich and Merck. Sodium sulfate, sodium hydroxide pellets and
120 concentrated sulfuric acid were purchased from Merck. $\text{FeCl}_3 \cdot 6\text{H}_2\text{O}$, *p*-phthalic acid (H_2BDC),
121 dimethylformamide (DMF) and thioacetamide (TAA) from Sigma-Aldrich were employed for
122 the synthesis of the MIL-88B(Fe)/ Fe_3S_4 hybrids. Analytical grade TiOSO_4 used for H_2O_2
123 determination and 1,10-phenantroline monohydrate needed for determining the leached iron
124 concentration were acquired from Merck. Organic solvents of HPLC grade and all the other
125 chemicals were supplied by Sigma-Aldrich and Merck. The urban wastewater for selected trials
126 was collected from the secondary effluent of a wastewater treatment facility located near
127 Chongqing, being immediately preserved at 4 °C to keep constant its main properties: 4.6 mg L⁻¹
128 TOC, 15.9 mg L⁻¹ COD and 12.5 mg L⁻¹ $\text{NH}_4\text{-N}$. In all other cases, the solutions were prepared
129 with water of resistivity greater than 18.2 MΩ cm, obtained from a Millipore Milli-Q system.

130 2.2. Catalyst synthesis

131 The route for synthesis of MIL-88B(Fe)/ Fe_3S_4 hybrids is schematized in Fig. 1a.
132 MIL-88B(Fe) was first prepared following a typical solvothermal methodology. $\text{FeCl}_3 \cdot 6\text{H}_2\text{O}$
133 and H_2BDC (10 mmol of each) were dissolved in 50 mL DMF to form a homogeneous
134 solution. Then, 4 mL of 2 M NaOH solution were added dropwise under vigorous stirring. The
135 as-obtained yellow mixed solution was transferred into a 75 mL Teflon-lined stainless steel
136 autoclave and heated at 100 °C for 12 h. Once cooled down naturally, the resulting powder was

137 collected by centrifugation and repeatedly rinsed with ultrapure water and ethanol. The final
138 MIL-88B(Fe) was dried overnight in a vacuum drying oven at 60 °C.

139 To prepare the MIL-88B(Fe)/Fe₃S₄ hybrids, 200 mg MIL-88B(Fe) were suspended in 50
140 mL ethanol solution, then a certain amount of TAA was added as sulfidation reagent and the
141 mixture was sonicated for 20 min to ensure homogeneity. The solution was sealed in the
142 Teflon-lined autoclave to conduct solvothermal reaction at 150 °C for 3 h. Once cooled down,
143 the final black solid product was collected by centrifugation, washed exhaustively with
144 ultrapure water and ethanol, and dried overnight in a vacuum drying oven at 60 °C. The product
145 was named as S-MIL-88B-3h-*x* (where *x* denotes the mass ratio of TAA to MIL-88B(Fe), i.e.,
146 0.5:1, 1:1, 2:1, 3:1 and 4:1). Similarly, the catalysts prepared at different hydrothermal
147 treatment time under the TAA/MIL-88B(Fe) ratio of 3 was named as S-MIL-88B-*y*h-3 (where
148 *y* denotes the treatment time, i.e., 1, 2, 3 and 4 h).

149 2.3. Catalyst characterization

150 The morphology of the catalyst was observed by high-resolution transmission electron
151 microscopy (HRTEM) using a FEI TF20 microscope that was operated at 200 kV. The
152 microscope was coupled to an energy dispersive X-ray (EDX) detector for mapping acquisition.
153 For X-ray diffraction (XRD) analysis, an X-ray powder diffractometer (Rigaku SmartLab) was
154 employed, using Cu K_{α1} radiation ($\lambda = 1.5406 \text{ \AA}$) and operating at 40 kV and 20 mA. X-ray
155 photoelectron spectroscopy (XPS) measurements for the elucidation of the chemical states were
156 obtained in an ultrahigh vacuum spectrometer equipped with a VSW Class WA hemispherical
157 electron analyzer (Thermo Scientific K-Alpha spectrometer). Fourier transform-infrared

158 (FT-IR) spectra were collected using a Thermo Scientific Nicolet iS20 FTIR spectrometer, at
159 room temperature. The specific surface area of the catalysts was obtained with the Brunauer–
160 Emmett–Teller (BET) analyzer, and the particle size distribution was determined by dynamic
161 light scattering (DLS) using a Malvern Zetasizer Nano ZS90 laser diffraction particle size
162 analyzer. The magnetization characterization was carried out on a LakeShore7404 vibrating
163 sample magnetometer (VSM). Electrochemical impedance spectroscopy (EIS) and Tafel
164 polarization were performed using a CHI 760E electrochemical workstation. The details are
165 described in Text S1 of Supplementary Material (SM).

166 The structural modelling and DFT calculations were carried out with the Vienna Ab initio
167 simulation package (VASP). The exchange-correlation interaction was described by generalized
168 gradient approximation of Perdew-Burke-Ernzerhof (GGA-PBE). The projector
169 augmented-wave (PAW) method was employed to treat interactions between ion cores and
170 valence electrons. The plane-wave cut-off energy was fixed to 450 eV. During the relaxation, the
171 Brillouin zone was sampled by $2 \times 2 \times 1$ K-point grid. And the vacuum slab was set up to 20 Å.

172 *2.4. Electrochemical systems and analytical procedures*

173 The electrolytic trials to evaluate the degradation performance were performed in a
174 single-chamber glass cell containing 160 mL of 0.050 M Na₂SO₄ solution and a given
175 concentration of TMP (and other micropollutants in some trials), at 25 °C and kept under
176 vigorous magnetic stirring. The anode was a commercial IrO₂-based plate (i.e., dimensionally
177 stable anode, DSA) in most of the assays, although a boron-doped diamond (BDD) thin film on
178 Si substrate was employed for comparison. The anode had a geometric surface area of 3 cm² (i.e.,

179 area exposed to the solution), as was also the case of the cathode made with
180 carbon-polytetrafluoroethylene (PTFE) on carbon cloth. This material was purchased from
181 BASF and placed inside a tubular gas chamber to be fed with atmospheric air pumped at flow
182 rate of 1 L min^{-1} for H_2O_2 generation. The electrodes were mounted with a gap of 1.0 cm between
183 each other. The EF treatments started after the addition of the catalyst and the supply of a
184 constant current from a DC power source (IT6322A from ITECH, China). For cycling tests, the
185 catalyst was recovered by centrifugation, washed with ultrapure water and dried overnight in a
186 vacuum drying oven at $60 \text{ }^\circ\text{C}$.

187 The pH was measured with a PHS-3C pH-meter. At selected time intervals, samples were
188 collected and filtered ($0.2 \text{ }\mu\text{m}$ PTFE syringe filters) prior to analysis to remove the solid. The
189 H_2O_2 concentration accumulated during the electrolytic trials was determined from the
190 absorbance of the complex formed between the oxidant and a Ti(IV) reagent, using a UNIC
191 UV2365 UV/Vis spectrophotometer ($\lambda = 408 \text{ nm}$, $25 \text{ }^\circ\text{C}$) [30]. The iron concentration leached
192 from the catalyst was quantified from the absorbance of the complex formed between Fe^{2+} and
193 1,10-phenanthroline, employing the same spectrophotometer ($\lambda = 510 \text{ nm}$, $25 \text{ }^\circ\text{C}$). Some of these
194 results were also confirmed by means of inductively-coupled plasma optical emission
195 spectrometry (ICP-OES, performed with a ICPS-8100 instrument from Shimadzu). TMP
196 concentration was determined by HPLC using a SCION6000 chromatograph equipped with a
197 CHromcore C18 $5 \text{ }\mu\text{m}$ ($250 \text{ mm} \times 4.6 \text{ mm}$) column, thermostated at $35 \text{ }^\circ\text{C}$, and a SC6000
198 detector set at 270 nm . A mixture of CH_3OH and $0.010 \text{ M KH}_2\text{PO}_4$ solution at pH 3.0, with ratio
199 30:70 (v/v), was eluted at 1.0 mL min^{-1} as mobile phase, disclosing a well-defined peak

200 corresponding to TMP at retention time of 4.8 min. The total organic carbon (TOC) concentration
201 was measured with a TOC analyzer (TOC-L CPH, Shimadzu). The S content of catalysts was
202 analyzed by inductively coupled plasma with optical emission spectroscopy (ICP-OES, Agilent
203 5110). The reaction intermediates were identified by LC-QTOF-MS analysis, which was carried
204 out using a Chromatograph Ultimate 3000 (Thermo Scientific) coupled to an LTQ Orbitrap Velos
205 mass spectrometer (Thermo Scientific), operating in positive ion mode. An Acquity UPLC BEH
206 C18 column 1.7 μm (50 mm \times 2.1 mm) column, at 40 $^{\circ}\text{C}$, was utilized. The chromatograph also
207 had a UV detector, which was set at 270 nm. The mobile phase was a mixture of CH_3CN (A) and
208 0.1% CH_3COOH (B) eluted at 0.3 mL min^{-1} according to the following gradient (t , %B): (0, 5),
209 (15, 50), (16,100), (18,100), (19, 5) and (24, 5).

210 **3. Results and discussion**

211 *3.1. Characterization of catalysts*

212 The morphological features of the as-prepared catalysts evaluated by TEM analysis can be
213 observed in Fig. 1b. MIL-88B(Fe) is composed of typical fusiform rods (i.e., spindle-shaped),
214 with length of around 450 nm [17]. After sulfidation, the hybrid S-MIL-88B-3h-3 inherited the
215 morphology and dimensions of its MIL-88B(Fe) precursor (Fig. 1c), which informs about the
216 good stability of catalyst and the excellent mass transport of species during the synthesis as a
217 result of the strong coordination environment and the high porosity of MIL-88B(Fe). The
218 elemental mapping in Fig. 1d reveals the outstanding composition uniformity, with C, O, S and
219 Fe elements perfectly distributed in the S-MIL-88B-3h-3, thus discarding the aggregation of
220 Fe_3S_4 particles. The loose backbone of the MIL-88B(Fe) precursor not only prevented the

221 agglomeration of Fe_3S_4 crystals, but it also ensured a wide exposure of active sites that
222 facilitated the electron transfer for reactions during the synthesis [31].

223 **Fig. 2a** depicts the XRD patterns of MIL-88B(Fe) and S-MIL-88B-3h-3. The main peaks
224 for the as-prepared MIL-88B(Fe) appear at 9.1° (002), 10.6° (101), 12.5° (102), 17.7° (200),
225 21.8° (202), and 26.7° (211), which is in perfect agreement with the simulated diffractogram
226 reported in the CIF database, thus confirming the successful synthesis [31]. These main peaks are
227 present in the pattern of S-MIL-88B-3h-3, being accompanied by characteristic peaks located at
228 25.4° , 30.0° , 36.3° , 44.9° , 47.8° and 52.4° that can be ascribed to (220), (311), (400), (422), (511)
229 and (440) crystal planes of Fe_3S_4 (JCPDS 16-0713) [32]. This proves the co-existence of
230 MIL-88B(Fe) structure and Fe_3S_4 particles after the sulfidation treatment. Worth noting, the
231 position of the diffraction peak corresponding to the (102) facet of MIL-88B(Fe) exhibited a
232 remarkable shift. Such modification of the crystallographic characteristics can be explained by
233 the structural flexibility of MIL-88B(Fe), which induces slight structural changes upon entry of
234 the guest species (i.e., H_2S produced from TAA) into the pore channels [31]. The variations in
235 crystal and pore structures are more clearly evidenced by the N_2 sorption analysis (**Fig. S1a**, **Fig.**
236 **S1b and Table S1**). The specific surface area and total pore volume decreased drastically upon
237 sulfidation treatment, which is due to the collapse of pore tunnels and the formation of Fe_3S_4 [33].
238 However, the DLS analysis in **Fig. S1c** reveals a similar particle size distribution in both catalysts,
239 implying that the generated ultra-small Fe_3S_4 crystals are uniformly dispersed on the
240 MIL-88B(Fe) framework, not being detectable by DLS. The diameter of most of the MOF
241 particles was between 400 and 1000 nm, which agrees with the particle size determined by TEM

242 images.

243 The surface chemical composition and oxidation states of MIL-88B(Fe) and
244 S-MIL-88B-3h-3 were analyzed by XPS. The high resolution Fe 2p spectrum of MIL-88B(Fe) in
245 Fig. 2b exhibits two sets of fitting peaks, which account for Fe 2p_{2/3} and Fe 2p_{1/2} bands assigned
246 to Fe(III). The peaks centered at 711.08 and 724.79 eV correspond to Fe(III) of Fe-O-C (BDC),
247 whereas those appearing at 713.82 and 729.87 eV are assigned to Fe(III) of μ_3 -OFe [33,34]. In
248 addition, a couple of weaker peaks can be ascribed to Fe(II). These results inform about the
249 predominance of the Fe(III) form of iron species in MIL-88B(Fe). As for S-MIL-88B-3h-3
250 hybrids, a new peak appearing at 706.43 eV is attributed to the presence of Fe(II)-S species,
251 whereas the peaks at 710.70, 713.41, 724.65 and 728.95 eV corresponded to Fe 2p_{3/2} and Fe 2p_{1/2}
252 of Fe(III), which could be originated from the formation of Fe(III)-S species alongside the
253 presence of the Fe(III) species in MIL-88B(Fe) [32,35]. Note that significant shifts of the Fe 2p
254 peaks toward lower binding energies can be observed for S-MIL-88B-3h-3, which is attributed to
255 the strong interactions between MIL-88B(Fe) and Fe₃S₄ that affect the electron density of the
256 iron sites [36]. Furthermore, the peak intensities of Fe(II) increased, demonstrating the
257 conversion of Fe(III) into Fe(II) during the sulfidation treatment. The XPS spectrum of S 2p in
258 Fig. 2c has been deconvoluted into five peaks: S_{bulk}²⁻, S_{surface}²⁻, S_n²⁻, S⁰ and SO₄²⁻ [35,37]. The
259 presence of S_n²⁻ species can be related to the thermodynamically-driven redox process
260 comprising S²⁻ oxidation to S_n²⁻ and Fe(III) reduction to Fe(II) during the sulfidation treatment,
261 which agrees with the increase in the amount of Fe(II) species [38]. The production of S⁰ and
262 SO₄²⁻ is attributed to the reactions between S²⁻ and Fe(III) [39,40]. All the possible reactions

263 occurred during the sulfidation are summarized in [Table S2](#). In short, the solvothermal treatment
264 with TAA can modify the chemical and electronic structures of MIL-88B(Fe), generating Fe₃S₄
265 particles and enhancing the amount of Fe(II) active sites, which are expected to play key roles in
266 H₂O₂ activation. Moreover, the proportion of Fe₃S₄ in S-MIL-88B-3h-3 was determined as 20.8
267 wt.% from the content of S elements measured by ICP-OES/MS ([Table S1](#)).

268 In addition, the FTIR spectra of MIL-88B(Fe) and S-MIL-88B-3h-3 in [Fig. 2d](#) inform
269 about the surface functional groups. The peaks at 1657, 1600 and 1393 cm⁻¹ for MIL-88B(Fe)
270 are associated to the C=O tensile shock, asymmetric vibration and symmetric vibration of
271 carboxylate groups. The absorption peaks at 3430 and 749 cm⁻¹ can be assigned to the O-H
272 stretching vibration and the C-H bending vibration [\[41\]](#). The characteristic peak at 551 cm⁻¹ is
273 related to the Fe-O stretching mode arising from the link between Fe atoms and the ligand. The
274 appearance of these peaks in S-MIL-88B-3h-3 demonstrates the stability of the MIL-88B(Fe).
275 Furthermore, the magnetic properties of S-MIL-88B-3h-3 were verified from the magnetic
276 hysteresis curve, depicted in [Fig. S1d](#). The saturation magnetization (M_s) of S-MIL-88B-3h-3
277 was 12.7 emu·g⁻¹, a much higher value than that of MIL-88B(Fe) (2.66 emu·g⁻¹). The enhanced
278 magnetism upon sulfidation treatment enables the facile post-treatment recovery of the catalyst.

279 *3.2. Evaluation of the catalytic performance*

280 Several systems were applied to treat solutions containing 0.060 mM (i.e., 10 mg C L⁻¹)
281 TMP + 0.050 M Na₂SO₄ at pH 7.0. Prior to investigate the viability of electrochemical
282 degradation, adsorption trials were carried out. As depicted in [Fig. 3a](#), the presence of either
283 0.10 g L⁻¹ MIL-88B(Fe) or S-MIL-88B-3h-3 as suspended particles in the aforementioned drug

284 solution yielded a TMP removal close to 4%, which means that the contribution of this
285 phenomenon during the following electrochemical trials made at 50 mA can be considered as
286 negligible. The electro-oxidation with electrogenerated H₂O₂ (EO process) in a cell equipped
287 with a DSA plate as the anode allowed achieving a small TMP removal of 22% after 90 min of
288 electrolysis, in agreement with the expected low oxidation power of H₂O₂ and IrO₂(•OH)
289 produced cathodically and anodically, respectively [20]. In contrast, the MIL-88B(Fe)-catalyzed
290 HEF process led to a more substantial degradation of 65% at 90 min, resulting from the
291 formation of •OH upon occurrence of Fenton's reaction. However, despite possessing a certain
292 ability to trigger the H₂O₂ decomposition, the unsaturated iron active sites of this catalyst were
293 not sufficiently active. In contrast, the S-MIL-88B-3h-3-catalyzed HEF process showed an
294 outstanding performance as compared to all the previous trials, reaching complete TMP
295 abatement in only 45 min. To describe the kinetics of TMP degradation during different
296 electrochemical trials, zero-, first- and second-order models were investigated. As summarized in
297 [Table S3](#), the zero-order model shows the highest correlation coefficients (R^2) for both HEF
298 treatments, indicating that the catalytic reactions agreed with a Langmuir-Hinshelwood
299 mechanism, which means that the active sites on the catalyst surface were substantially covered
300 by TMP and H₂O₂. In addition, the zero-order kinetic constant in S-MIL-88B-3h-3-catalyzed EF
301 was 0.3399 mM min⁻¹, being approximately 4-fold greater than that found in HEF with
302 MIL-88B(Fe). In the case of EO, the three models show high R^2 values but, considering that the
303 EO process is usually related to pseudo-first-order kinetics due to the fact that a constant M(•OH)
304 amount is produced at the anode surface [11], the k -value under such model was determined as

305 0.0028 min⁻¹. The superior catalytic activity of S-MIL-88B-3h-3 can be assigned to the
306 synergistic effect between MIL-88B(Fe) and Fe₃S₄. The main reactions occurred during the
307 S-MIL-88B-3h-3-catalyzed HEF process are listed in [Table S4](#). The uniformly dispersed Fe(II)
308 species from both MIL-88B(Fe) and Fe₃S₄ act as the active sites for H₂O₂ decomposition to form
309 abundant •OH. Meanwhile, the S²⁻ and S_n²⁻ species provide electrons for Fe(III) reduction at high
310 rate, continuously renewing the Fe(II) active sites that ensures a fast production of •OH [38,42].
311 The unique morphology and structure of the hybrids, namely ultra-small Fe₃S₄ crystals with
312 uniform distribution on/in the MIL-88B(Fe) nanoparticles, ensures the access to plenty of
313 exposed active sites for the catalytic reactions. [Fig. 3b](#) evidences a very low iron leaching from
314 both MIL-88B(Fe) and S-MIL-88B-3h-3 during the HEF treatments, being 0.58 and 1.23 mg L⁻¹
315 at 90 min, respectively, which confirms the great stability of the catalysts. The higher dissolved
316 iron concentration from S-MIL-88B-3h-3 can be due to the partial collapse of the framework
317 during the synthesis and the partial decomposition of Fe₃S₄ during the treatment. In spite of this,
318 the leached Fe concentration is still far below the European Union standard of 2 mg L⁻¹ [43]. [Fig.](#)
319 [3b](#) also shows the decrease of pH in both cases, thanks to the formation of acidic intermediates
320 like carboxylic acids, as well as to the spontaneous acidification occurring upon Fe(III) reduction
321 by S²⁻ to form sulfite or sulfate ([Table S4](#)) [14].

322 The TAA/MIL-88B(Fe) ratio and hydrothermal treatment time are considered crucial factors
323 for the optimization of the sulfidation process, thus being necessary to evaluate the catalytic
324 performance of S-MIL-88B-*y*h-*x* in the HEF process. [Fig. 4a](#) shows the TMP decays using
325 several S-MIL-88B-3h-*x* catalysts. The increase in the TAA/MIL-88B(Fe) ratio from 0.5 to 3

326 gave rise to a substantial promotion in the TMP degradation efficiency, from 50% at 90 min to a
327 faster and total removal. Nonetheless, further increase of the ratio to 4 was detrimental. Note that,
328 at the lowest ratio of 0.5, the sulfidated catalyst exhibited a poorer activity as compared to
329 MIL-88B(Fe), suggesting that such a small amount of TAA causes the collapse of the
330 MIL-88B(Fe) framework but is insufficient to form abundant Fe₃S₄ crystals. This is confirmed
331 by the XRD patterns of the five as-synthesized catalysts (Fig. 4b), where the peak shifts as
332 compared to MIL-88B(Fe) and the absence of Fe₃S₄ peaks are evident for S-MIL-88B-3h-0.5.
333 The progressive increase in the amount of TAA enhanced the structural modification of
334 MIL-88B(Fe) with formation of Fe₃S₄, finding an excellent catalytic performance of the
335 S-MIL-88B-3h-3 catalyst (i.e., ratio of 3) thanks to the optimal Fe₃S₄ content (Fig. 4a). The
336 peaks of MIL-88B(Fe) in S-MIL-88B-3h-4 almost disappeared, implying the severe collapse of
337 the framework with the consequent loss of iron active sites from MIL-88B(Fe). Consequently,
338 the poor mass transport due to that collapse of the porous structure decelerated the TMP
339 degradation. In addition, the iron leaching during the TMP treatment was kept low but it
340 increased sharply at an excessive TAA/MIL-88B(Fe) ratio (Fig. S2a), which informs about the
341 importance of the strong coordination between metal atoms and ligands in MIL-88B(Fe) to
342 stabilize the iron active sites, avoiding their loss during the HEF treatment. The MIL-88B(Fe)
343 owns a topological Fe₃O(BDC)₃ structure, in which Fe atoms exhibit an octahedral environment
344 that is terminated by some nonbridging ligands like water, a unique structure that confers
345 excellent stability to the Fe sites [18].

346 Once established that a ratio of 3 was optimum, the catalytic performance of

347 S-MIL-88B-yh-3 was investigated. In Fig. 4c, the superiority of the S-MIL-88B-3h-3 sample is
348 corroborated, since the TMP removal efficiency increased as the hydrothermal treatment time
349 was prolonged from 1 to 3 h, whereupon a longer time became detrimental. These results
350 demonstrate again that insufficient sulfidation certainly alters the backbone of MIL-88B(Fe) but
351 yields a small amount of Fe₃S₄, whereas an excessively long synthesis may destroy most of the
352 MIL-88B(Fe) particles, leaving the Fe₃S₄ crystals irregularly distributed on a structurally
353 affected MOF support (Fig. S2c). The highest dissolved iron concentration found using the
354 S-MIL-88B-4h-3 in HEF (Fig. S2b) confirms the crucial role of MIL-88B(Fe) to ensure the
355 catalyst stability.

356 The effect of initial solution pH, catalyst dosage and applied current on the drug
357 concentration decay when operating the S-MIL-88B-3h-3-catalyzed HEF system is displayed in
358 Fig. 4d-4f. As can be observed in Fig. 4d, the fastest TMP decay was achieved at initial pH 3.0,
359 attaining the total removal after only 30 min, which can be ascribed to the greater oxidation
360 potential of •OH at pH 3.0 and the increased iron solubilization (7.1 mg L⁻¹ at 90 min, Fig. S2d).
361 The latter phenomenon results in a larger •OH production from homogenous Fenton's reaction (1)
362 [14]. Note that such large accumulation of dissolved iron at initial pH 3.0 implies the intolerance
363 of S-MIL-88B-3h-3 to strong acidic condition. Fortunately, total removal of TMP could be still
364 obtained at 45 min at initial pH 5.0-7.0, whereas TMP concentration decay of 96% at 90 min was
365 attained at initial pH 9.0. The final leached iron content in these trials was lower than 2.0 mg L⁻¹
366 (Fig. S2d), a very positive finding referred to the stability of S-MIL-88B-3h-3 at mild pH. In
367 contrast, a remarkably poor TMP removal of 22% was observed at initial pH 11.0 due to the

368 relatively low oxidation potential of $\bullet\text{OH}$ and the self-decomposition of H_2O_2 at alkaline pH [18].
369 Therefore, it can be concluded that the S-MIL-88B-3h-3-catalyzed HEF is advantageous to work
370 over a wide pH range. The solutions became acidified in all cases (Fig. S2d), owing to the
371 production of acidic organic by-products and pH self-regulation (Table S4) [14].

372 Fig. 4e highlights that a higher amount of catalyst from 0.05 to 0.10 g L^{-1} gives rise to a
373 substantial enhancement in the TMP degradation efficiency, increasing from 53% to >98% at
374 45 min. The increase in the catalyst dosage provides more available active sites for the H_2O_2
375 adsorption and activation, generating abundant $\bullet\text{OH}$ to destroy TMP. Conversely, when
376 increasing to 0.15 g L^{-1} , the acceleration of the degradation was insignificant, probably due to the
377 parasitic reaction between excessive iron sites and $\bullet\text{OH}$ [10]. Moreover, at the greatest catalyst
378 content, a more severe iron leaching was found (insert figure), thereby confirming that the
379 optimum dosage was 0.10 g L^{-1} .

380 As can be seen in Fig. 4f, the applied current played a minor role in the
381 S-MIL-88B-3h-3-catalyzed HEF, since quite similar TMP decays were obtained (i.e., 94%, 97%,
382 98% and 100% at 45 min, respectively). Fig. S2e depicts the H_2O_2 concentration accumulation in
383 the solution from reaction (3), gradually rising at higher applied current. However, this
384 improvement was not realized in a considerably faster TMP removal, suggesting that an excess
385 of H_2O_2 is mostly wasted because the rate of heterogeneous Fenton's reaction is actually limited
386 by the availability and activity of the given catalyst. Instead, a further rise in current to 100 mA
387 was detrimental due to the scavenging reaction occurring between $\bullet\text{OH}$ and the excess of
388 accumulated H_2O_2 [10,31].

389 3.3 Recyclability of the catalyst and treatment of micropollutants in urban wastewater

390 The reusability of Fenton catalysts is one of the critical issues to be addressed for practical
391 application of this type of EAOPs. The evaluation was conducted upon simple magnetic
392 recovery of the S-MIL-88B-3h-3 catalyst from the treated solution, followed by washing with
393 ultrapure water. Note that the recovery percentage of the catalyst reached up to $95\pm 3\%$. As
394 illustrated in Fig. 5a, the TMP concentration diminished completely in 45 min in the first three
395 runs, whereas it was still possible to achieve more than 90% TMP removal in the 4th cycle.
396 These results demonstrate the relatively high reusability of the catalyst for HEF. The slower
397 degradation once a certain number of cycles has been performed can be accounted for by surface
398 passivation and deactivation, as well as by the spontaneous acidification during the runs that
399 contributes to some iron leaching. Therefore, the used catalyst after the fourth trial was
400 characterized by XRD and XPS, trying to correlate the observed behavior with the chemical and
401 structural changes. The XRD patterns in Fig. S3, corresponding to fresh and used
402 S-MIL-88B-3h-3, demonstrated that the crystallinity of the catalyst remained quite stable along
403 the treatment, without any obvious alteration. The Fe 2p spectra depicted in Fig. 5b highlight the
404 significant reduction of the peak intensities of Fe(II)-S and other Fe(II) species, implying the
405 intense consumption of Fe(II) active sites by Fenton's reaction during the four consecutive
406 cycles. Regarding to S 2p spectra in Fig. 5c, the decrease in the peak intensities of S_{bulk}^{2-} and
407 S_{surface}^{2-} species and the increase in those of S_n^{2-} , S^0 and SO_4^{2-} species when comparing the fresh
408 and used catalyst is a clear proof of the promotion of reactions listed in Table S4 by S^{2-} . The
409 electrons are transferred from the S_{bulk}^{2-} and S_{surface}^{2-} species to the Fe(III) sites during the

410 catalysis, leading to the Fe(III)-to-Fe(II) conversion and the formation of oxidized sulfur species
411 [42]. Hence, the progressive consumption of S^{2-} species at the catalyst surface decelerates the
412 Fe(II) regeneration, eventually reducing the production of $\bullet OH$ for TMP degradation. Despite the
413 inevitable deactivation of the catalyst, proper cleaning with methanol and 10 mM HCl allowed its
414 complete regeneration, being feasible to recover 100% TMP decay in 60 min (cycle 1st in Fig.
415 5a). This was due to the fact that the loss of S^{2-} species pre-eminently occurs at the surface of the
416 catalyst and thus, the generated sulfur species (S^0 and SO_4^{2-}) can be removed by facile washing
417 with methanol [35]. As another interesting feature to support the good stability, note that the
418 dissolved iron concentration from S-MIL-88B-3h-3 was much lower than that from relatively
419 pure Fe_3S_4 (Fig. S2a and S2b), which also implied the suppressed decomposition of Fe_3S_4 in
420 S-MIL-88B-3h-3 due to the unique structure of MIL-88B(Fe).

421 The high performance of S-MIL-88B-3h-3 catalyzed HEF treatment of several
422 micropollutants spiked into urban wastewater was further confirmed (Fig. 5d-5e). It is
423 highlighted that 90% TMP could be removed at initial pH 7.0, a worse behavior than that
424 observed in 0.050 M Na_2SO_4 medium (Fig. 3a) due to the role of inorganic carbon and natural
425 organic matter as $\bullet OH$ scavengers, but still quite effective. Worth noting, the decay of TMP
426 concentration was complete at 45 min at a slightly more acidic pH of 6.0 (Fig. 5d), which can be
427 attributed to the partial removal of inorganic carbon and increased catalytic activity. Moreover,
428 the HEF treatment of other four ubiquitous micropollutants like naproxen, bisphenol A,
429 ciprofloxacin and 2,4-dichlorophenol spiked into urban wastewater at pH 6.0 was evaluated
430 positively, as shown in Fig. 5e. The treatment was very efficient for the former two, attaining 100%

431 and 94%, respectively, at 90 min, whereas 86% disappearance of 2,4-dichlorophenol and 76%
432 destruction of ciprofloxacin were achieved. The difference in their degradation kinetics can be
433 related to the specific structure of the target molecules, which affects their interaction and
434 reactivity with $\bullet\text{OH}$. Finally, the performance of the S-MIL-88B-3h-3-catalyzed HEF treatment
435 was not only evaluated by determining the time course of the TMP concentration but also by
436 assessing the trend of solution TOC in both sulfate medium and urban wastewater. Fig. 5f reveals
437 substantial TOC abatements of 70% and 57% in sulfate and wastewater, respectively, after 240
438 min of treatment employing the IrO_2 -based DSA anode at 50 mA. When replacing the anode by
439 BDD, the TOC abatement was significantly increased to 86% and 73% at 240 min, which is
440 attributed to the production of a much stronger oxidant like physisorbed BDD($\bullet\text{OH}$) [44]. This is
441 not as free in solution as the $\bullet\text{OH}$ produced via Fenton's reaction, but it is clearly superior to
442 $\text{IrO}_2(\bullet\text{OH})$. On the other hand, the presence of natural organic matter retarded the TOC abatement
443 in urban wastewater. Note that a very negligible TOC decay could be achieved during the last 120
444 min treatment in all the cases, probably because of the accumulation of small persistent but
445 non-toxic (i.e., non-aromatic) organic molecules.

446 *3.4 Identification of aromatic intermediates and proposed TMP degradation routes*

447 As summarized in Table S5, six main aromatic intermediates generated during the TMP
448 degradation were identified by LC-QTOF-MS analysis. The prevailing degradation routes were
449 thus proposed (Fig. 6), involving carbonylation, consecutive pure hydroxylation and mixed
450 hydroxylation steps accompanied either by oxidation or loss of methoxy group. The direct
451 attack of TMP by $\bullet\text{OH}$ and $\text{M}(\bullet\text{OH})$ may cause carbonylation at the methylene bridge, giving rise

452 to the primary product **P1** [45]. Hydroxylation in one of the methoxy positions of the benzene
453 ring was confirmed by the production of intermediate **P2**, also reported by other authors [46].
454 Hydroxylation has been widely reported as the preferred pathway in other AOPs [47,48];
455 hydrogen abstraction of the bridge $-\text{CH}_2-$ group by $\bullet\text{OH}$ resulted in the formation of a
456 carbon-centered radical, which was followed by the reaction with molecular oxygen and
457 elimination of the hydroperoxyl radical, finally yielding the α -hydroxytrimethoprim product **P3**.
458 Further oxidation of **P3** also gave rise to the keto-derivative **P1**. Note that the addition of
459 electrophilic $\bullet\text{OH}$ to the aromatic ring of TMP agreed with the same hydrogen abstraction
460 mechanism, originating the monohydroxylated by-product **P4**. Moreover, the latter underwent
461 subsequent $\bullet\text{OH}$ attack, leading to the formation of di- (**P5**) and tetra- (**P6**) hydroxylated
462 compounds via the hydroxylation reactions, being accompanied by the loss of all methoxy
463 groups in the case of **P6** generation. Alternatively, the hydroxylation of **P2** can also justify the
464 production of **P6**. Note that the loss of N atoms in N-containing compounds like TMP can give
465 rise to inorganic ions such as NH_4^+ , NO_3^- and NO_2^- [49]. As reported elsewhere, it is expected
466 that 20%-40% of initial N is transformed into NH_4^+ and NO_3^- , without no trace of NO_2^- , during
467 Fenton-based treatments [50,51].

468 *3.5 Mechanistic insights*

469 EIS and Tafel tests were first carried out to investigate the electron transfer capability of the
470 catalysts. The Nyquist plots of S-MIL-88B-3h-3 and MIL-88B(Fe) samples are displayed in Fig.
471 S4a, with the equivalent circuit shown inside. The interfacial charge-transfer resistance (R_{ct})
472 obtained from the semicircle arcs reflects the electron transfer capability [52]. The R_{ct} value of

473 S-MIL-88B-3h-3 (1.1 k Ω) was much lower than that of MIL-88B(Fe) (7.6 k Ω), implying a much
474 faster charge transfer kinetics using the S-MIL-88B-3h-3. On the other hand, the Tafel slopes for
475 the polarization curves obtained with both samples are compared in Fig. S4b, being 66 and 83
476 mV dec⁻¹ using S-MIL-88B-3h-3 and MIL-88B(Fe) catalyst, respectively. Since a lower Tafel
477 slope can be correlated with a greater catalytic activity, it is evident that the S-MIL-88B-3h-3
478 catalyst possess a faster electron transfer rate, requiring a lower overpotential to reach a given
479 current [53]. These results agree with the R_{ct} values from the EIS test. The higher electron
480 transfer efficiency of S-MIL-88B-3h-3 can thus contribute to accelerate the activation of H₂O₂
481 and the Fe(III)-to-Fe(II) conversion, justifying the better catalytic performance in HEF.

482 To gain a deeper insight into the synergistic effect of MIL-88B(Fe)/Fe₃S₄ hybrids that
483 causes the enhancement of HEF process, the structure modeling, charge density difference and
484 adsorption of H₂O₂ were established by DFT calculations. As shown in Fig. 7a-7c, the optimized
485 configurations of MIL-88B(Fe), Fe₃S₄ and their hybrids were successfully constructed through
486 the JCPDS card No. 16-0713 of MIL-88B(Fe) and (400) planes of Fe₃S₄ [54]. The charge density
487 difference was calculated to evaluate the charge transfer and separation at the interface of the
488 hybrids. In Fig. 7d-7g, the purple regions denote charge depletion and the azure regions denote
489 charge accumulation. The side and top views of the charge density difference in MIL-88B(Fe)
490 (Fig. 7d and 7f) reveal that the charge accumulation mainly occurs around the iron atoms,
491 whereas charge depletion is concentrated near the oxygen atom. The facile electron transfer from
492 oxygen to iron could promote the Fe(III)-to-Fe(II) conversion. Regarding to MIL-88B(Fe)/Fe₃S₄
493 heterostructure, more dense charge accumulation is centered around the iron sites due to the

494 presence of sulfur atoms (Fig. 7e and 7g). The enhanced charge redistribution is expected to
495 produce more electron-rich iron active sites, and the Fe(III)/Fe(II) redox cycling could be
496 accelerated by promoting the electron transfer speed [55]. The adsorption energy (E_{ads}) of H_2O_2
497 on the catalysts was calculated by the following equation to further evaluate the catalytic
498 performance:

$$499 \quad E_{\text{ads}} = E_{\text{total}} - E_{\text{H}_2\text{O}_2} - E_{\text{catalyst}} \quad (7)$$

500 where E_{total} is the total energy of H_2O_2 /catalyst complexes, and $E_{\text{H}_2\text{O}_2}$ and E_{catalyst} are the energies
501 of isolated H_2O_2 molecule and catalyst, respectively. As depicted in Fig. 7h and 7i, the E_{ads} value
502 of MIL-88B(Fe)/ Fe_3S_4 hybrids with H_2O_2 (-0.80 eV) is higher (in absolute value) than that using
503 pure MIL-88B(Fe) (-0.64 eV). The negative value of E_{ads} implies the stable adsorption of H_2O_2
504 on the catalysts, and the more negative binding energy means the stronger interaction between
505 H_2O_2 and MIL-88B(Fe)/ Fe_3S_4 hybrids [56]. The DFT results unambiguously reveal the critical
506 role of Fe_3S_4 on the modulation of the electronic structure of the MOF precursor and the
507 enhancement of the catalytic performance during HEF treatments.

508 Taking into account the aforementioned findings, a thorough catalytic mechanism is
509 proposed in Fig. 8 for the S-MIL-88B-3h-3-catalyzed HEF treatment of TMP at neutral pH.
510 H_2O_2 is first generated at the cathode through 2-electron oxygen reduction reaction (3), thereby
511 being transported to get adsorbed onto the S-MIL-88B-3h-3 particles. The adsorbed H_2O_2
512 molecules are quickly activated by the Fe(II) active sites from either MIL-88B(Fe) or Fe_3S_4 to
513 form abundant $\bullet\text{OH}$, which is responsible for the efficient destruction of TMP molecules. In
514 addition, the $\text{M}(\bullet\text{OH})$ produced via the anodic reaction can also contribute to the degradation.

515 More importantly, the excellent catalytic performance of S-MIL-88B-3h-3 is ensured by the
516 presence of abundant exposed Fe(II) active sites, the acceleration of Fe(III)/Fe(II) redox cycling
517 and the facile mass transport of H₂O₂ to the catalyst. The introduction of well distributed S²⁻
518 species as electron donors for Fe(III) reduction makes reaction (5) no longer the rate-limiting
519 step of HEF process, as the regeneration of Fe(II) active centers is greatly boosted. Moreover, the
520 partial inheritance of the morphology and crystal structure of MIL-88B(Fe) precursor largely
521 enhances the stability and recyclability of S-MIL-88B-3h-3 during the treatment.

522 **4. Conclusions**

523 This work proves how rational design results in very effective and stable HEF catalysts to
524 treat micropollutants in actual wastewater. A facile sulfidation strategy to prepare ultra-uniform
525 MIL-88B(Fe)/Fe₃S₄ hybrids as an efficient catalyst in HEF treatment of TMP has been
526 developed. The as-synthesized material owns stable morphological and crystal structure
527 inherited from the MIL-88B(Fe) precursor, allowing the immobilization of ultra-small Fe₃S₄
528 particles. As a result, the S-MIL-88B-3h-3-catalyzed HEF system achieved the quickest
529 complete removal of TMP at mild pH, only requiring 45 min. A mechanistic study has revealed
530 that the excellent catalytic performance can be attributed to: (i) the acceleration of the
531 Fe(III)/Fe(II) redox cycling by S²⁻ species; (ii) the presence of a higher amount of Fe(II) active
532 centers; (iii) the promotion of the electron transfer rate; and (iv) the efficient mass transport of
533 H₂O₂ towards the catalyst surface. The sulfidation conditions as well as the HEF parameters
534 have been optimized, concluding that the treatment is viable at low catalyst dosage and current
535 over a wide pH range. The S-MIL-88B-3h-3 catalyst undergoes a slight deactivation due to the

536 consumption of S^{2-} species, although reactivation is feasible upon removal of adsorbed sulfur
537 products and organic byproducts by proper rinsing. It can be concluded that sulfidation of
538 MIL-88B(Fe) allows enhancing the catalyst activity at the expense of its stability to a small
539 extent, being these two features identified as the preeminent advantage and disadvantage,
540 respectively. A thorough reaction mechanism for MIL-88B(Fe)/ Fe_3S_4 -catalyzed HEF treatment
541 of TMP has been finally proposed, opening a new chapter in the practical application of HEF
542 process.

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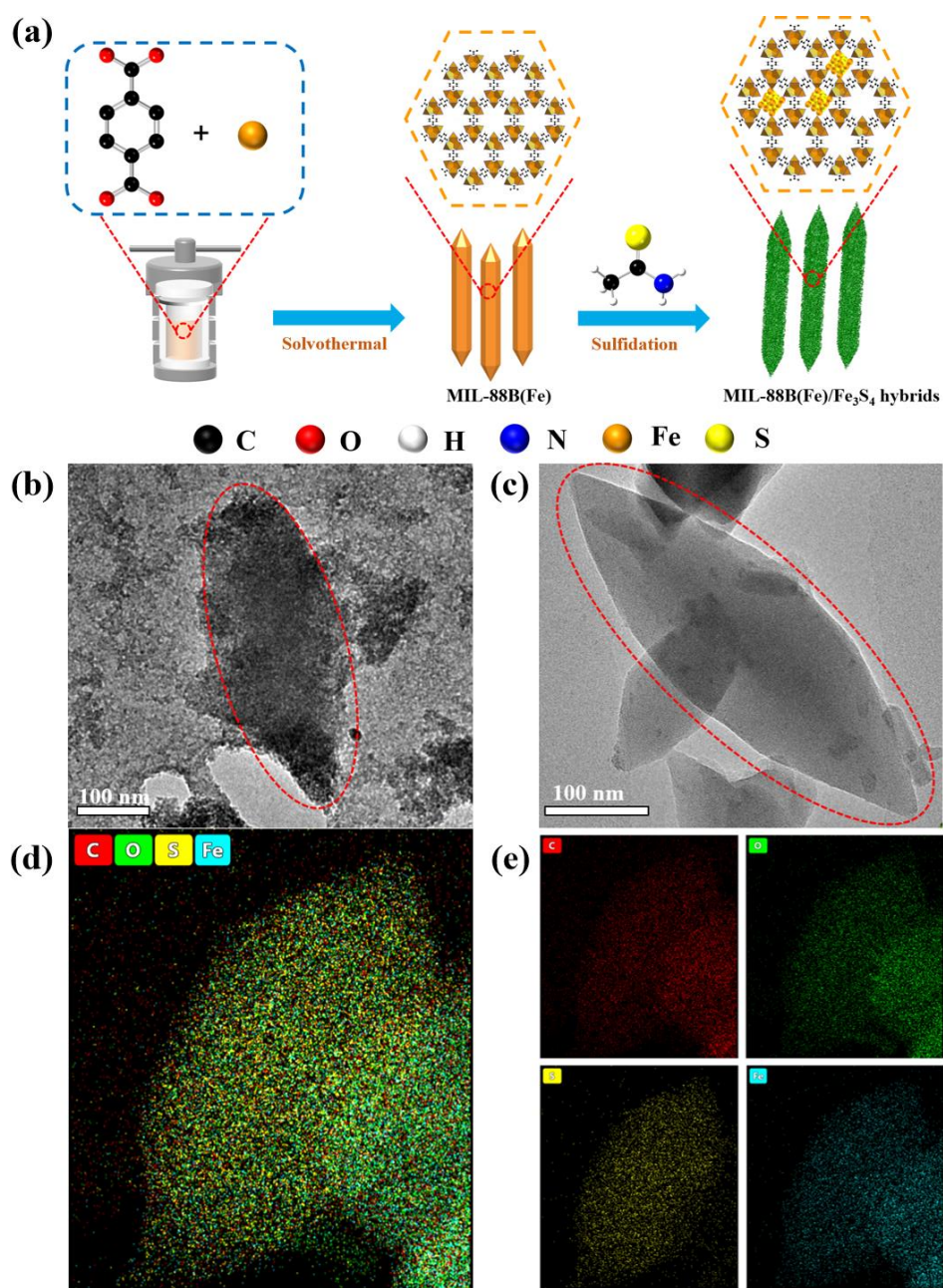


Fig. 1. (a) Scheme of the synthesis route to sulfidation-engineered MIL-88B(Fe)/Fe₃S₄ hybrids. TEM images of (b) MIL-88B(Fe) and (c) S-MIL-88B-3h-3. (d) EDS mapping displaying the uniform dispersion of elements in S-MIL-88B-3h-3.

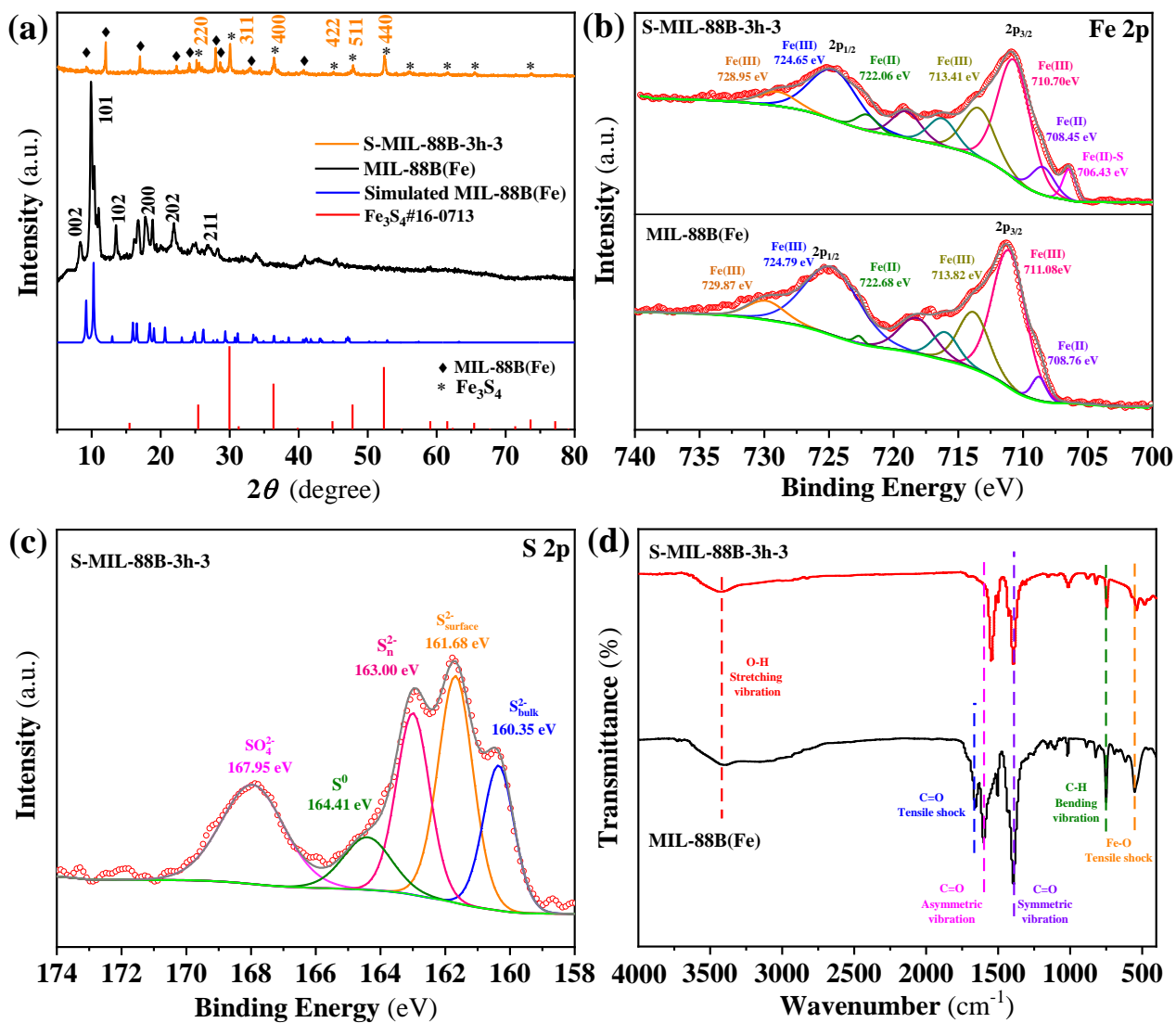


Fig. 2. (a) XRD patterns, (b) Fe 2p XPS spectra, and (d) FTIR spectra of MIL-88B(Fe) and S-MIL-88B-3h-3. (c) S 2p XPS spectrum of S-MIL-88B-3h-3.

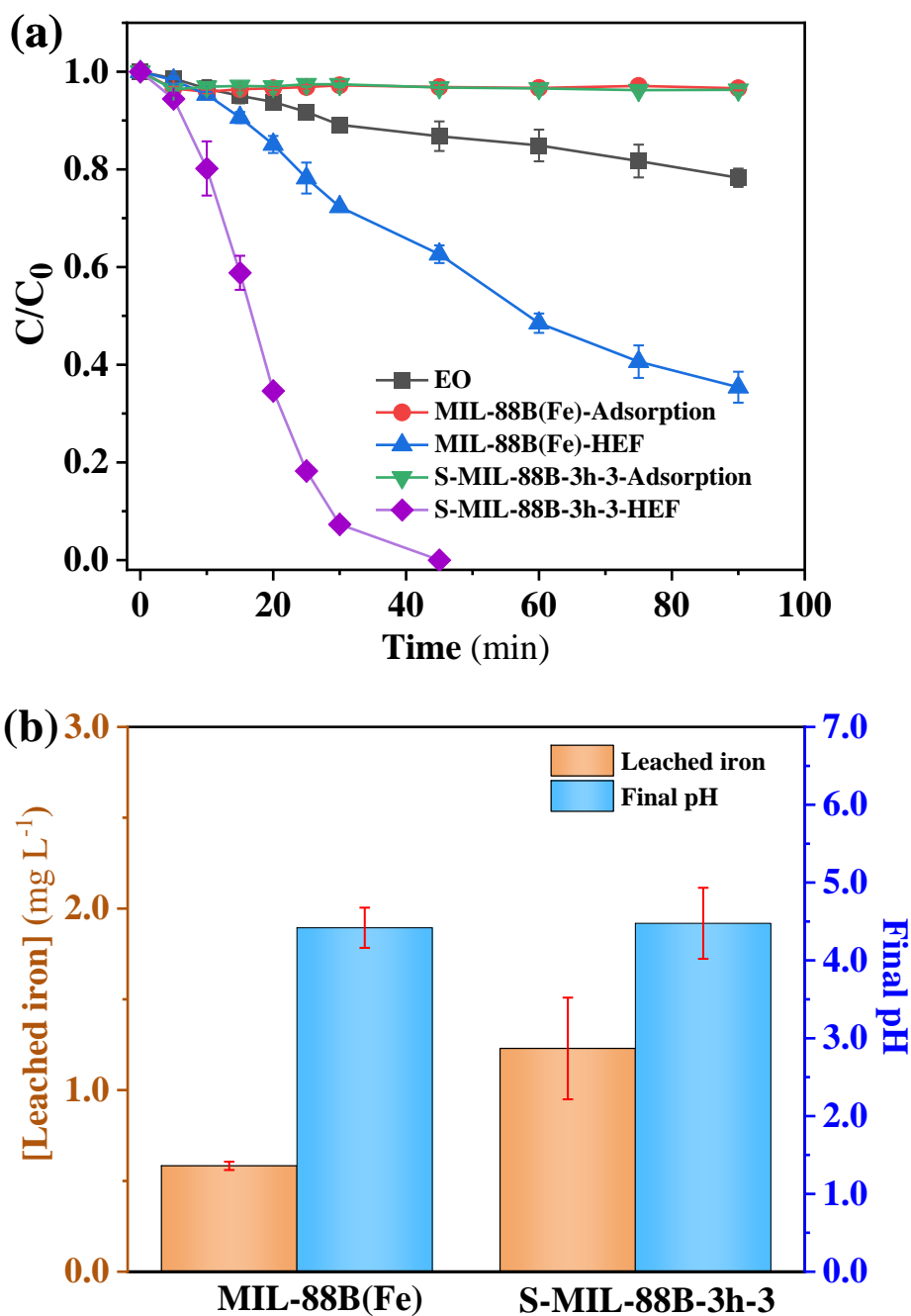


Fig. 3. (a) Normalized TMP decay during the treatment of 160 mL of 0.060 mM drug solutions with 0.05 M Na₂SO₄ under different conditions. General conditions: [Catalyst] = 0.10 g L⁻¹; current = 50 mA; initial pH 7.0; IrO₂-based anode in EO and HEF. (b) Leached iron concentrations and final pH values after 90 min of the trials MIL-88B(Fe)-HEF and S-MIL-88B-3h-3-HEF shown in plot (a).

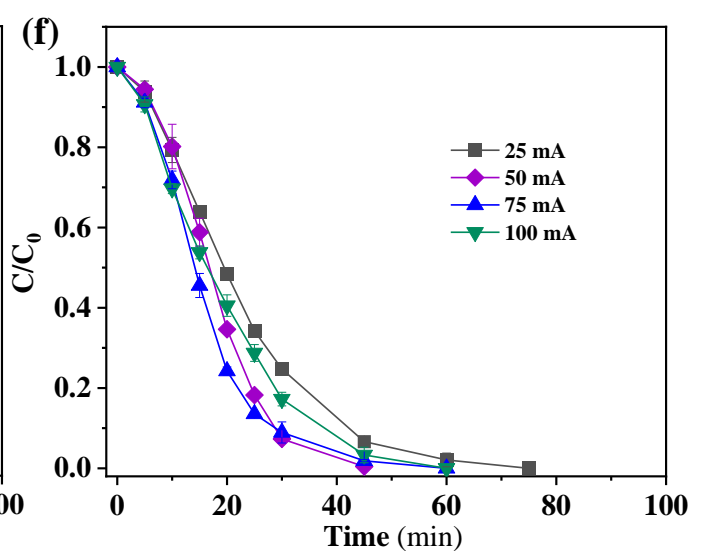
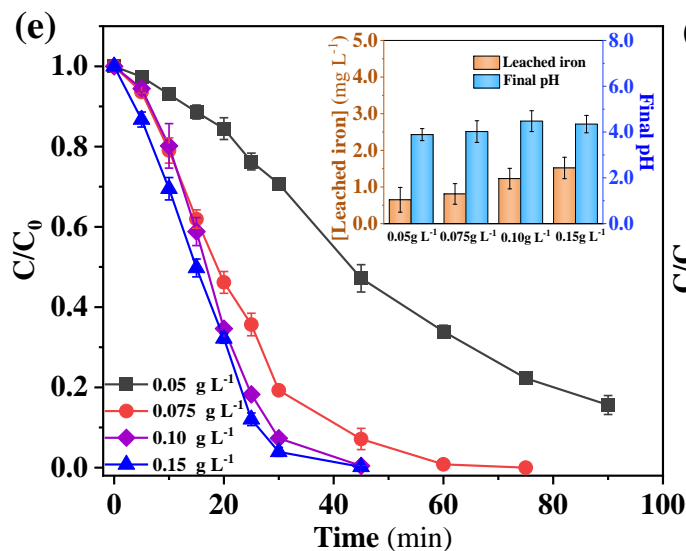
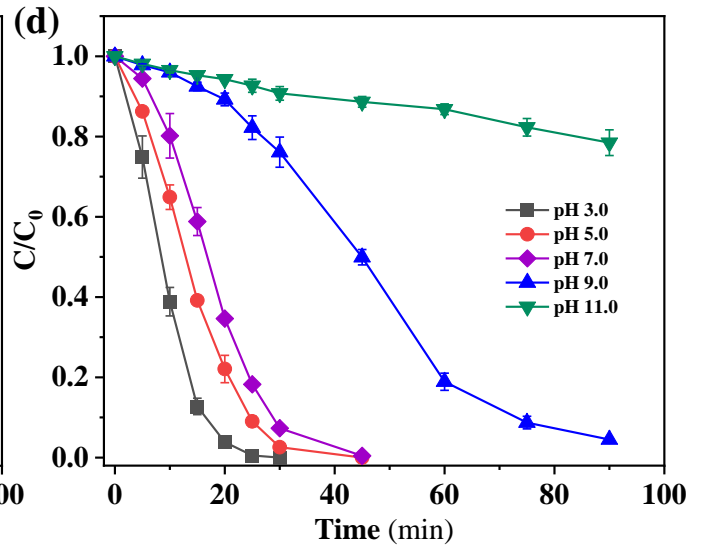
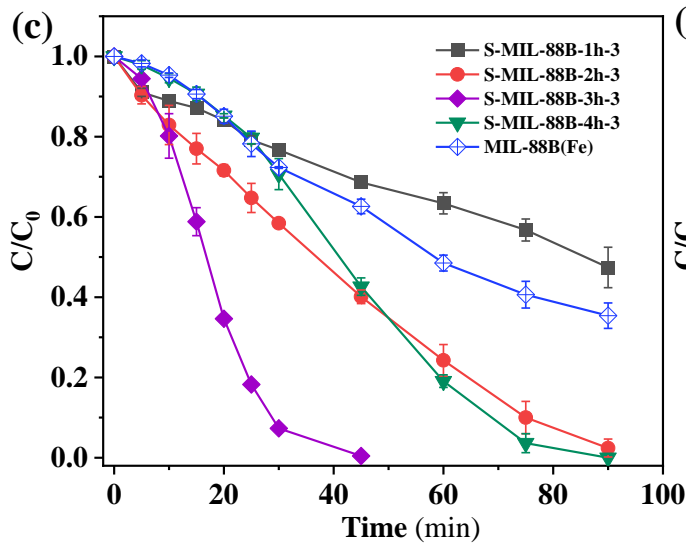
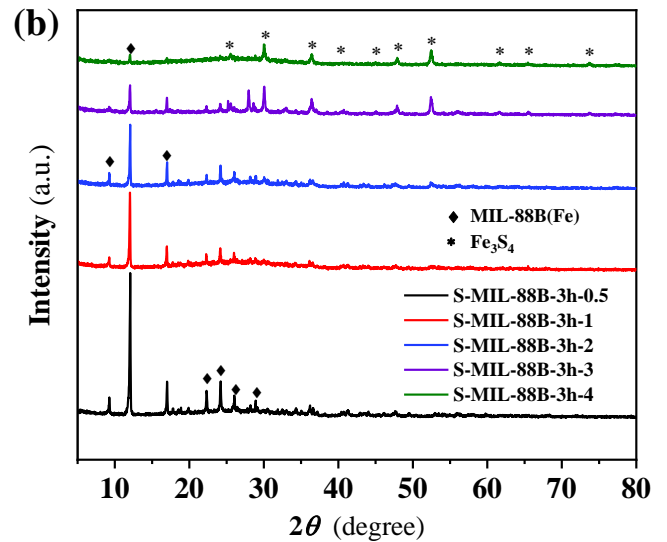
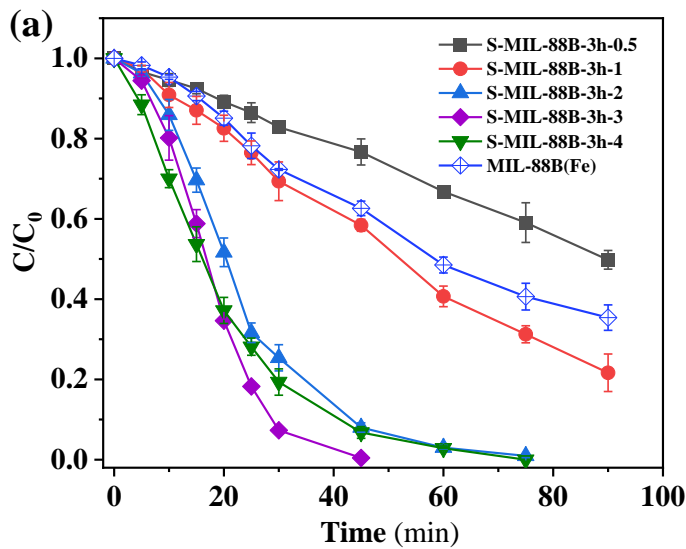


Fig. 4. (a) Effect of TAA/MIL-88B(Fe) ratio (employed for the catalyst synthesis) on the HEF performance and (b) XRD pattern for each catalyst. (c) Effect of hydrothermal treatment time (employed for the catalyst synthesis) on the HEF performance. Effects of (d) initial pH, (e) catalyst dosage and (f) applied current on TMP decay in the S-MIL-88B-3h-3-catalyzed HEF system. The inset in plot (e) shows the leached iron concentrations and final pH values after 90 min of the trials depicted in the main plot. General conditions, except when a specific parameter is modified: $[\text{TMP}]_0 = 0.060 \text{ mM}$ (+ $0.050 \text{ M Na}_2\text{SO}_4$); $[\text{catalyst}] = 0.10 \text{ g L}^{-1}$; current = 50 mA ; initial pH 7.0 ; IrO_2 -based anode.

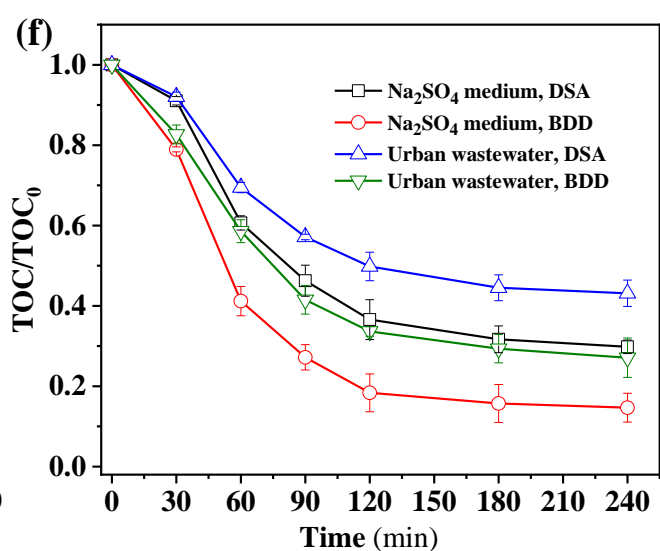
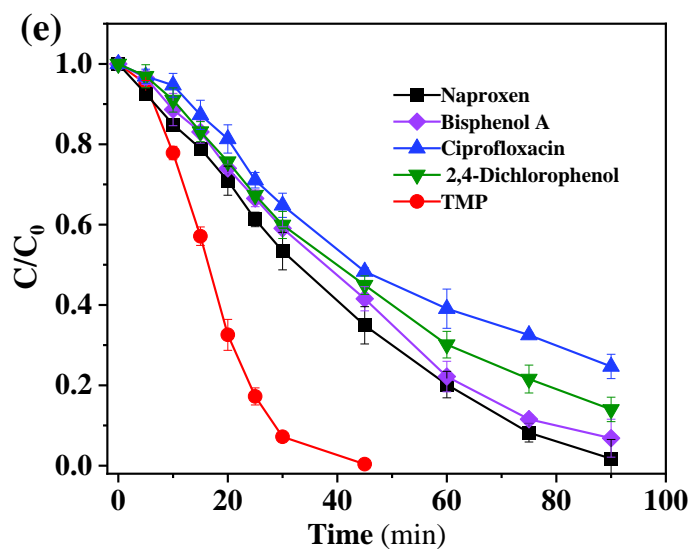
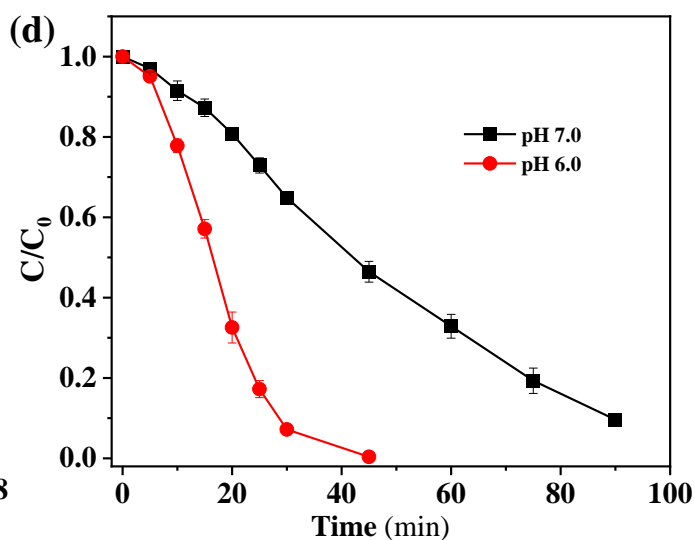
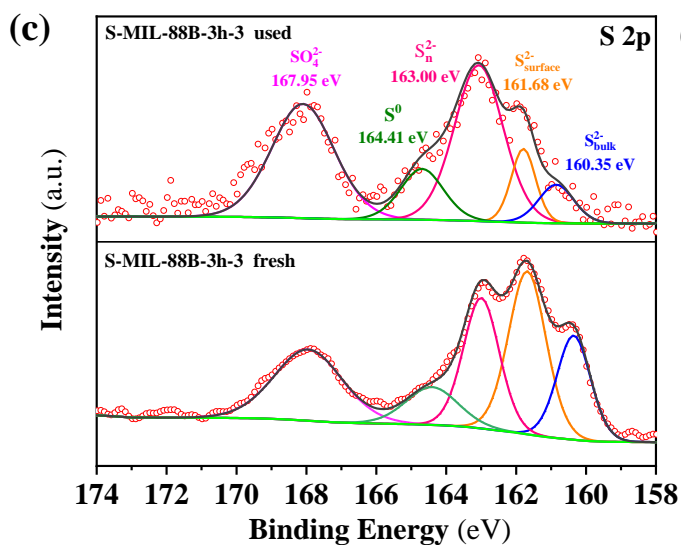
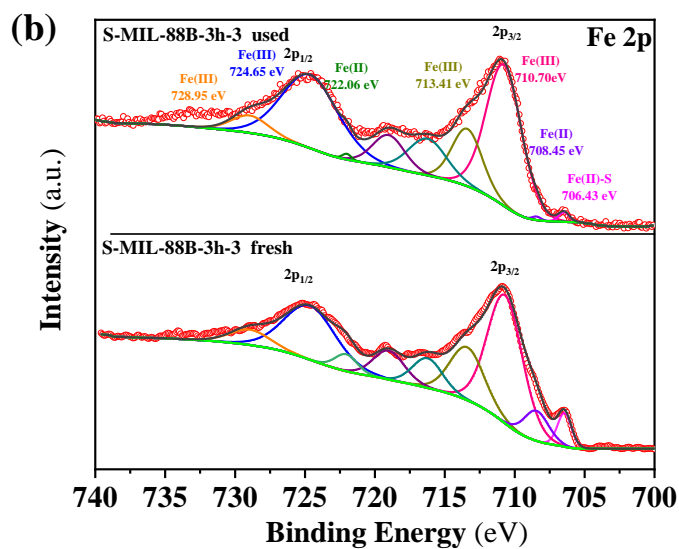
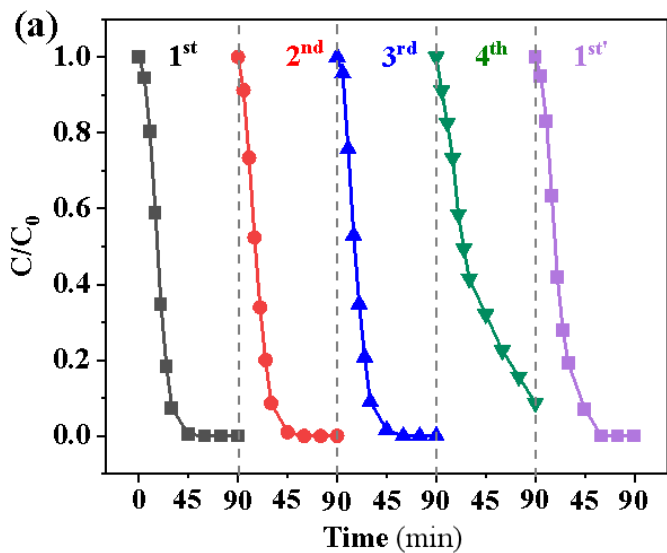


Fig. 5. (a) Reusability of S-MIL-88B-3h-3 catalyst in four consecutive 90-min HEF runs with 0.10 mg L^{-1} catalyst under the conditions described in Fig. 3a. Cycle 1st was made once the catalyst regeneration was performed at the end of the fourth cycle. (b) Fe 2p and (c) S 2p XPS spectra of fresh and used S-MIL-88B-3h-3 catalyst. (d) Treatment of TMP spiked into urban wastewater by S-MIL-88B-3h-3-catalyzed HEF at initial pH 6.0 and 7.0. (e) Normalized decay of micropollutants concentration during the HEF treatment of 160 mL of solutions containing one of the contaminants (at 10 mg L^{-1} C) spiked into urban wastewater at initial pH 6.0. (f) TOC abatement during the HEF treatment of 0.060 mM TMP solutions (using $0.050 \text{ M Na}_2\text{SO}_4$ or urban wastewater) with a DSA or BDD anode. General conditions, except when a specific parameter is modified: $[\text{TMP}]_0 = 0.060 \text{ mM}$; $[\text{catalyst}] = 0.10 \text{ g L}^{-1}$; current = 50 mA ; initial pH 7.0; IrO_2 -based anode.

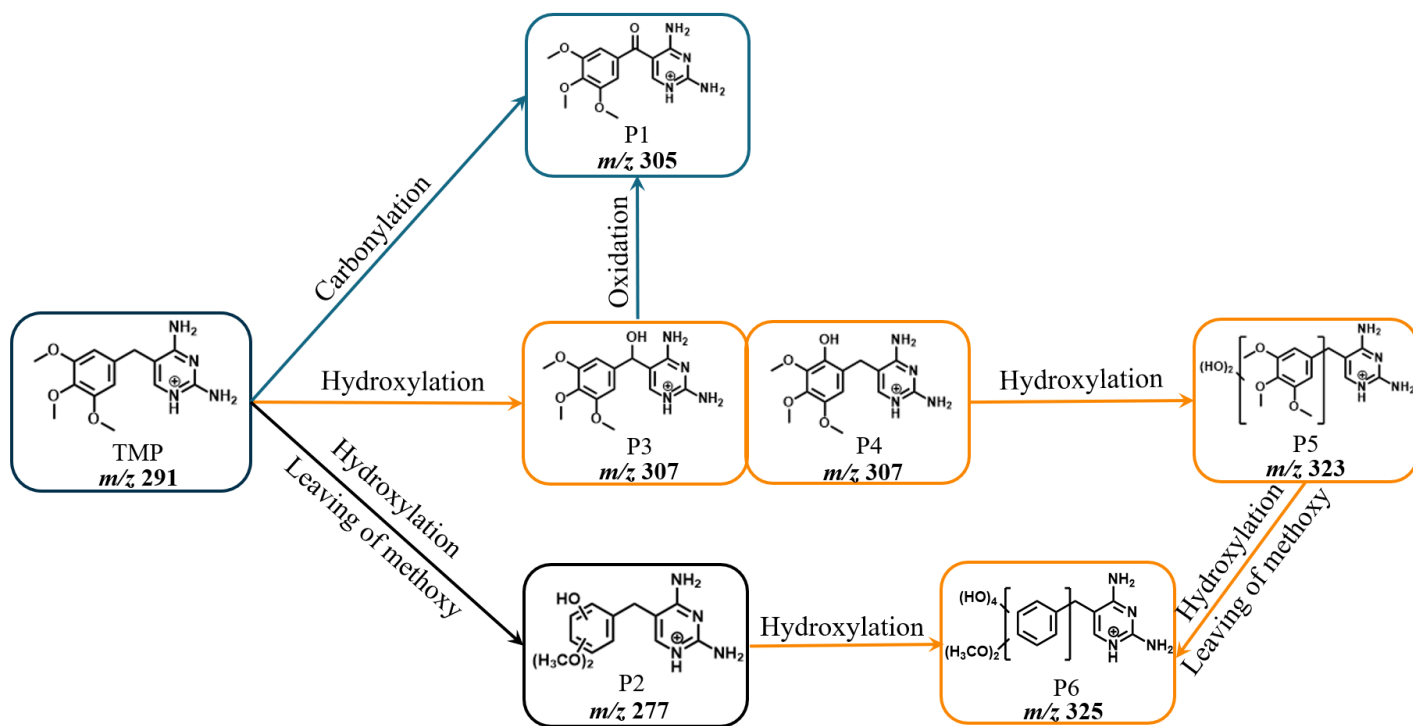


Fig. 6. Proposed routes for the degradation of TMP by S-MIL-88B-3h-3-catalyzed HEF treatment at neutral pH.

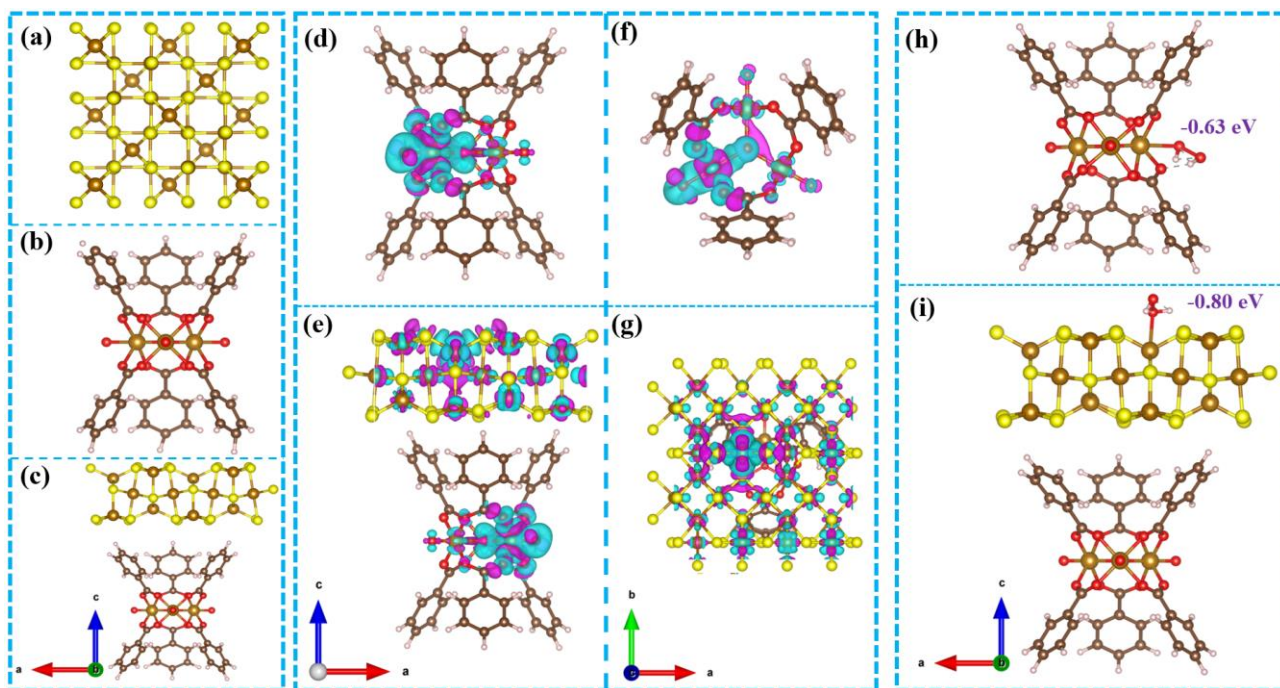


Fig. 7. Optimized structure models of (a) Fe_3S_4 , (b) MIL-88B(Fe), and (c) S-MIL-88B-3h-3. (d, e) Side and (f, g) top views of the charge density difference in (d, f) MIL-88B(Fe) and (e, g) S-MIL-88B-3h-3 (The purple regions denote charge depletion while azure regions denote charge accumulation). Side views for H_2O_2 adsorption on (h) MIL-88B(Fe) and (i) S-MIL-88B-3h-3. Color key: C (brown), O (red), H (white), Fe (orange), S (yellow).

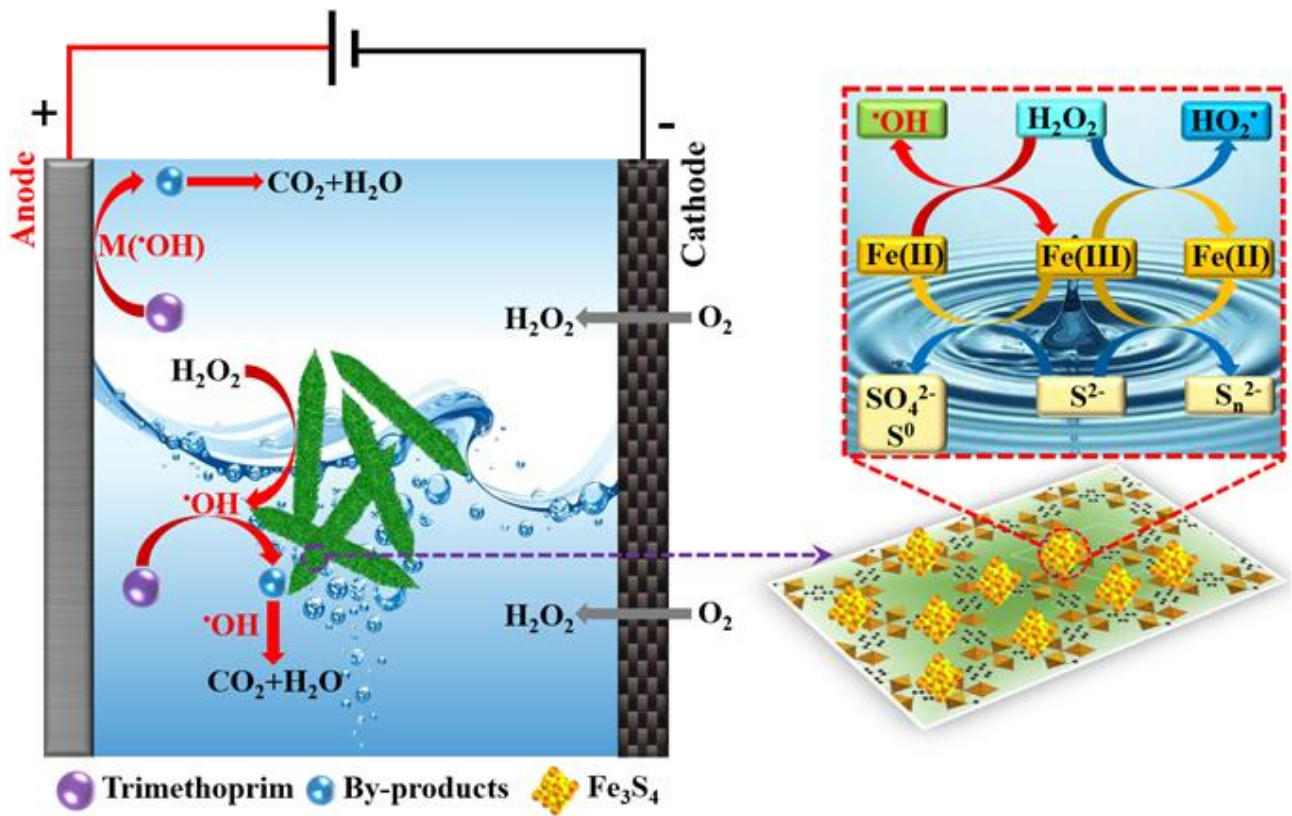


Fig. 8. Proposed mechanism for the S-MIL-88B-3h-3-catalyzed degradation of TMP by HEF treatment at mild pH.