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**ALTERATION AND CONTAMINATION OF ARCHAEOLOGICAL  
CERAMICS: THE PERTURBATION PROBLEM.**

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## ALTERATION AND CONTAMINATION OF ARCHAEOLOGICAL CERAMICS: THE PERTURBATION PROBLEM.

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### Abstract.

Alteration and contamination processes modify the chemical composition of ceramic artefacts. This is not restricted solely to the affected elements, but also affects general concentrations. This is due to the compositional nature of chemical data, enclosed by the restriction of unit sum. Since it is impossible to know prior to data treatment whether the original compositions have been changed by such processes, the methodological approach used in provenance studies must be robust enough to handle materials that might have been altered or contaminated. The ability of the logratio transformation proposed by Aitchinson to handle compositional data is studied and compared with that of present data treatments. The logratio transformation appears to offer the most robust approach.

### Key words.

Alteration, contamination, perturbation, logratio transformation, variation matrix, statistical treatment, provenance, ceramics.

### Introduction.

The two main principles of provenance studies through chemical characterisation were formally established in the 70s: On the one hand, the equation which models all sources of variation (Bieber *et al.*, 1976):

$$\text{var}_T = \text{var}_N + \text{var}_S + \text{var}_A, \quad (1)$$

where  $\text{var}_T$  is the total variance in the determination of concentration of one particular element for one individual,  $\text{var}_N$  the natural variance,  $\text{var}_S$  the sampling variance, and  $\text{var}_A$  the analytical variance (*vid.* Beier & Mommsen, 1994); and on the other hand, the provenance postulate: "...namely that there exist differences in chemical composition between different natural sources that exceed, in some recognisable way, the differences observed within a given source." (Weigand *et al.*, 1977, 24). Both principles are related and both point to compositional variability as being the basic principle in chemical characterisation.

As used in (1), the term 'natural' simplifies a more complex reality. In addition to the differences that exist between two raw materials of different origin, there are three distinct stages in pottery fabrication that must be taken into consideration as each can introduce variability through the particular technological processes involved. In the first stage, there is the selection of one or more raw materials, which contain the information of provenance (which is not necessarily the same as that of the the pottery, if trade in raw materials have occurred). In the second stage, there exists the variability introduced by the potter during the preparation of one or more pastes, depending on the particular use the pottery is to be put to (Steponaitis, 1984; Cuomo di Caprio, 1985; Arnold, 1992). Finally, the paste can be diversified during firing,

resulting in different transformations which affect mineralogy (Maggetti, 1981), chemical composition (Widemann *et al.*, 1975; Kilikoglou *et al.*, 1988), as well as physical properties including microstructure and colour (Picon, 1973; Tite & Maniatis, 1975; Dufournier, 1982; Béarat *et al.*, 1989). As a result of these changes a paste may then result in the production of one or more fabrics (adapted from Whitbread, 1989, 127). Therefore, in case studies the relation between the paste and the derived fabrics should be satisfactorily explained by a model of transformation during firing, which can then be verified by experimental work (Buxeda *et al.*, 1995). In addition to these three stages, there exists another source of variability, which is the subject of this paper. This final source of variability refers to unintentional alteration and contamination processes that take place during the phases of manufacture, use, burial, excavation, conservation and analysis.

It was at the end of the 60s and the beginning of the 70s, when the processes of alteration and contamination of pottery were first taken into consideration (Freeth, 1967; Millet, 1967; Matson, 1971; Sayre *et al.*, 1971; Duma, 1972). In subsequent years, there has been a not unexpected increase in research in this field, and considerable advances have been made (Béarat, 1990; Picon, 1991). Surprisingly, the effects of alteration and contamination processes on chemical composition have not received the same level of attention. Studies almost exclusively focus on the variations observed in the elements directly affected by these processes. As far as we know, only Picon (1986) has proposed a general correction of the elemental concentrations determined as well as recently pointing out the implications of the ‘residual distances’ that exist when we compare one individual with a previously established reference group (Picon, 1992; Morel & Picon, 1995).

The main purpose of this paper is the theoretical study of the implications that alteration and contamination processes have on elemental concentrations, and their effect on the treatment of the chemical data.

### **The perturbation problem.**

Alteration and contamination processes modify the original composition according to the properties of compositional data. The operation introduced by Aitchinson (1986, 42-43 and 123-125)

$$\mathbf{x}_1 = \mathbf{u}_1 \circ \mathbf{x}_0 = C(x_{01}u_{11}, \dots, x_{0D}u_{1D}) \quad (2)$$

is defined as perturbation. During that operation, the D-parts compositional vector  $\mathbf{x}_0$ , which we can identify with the original compositional vector of a ceramic artefact, is operated by the D-parts perturbing vector  $\mathbf{u}_1$  of positive elements. The result is the perturbed compositional vector  $\mathbf{x}_1$ .  $C$  represents the constraining operator which transforms each D-parts vector in one vector with unit sum. A generalisation of (2), for the processes that involve a sequence of compositions generated by independent successive perturbations, is possible according to the rules of the  $\circ$  operator (Aitchinson, 1992):

$$\mathbf{x}_n = \mathbf{u}_n \circ \mathbf{x} \quad (\mathbf{x} = \mathbf{x}_0; \mathbf{u} = (\mathbf{u}_n \circ \dots \circ \mathbf{u}_1) \quad (n=1,2,\dots)). \quad (3)$$

Thus, taking expression (3) as a starting point, we are able to develop a theory of alteration processes which can deal with more than one perturbation operation.

The values of the components of the perturbing vector will be in the range  $0 < u_j < 1$  when the perturbation implies a drop in the concentration of the  $x_j$  component

of the compositional vector, or  $u_j > 1$  if it implies an increment. Finally, the value will be  $u_j = 1$  if it does not imply any change. Thus, 1 is the neutral element for the perturbation. Then, the operation of perturbation of one compositional vector by one perturbing vector with all its components  $u_j = 1$  ( $j=1, \dots, D$ ), is the identity perturbation.

Now, taking (2) and (3) together, we can develop these expressions to

$$\mathbf{x}_n = \mathbf{u}^\circ \mathbf{x} = 100C(x_1 u_1, \dots, x_D u_D) = 100 \left( \frac{x_1 u_1}{\sum_{j=1}^D x_j u_j}, \dots, \frac{x_D u_D}{\sum_{j=1}^D x_j u_j} \right)$$

and, developing the denominator as

$$\sum_{j=1}^D x_j u_j = 100 + (((x_1 u_1) - x_1) + \dots + ((x_D u_D) - x_D)) = k, \quad (4)$$

we arrive to the expression

$$\mathbf{x}_n = 100 \left( \frac{x_1 u_1}{k}, \dots, \frac{x_D u_D}{k} \right) = \left( \frac{100(x_1 u_1)}{k}, \dots, \frac{100(x_D u_D)}{k} \right). \quad (5)$$

Note that in these developments the constant 100 has been introduced in order to express the data in percentage values.

According to (5), we can verify that in fact the perturbation operation in compositional data establishes two types of perturbation. The first, which we shall call direct, comes from the fact that one component  $x_j$  is multiplied by one component  $u_j$ , as is established in (2). The second, which we shall call indirect, comes from the fact that one component  $x_j$  is divided by the value  $k$  defined in (4) and is a perturbation imposed by the constraining operator. Thus, the possible sources of variation in the  $D$  components of  $\mathbf{x}_0$  are actually the direct and indirect perturbations present in all the perturbation operations.

The value  $k$ , as expressed in (4), is the result of the sum of the  $D$  components of the original compositional vector  $\mathbf{x}_0$  plus those terms  $((x_j u_j) - x_j)$  ( $j=1, \dots, D$ ) which are not cancelled when being operated by the neutral element (i.e.  $u_j \neq 1$ ). Therefore, the fact that  $k$  deviates from 100 depends only on those components of the perturbing vector other than the neutral element. Moreover, it is clear that 100 is the neutral element of the indirect operation because it cancels the indirect operation. Nevertheless, it is possible for  $k$  to assume the value of 100, if there are two or more terms  $((x_j u_j) - x_j)$  with  $u_j \neq 1$  producing equal perturbations but in opposite directions. At the same time, a discrepancy appears between the expected value from the direct perturbation operation and the observed value which arises from the final indirect operation. In this sense, the value determined by the chemical analysis is an overestimation of that value resulting from the direct perturbation if  $k < 100$  and, on the contrary, it is an underestimation if  $k > 100$ .

It is clear from the above that the validity of a methodology able to deal with perturbed data depends on its ability to avoid the effects of the indirect operations, because the latter become a source of spurious error propagation with no connection to the natural processes, but rather to the constraining operator of the compositional data. At the same time, having proved its ability to cancel the indirect operations, it would be desirable for such a methodology to facilitate the identification of the effects of the direct operations, in order that they might be recognised and taken into consideration.

## Traditional data treatments.

Traditional data treatments use the data in one of two ways. The raw data can be either used in their original values or by taking their logarithms; or some scholars normalise the subcompositions in such a way that the sum of the determined components is 100. The main reason for doing this is to achieve a better intercomparability of the elemental concentrations of the same component in two different compositional vectors. This is a common way of working on subcompositions that include the most of major and minor elements. However, it is not used at all by those who determine almost exclusively trace elements.

The compositional vectors in chemical characterisation have no  $D$  random dimensions, but rather the  $D$  dimensions are the number of elements in the Periodical System that occur naturally. However, in practice the analytical determinations are never performed for all the  $D$  components, but for a subcomposition  $S$  ( $S < D$ ) that is imposed by either the technical possibilities, the theoretical assumptions, or both factors together. Therefore, (5) can be written as

$$\mathbf{x}_{\text{Subc n}} = \left( \frac{100(x_1 u_1)}{k}, \dots, \frac{100(x_s u_s)}{k} \right). \quad (6)$$

It is important to consider that, in (6),  $k$  has the same meaning given by (4). Thus, the elemental concentrations of the determined subcomposition are affected by the direct perturbations which depend on the components  $u_j$  ( $j=1, \dots, S$ ), but they are also affected by the indirect perturbations that are dependent on all the components  $u_j$  ( $j=1, \dots, D$ ). Expression (6) actually forms the basis for those data treatments conducted on the raw data.

However, in the case where the subcomposition is normalised we start from another basis:

$$\mathbf{x}_{\text{SubcNor n}} = 100C(\mathbf{x}_{\text{Subc n}}) = 100C\left(\frac{100(x_1 u_1)}{k}, \dots, \frac{100(x_s u_s)}{k}\right).$$

Due to the constraining operator, imposed during normalisation, a second indirect operation is performed by a new value which is similar to the value  $k$  defined in (4). This new value is formed only from the values of the  $S$  components of the determined subcomposition:

$$k_{\text{Subc}} = \frac{100(x_1 u_1)}{k} + \dots + \frac{100(x_s u_s)}{k} = \frac{100}{k} ((x_1 u_1) + \dots + (x_s u_s)).$$

Thus, the resulting expression can be written as

$$\mathbf{x}_{\text{SubcNor n}} = 100 \left( \frac{\frac{100(x_1 u_1)}{k}}{k_{\text{Subc}}}, \dots, \frac{\frac{100(x_s u_s)}{k}}{k_{\text{Subc}}} \right) = \left( \frac{100(x_1 u_1)}{c}, \dots, \frac{100(x_s u_s)}{c} \right), \quad (7)$$

where  $c$  corresponds to

$$c = (x_1 u_1) + \dots + (x_s u_s). \quad (8)$$

Expressions (7) and (8) allow us to confirm the intuitive idea that the normalisation of the subcompositions produces new values that are independent of the undetermined components and, more importantly, that are independent of those undetermined components of the perturbing vector. In spite of this corrective effect, other problems exist in using the normalised subcompositions, because the normalisation finally multiplies each component of the determined subcomposition by a scale factor

$$a = \frac{100}{c}, \quad (9)$$

where  $c$  has the meaning defined by (8).

These developments clearly show that working with the elemental concentration of the determined subcompositions, either with the raw data, or with the normalised subcompositions, implies several serious problems, mainly because the determined concentrations depend, through the indirect operation, on the value  $k$  defined by (4) for the raw data, or on the scale factor  $a$  defined by (9) for the normalised subcompositions.

On top of these problems, two other objections need to be raised. First, intra-vector ratios are maintained for those components directly operated by the same value in the perturbing vector, but not necessarily for the inter-vector ratios. Expressed as the product of the original ratio multiplied by a new ratio due to the perturbation, the inter-vector ratio between compositional vectors  $A$  and  $B$  becomes

$$r_{ABj} = \frac{X_{Aj}}{X_{Bj}} \frac{\frac{100u_{Aj}}{k_A}}{\frac{100u_{Bj}}{k_B}} \quad (j = 1, \dots, S),$$

in the raw data case, and

$$r_{Subc ABj} = \frac{X_{Aj}}{X_{Bj}} \frac{u_{Aj}a_A}{u_{Bj}a_B} \quad (j = 1, \dots, S),$$

in the normalised subcomposition case, exhibiting their dependence to  $k$  (4) and to  $a$  (9), which can differ for each compositional vector.

Secondly, during the definition of compositional groups it is necessary to estimate the distribution function parameters. If we assume, for example, that this function fits a normal multivariate function, the parameters mean, variance and covariance will be estimated. Therefore, as it easily demonstrated, the value  $k$  (4) for raw data, or the scale factor  $a$  (9) for normalised data, will be used in a recurrent way in every step of these calculations. Thus the estimation of these parameters represents a serious source of error propagation.

It has been shown so far that the traditional methods of chemical data treatment cannot handle perturbations. This inability is especially important because it is an axiom that all the compositional vectors of the ceramic individuals analysed are possibly perturbed but those perturbations are unknown before the chemical data have been studied. Then, the methodology employed should be robust enough to deal with perturbed data, and situations where the data are not perturbed must be seen as particular cases in the general theory, as being operated by the identity perturbation.

### **Aitchinson's proposals for using ratios.**

Besides the perturbation, another major problem of traditional data treatment methods arises from the absence of an interpretable covariance structure and from the difficulties involved in parametric modelling (Aitchinson, 1986, 52 onwards). To tackle these problems Aitchinson (1986, 1989, 1990, 1992) has proposed the use of

ratios. In fact, the logarithms of these ratios are used in order to achieve the desired symmetry (Aitchinson, 1992).

Aitchinson's proposals are based on the use of the symmetric centred logratio transformation according to

$$\mathbf{x} \in S^d \rightarrow \mathbf{z} = \log\left(\frac{\mathbf{x}}{g(\mathbf{x})}\right) \in R^D \quad (10)$$

where  $S^d$  is the d-dimensional simplex ( $d=D-1$ ) and  $g(\mathbf{x})$  is the geometric mean of all the  $\mathbf{x}$  D components, and on the use of the asymmetric logratio transformation according to

$$\mathbf{x} \in S^d \rightarrow \mathbf{y} = \log\left(\frac{\mathbf{x}_{-D}}{x_D}\right) \in R^d \quad (11)$$

where  $\mathbf{x}_{-D}=(x_1, \dots, x_d)$ .

The impact of these proposals on archaeometry has, however, been limited and, additionally, they have always been related, sometimes in a critical sense, to the symmetric centred logratio transformation (10) (Baxter, 1989, 1991, 1992, 1993, 1994; Leese *et al.*, 1989; Tangri & Wright, 1993; Neff, 1994; Hoard *et al.*, 1995). In contrast, our efforts have been directed to the study and use of the asymmetric logratio transformation (11) because, as we shall see, the disadvantages arising from asymmetry can be kept under control (Buxeda, 1995a, 1995b; Buxeda & Cau, 1995a; Buxeda & Gurt, 1995; Buxeda *et al.*, 1995).

Based on the preceding discussion, the centred logratio transformation can be expressed as follows:

$$\mathbf{z}_{\text{Subc}} = \left( \ln\left(\frac{100(x_1 u_1)}{\left(\prod_{j=1}^s \frac{100(x_j u_j)}{k}\right)^{\frac{1}{s}}}\right), \dots, \ln\left(\frac{100(x_s u_s)}{\left(\prod_{j=1}^s \frac{100(x_j u_j)}{k}\right)^{\frac{1}{s}}}\right) \right).$$

Developing the denominator and simplifying the initial expression, this expression can be written as:

$$\mathbf{z}_{\text{Subc}} = \left( \ln\left(\frac{x_1}{\left(\prod_{j=1}^s x_j\right)^{\frac{1}{s}}}\right) + \ln\left(\frac{u_1}{\left(\prod_{j=1}^s u_j\right)^{\frac{1}{s}}}\right), \dots, \ln\left(\frac{x_s}{\left(\prod_{j=1}^s x_j\right)^{\frac{1}{s}}}\right) + \ln\left(\frac{u_s}{\left(\prod_{j=1}^s u_j\right)^{\frac{1}{s}}}\right) \right). \quad (12)$$

So, in (12) we can observe that the centred logratio transformation removes the indirect perturbation, and it does not imply any arbitrary change of scale as normalisation would. Nevertheless, a new indirect operation, in the second term of the sum of logarithms for each component, arises, imposed by the use of ratios, and involves all the determined components of the perturbing vector.

In contrast, the logratio transformation gives more simple equations. The initial equation being

$$\mathbf{y}_{\text{Subc}} = \left( \ln\left(\frac{100(x_1 u_1)}{k}\right), \dots, \ln\left(\frac{100(x_{s-1} u_{s-1})}{100(x_s u_s)}\right) \right),$$

after simplifying the expression we obtain

$$\mathbf{y}_{\text{Subc}} = (\ln(\frac{X_1}{X_S}) + \ln(\frac{u_1}{u_S}), \dots, \ln(\frac{X_{S-1}}{X_S}) + \ln(\frac{u_{S-1}}{u_S})). \quad (13)$$

As can be seen, in this transformation once the indirect perturbation imposed by the compositional nature of the data has been removed, another indirect operation imposed by the use of ratios appears. Unlike the centred logratio transformation, here the second term in the sum of logarithms in each component is only affected in the indirect operation by the Sth component used as divisor.

The main implication of these various indirect operations in the two transformations can be seen in the inter-vector ratios. In the case of the intra-vector ratios, two components directly operated by the same value do not change the ratio. In the case of two components of two different compositional vectors A and B the inter-vector centred logratio transformed data ratios are the result of

$$r_{zABj} = (\ln(\frac{X_{Aj}}{(\prod_{m=1}^S X_{Am})^{\frac{1}{S}}}) - \ln(\frac{X_{Bj}}{(\prod_{m=1}^S X_{Bm})^{\frac{1}{S}}})) + (\ln(\frac{u_{Aj}}{(\prod_{m=1}^S u_{Am})^{\frac{1}{S}}}) - \ln(\frac{u_{Bj}}{(\prod_{m=1}^S u_{Bm})^{\frac{1}{S}}})) \quad (14)$$

where  $j=1, \dots, S$ . In the case of logratio transformed data, the inter-vector ratios are the result of

$$r_{yABj} = (\ln(\frac{X_{Aj}}{X_{AS}}) - \ln(\frac{X_{Bj}}{X_{BS}})) + (\ln(\frac{u_{Aj}}{u_{AS}}) - \ln(\frac{u_{Bj}}{u_{BS}})) \quad (15)$$

where  $j=1, \dots, S-1$ . It must be noticed that in (14) as in (15) the subtraction on the left-hand side of the sum corresponds to the ratio between the original compositional vectors before the perturbation operation, while the subtraction on the right-hand side of the sum expresses the contribution of the direct and indirect operations. Thus it is clear that inter-vector ratios are only dependent on the perturbing vectors and hence not on the result of the calculation of  $k$  (4) or  $a$  (9) using both the perturbing and the compositional vectors. Furthermore, recovering the original inter-vector ratios depends, in the case of the symmetric transformation, on the equality of the values of the components of the perturbing vector used in the direct operation, and on the equality of the geometric mean of all the values of the components of the perturbing vector corresponding to the determined subcomposition. But, in the asymmetric transformation the conditions are less severe, because, once the equality in the direct operation has been proved, the equality in the indirect operation will only depend on the values of the Sth component of the perturbing vectors.

An important implication is that the inter-vector ratios (14) and (15) correspond to the form used in the calculation of the Euclidean distance (Aitchinson, 1992), which is

$$d_{AB}^2 = \sum_{j=1}^S r_{zABj}^2 \quad \text{and} \quad d_{AB}^2 = \sum_{j=1}^{S-1} r_{yABj}^2$$

for the centred logratio and for the logratio transformed data, respectively.

Moreover, the parameters of mean, variance and covariance that are estimated present the same advantages as the inter-vector ratios with respect to the raw and normalised data. Nevertheless, as can be easily seen the logratio transformation is more robust on the spurious error propagation induced by the indirect perturbations. In

the case of the asymmetric transformation, the calculation of the mean, variance and covariance statistics will be:

$$m_{y_j} = \frac{1}{N} \sum_{i=1}^N \left( \ln\left(\frac{x_{ij}}{x_{is}}\right) + \ln\left(\frac{u_{ij}}{u_{is}}\right) \right), \quad (16)$$

$$\text{var}_{y_j} = \frac{1}{N-1} \sum_{i=1}^N \left( \left( \ln\left(\frac{x_{ij}}{x_{is}}\right) + \ln\left(\frac{u_{ij}}{u_{is}}\right) \right) - m_{y_j} \right)^2, \quad (17)$$

where (j=1,...,S-1), and

$$\text{cov}_{y_{jl}} = \frac{1}{N-1} \sum_{i=1}^N \left( \left( \ln\left(\frac{x_{ij}}{x_{is}}\right) + \ln\left(\frac{u_{ij}}{u_{is}}\right) \right) - m_{y_j} \right) \left( \left( \ln\left(\frac{x_{il}}{x_{is}}\right) + \ln\left(\frac{u_{il}}{u_{is}}\right) \right) - m_{y_l} \right), \quad (18)$$

where (j=1,...,S-2) and (l=j+1,...,S-1).

The development of the expression for the inter-vector ratios, and for the statistics mean, variance and covariance, allows us, using Aitchinson's proposals, to express the values of any perturbed compositional vector as the sum of the original value plus the corresponding value from the perturbing vectors. Furthermore, dealing with the asymmetric transformation, the indirect operation is only dependent on the value of the Sth component of the perturbing vector. Therefore, provided that this value assumes the neutral element for all the individuals analysed, the spurious error propagation due to the indirect operations will be eliminated and we can recover the original unknown values, except for the presence of direct perturbation. This spurious error propagation for the centred logratio or logratio transformed data will depend only on the addition of the effect of the perturbing vector. On the contrary, for raw data and normalised subcompositions the indirect operation comes from the result of the different element  $x_i u_j$ , according to (4) or (9) respectively, and the effect of the indirect operations will be directly proportional to the  $x_i$  values.

The ability of logratio transformation to emphasise the presence of perturbation, allowing it to be identified, as well as its ability to identify which elements are more suitable for use as divisors in (13), in order to cancel the indirect perturbations, will now be exemplified using an archaeological case study of Hispanic Terra Sigillata kiln material, which presents heavily perturbed data.

### **The Abella workshop: an example of perturbed data.**

The Abella workshop (Navès, Solsonès) is situated in what is now Catalonia (Spain), in the north-east of the Iberian Peninsula. It constituted the first known workshop of Hispanic Terra Sigillata (Samian Ware). Discovered in 1912, a partial excavation was undertaken by Serra i Vilaró (Serra, 1925) during the first years of this century. As a result of this excavation, three kilns were discovered that belonged to a production centre of Terra Sigillata and common pottery. Moreover, some elements of the kiln were recovered, such as the gas extraction tubes used in irradiation kilns to isolate the firing chamber in order to achieve the completely oxidising atmosphere needed to produce the red Terra Sigillata (Picon, 1973). A new survey led to the discovery of a fourth kiln and a great variety of archaeological materials (Gurt *et al.*, 1987; Gurt, 1993a; Casas *et al.*, 1989; Buxeda, 1995a). The survey was conducted in a number of areas (Figure 1) which correspond to the four kilns (U2, F1, F2 and B) and to a further four sectors (E, Q2, G and A). The chronology of the workshop was

estimated as being the second half of the 2nd century - first half of the 3rd century AD, thanks to the results provided by the Roman villa of La Rectoria, ca. 500 m away from the workshop, where the Abella products were found in a clear stratigraphical sequence. Also, a  $^{14}\text{C}$  dating exists for the UE 7 stratigraphical unit (Gurt, 1993b; Buxeda, 1995a).

### **Sampling and analytical methods.**

The sampling, conducted in order to define the Abella reference group, included 108 individuals (Table 1), representing the Terra Sigillata, the moulds, the gas extraction tubes and the fine common pottery. All but one individual came from deposition contexts in the areas surveyed in Abella. Only one individual came from the La Rectoria site. However, the deposition context of 18 of the 107 individuals from the Abella site is unknown, because of earlier excavations.

Ten grams of each individual were taken and powdered in a Spex Mixer (Mod. 8000) tungsten carbide cell mill, after the outer surfaces had been mechanically removed. The chemical compositions of the 108 individuals were determined at the Scientific-Technical Services of the University of Barcelona with X-ray Fluorescence (XRF), using a Phillips PW 1400 spectrometer, with two excitation sources: Rh and Au. The quantification of the concentrations was obtained using a calibration line performed with 40 International Geological Standards. The elements determined were:  $\text{Fe}_2\text{O}_3$  (as total Fe),  $\text{Al}_2\text{O}_3$ , MnO,  $\text{P}_2\text{O}_5$ ,  $\text{TiO}_2$ , MgO, CaO,  $\text{Na}_2\text{O}$ ,  $\text{K}_2\text{O}$ ,  $\text{SiO}_2$ , Ba, Rb, Mo, Th, Nb, Pb, Zr, Y, Sr, Sn, Ce, Co, Ga, V, Zn, W, Cu and Ni. The loss on ignition (LOI) was measured by firing 0.5 g, of dried powder, at  $1000^\circ\text{C}$  for 1 h. Moreover, X-ray Diffraction analysis (XRD) was carried out for the 108 individuals included in the study, using the same powders prepared for XRF analysis. Measurements were performed at the Scientific-Technical Services of the University of Barcelona using a Siemens D-500 diffractometer working with the Cu K- $\alpha$  radiation ( $\lambda=1.5406\text{\AA}$ ), and monochromator graphite in the diffracted beam, at 1.2 kW (40kV, 30 mA). Spectra were taken from  $4$  to  $70^\circ 2\Theta$ , at  $1^\circ 2\Theta/\text{min}$  (step size= $0.05^\circ 2\Theta$ ; time=3 s). Individual 25 was chosen for a thermodiffractometric experiment, using the Siemens D-500 diffractometer equipped with a high temperature chamber and a Positional Sensitive Detector (PSD). Several spectra were taken at room temperature, 600, 700, 750, 800, 850, 900, 950, 1000, 1050 and  $1100^\circ\text{C}$ . A rate of  $100^\circ\text{C}/\text{h}$  was employed, and the temperature was kept for 1 h before the spectra were recorded. Individuals 1, 3, 6, 11, 13, 18, 24, 25, 26, 28, 29, 31, 32, 46 and 55 were chosen for the study of the microstructure and sintering state presented in its as-received-state (ARS). The observations were made on fresh fracture using a scanning electron microscopy (SEM) Phillips-SEM 515 (Laboratory of Archaeometry, NCSR "Demokritos", Aghia Paraskevi, Greece), and an SEM Stereoscan S120 (Cambridge Instruments) (Scientific-Technical Services, University of Barcelona). Four individuals (1, 6, 11 and 46) were also refired in oxidising atmosphere, using a rate of  $200^\circ\text{C}/\text{h}$  from room temperature up to 850, 950, 1080 and  $1100^\circ\text{C}$ , maintaining the temperature for 1 h and with a natural cooling process. A detailed description of the analytical conditions, precision, accuracy, and routine is given by Buxeda (1995a).

### **The study of elemental concentrations: the variation matrix.**

As established by Aitchinson (1986), the covariance structure in compositional data for a D-parts composition  $\mathbf{x}$  is the group of all the covariances

$$\sigma_{ij,kl} = \text{cov} \{ \log(x_i/x_k), \log(x_j/x_l) \} \quad (i,j,k,l=1,\dots,D).$$

Following this definition for covariance, the variances, representing the relative variations between two components, are defined as

$$\tau_{ij} = \sigma_{ii,jj} = \text{var} \{ \log(x_i/x_j) \}.$$

Furthermore, the covariance structure of a D-parts composition  $\mathbf{x}$  is actually completely determined by the previous  $1/2dD$  variances. Thus the  $D \times D$  matrix

$$\mathbf{T} = [\tau_{ij}] = [\text{var} \{ \log(x_i/x_j) \} : i,j=1,\dots,D] \quad (19)$$

which completely determines the covariance structure is called the variation matrix (Aitchinson, 1986, 1990).

If we develop Aitchinson's concepts for an S-parts subcomposition applying a logratio transformation, it is clear that given the relation  $\tau_{is} = \sigma_{ii,ss}$ , the values in the Sth column of the variation matrix are the same as those in the diagonal of the logratio covariance matrix calculated using the component  $x_s$  as divisor:

$$\boldsymbol{\Sigma} = [\sigma_{ij,ss}] = [\text{cov} \{ \log(x_i/x_s), \log(x_j/x_s) \} : i,j=1,\dots,S-1]. \quad (20)$$

It has to be pointed out that this correspondence is only partial, because the logratio covariance matrix (20) does not contain the variance  $\tau_{ss}$ , because it contains one dimension less. Even so, given  $\tau_{ss}=0$ , we can calculate a new value as

$$\tau_{.s} = \sum_{i=1}^S \tau_{is} \quad (21)$$

which corresponds to the value  $\text{tr}(\boldsymbol{\Sigma})$ , i.e. the total variance in the logratio covariance matrix.

Another important concept arising from the variation matrix (19) is the total variation (Aitchinson, 1990), given by

$$vt = (2S)^{-1} \mathbf{j}' \mathbf{T} \mathbf{j},$$

where  $\mathbf{j}$  is the  $S \times 1$  column vector of units. This total variation is the measure of the variability existing in the covariance structure for the subcompositional data matrix under study. The importance of the total variation concept is enhanced by the relation between the total variation and the trace of the logratio covariance matrix (20)

$$vt = \text{tr}(\boldsymbol{\Sigma}) - S^{-1} \mathbf{j}' \boldsymbol{\Sigma} \mathbf{j},$$

where  $\mathbf{j}$  is the  $(S-1) \times 1$  column of vector units, and therefore  $vt$  always assumes a lower value than  $\text{tr}(\boldsymbol{\Sigma})$ . The variation matrix will then allow us to measure the variability linked to the component used as divisor in (11), because the value

$$vt/\tau_{.s} \quad (\tau_{.s} = \text{tr}(\boldsymbol{\Sigma}))$$

can be considered the percentage of  $\text{tr}(\boldsymbol{\Sigma})$  explained by the total variation in the covariance structure, the subtraction  $1 - (vt/\tau_{.s})$  being the variability imposed on  $\boldsymbol{\Sigma}$  by the component  $x_s$  due to its special role in the asymmetric transformation (11). In this way, the variation matrix (19) will exhibit in its columns  $i$  ( $i=1,\dots,S$ ) the diagonals of the S possible logratio matrices that will result when using the component in the  $i$ th column as the divisor.

The variation matrix from Abella (Table 2), adapted in accordance with Aitchinson's proposal, exhibits in its columns the diagonals of all the possible logratio covariance matrices, and the values  $\tau_{.i}$  ( $i=1,\dots,S$ ) (21) corresponding to the traces of these logratio covariance matrices (Mo, Pb, Sn and Cu are not included due to undeterminations and analytical imprecision; Co, W and LOI will be considered

separately). The total variation is 1.07713. Two groups of elements can be observed. On the one hand, there are some components that, when used as divisors impose a low variability on the transformed data without greatly exceeding the total variation of the covariance structure. The use of SiO<sub>2</sub>, Y, Fe<sub>2</sub>O<sub>3</sub> and Al<sub>2</sub>O<sub>3</sub> as divisors keeps  $vt/\tau_i$  higher than 90%, and therefore they impose a variability below 10%. On the contrary, P<sub>2</sub>O<sub>5</sub>, CaO, Ba, K<sub>2</sub>O, Sr and Na<sub>2</sub>O give  $vt/\tau_i$  values below 50%, i.e. they impose a variability over 50%. These latter values reflect major relative variations between the components used as divisor and the other components determined, which is unexpected in a monogenic sample such as that from Abella. So, the variance matrix shows a covariance structure with a clear influence of these components, indicating their responsibility for most of the existing variability.

When SiO<sub>2</sub> is used as divisor in the transformation (11), because it is the component which imposes least variability, the logratio covariance matrix trace is 1.150966 (value of  $\tau_{\text{SiO}_2}$ ). However, the sum of the relative variations of the previous six components (P<sub>2</sub>O<sub>5</sub>, CaO, Ba, K<sub>2</sub>O, Sr and Na<sub>2</sub>O) with SiO<sub>2</sub> has a value of 0.898434, i.e. 78.06% of the total variability in the logratio covariance matrix. If we observe, for example, the histograms of the values  $\ln(\text{Na}_2\text{O}/\text{SiO}_2)$ ,  $\ln(\text{K}_2\text{O}/\text{SiO}_2)$  and  $\ln(\text{Sr}/\text{SiO}_2)$  (Figure 2), we see that some important asymmetries are present. These asymmetries are unexpected as we assume a normal multivariate distribution function, where a normal univariate must be observed for all the marginal. These asymmetries are at the origin of the high value of the corresponding variances. Furthermore, the highest values in all the variation matrix are observed in relative variations with Na<sub>2</sub>O,  $\tau_{\text{Sr Na}_2\text{O}}$  and  $\tau_{\text{K}_2\text{O Na}_2\text{O}}$ , because the individuals involved in these asymmetries are either the same in opposite directions, or different in the same direction (Figure 2). Finally, it is important to notice that two values appear markedly lower in the column of Sr,  $\tau_{\text{CaO Sr}}$  and  $\tau_{\text{Ba Sr}}$ .

These results show that the variation matrix is a powerful tool for quantification of the total variation in the compositional data matrix, and also for the identification of the origin of this variability. Certain aspects of this variability can be studied and controlled.

The variability imposed by the component used as divisor in (11) is not the only distortion that this transformation can introduce because of its special role. A second problem arises in the form of distortion of the general behaviour of the components in the covariance structure, a distortion which is due to the relations existing between these components and the component used as divisor. A measure of this distortion can be established with a correlation coefficient  $r_{v,\tau}$  between the  $\tau_{ji}$  ( $j=1,\dots,i-1,i+1,\dots,S$ ) values in the  $i$ th column and the  $\tau_j$  ( $j=1,\dots,i-1,i+1,\dots,S$ ) values of the totals of the other columns, 1 being the value for no distortion. In the case of Abella, the highest correlation is exhibited by the component SiO<sub>2</sub>, while the lowest is exhibited by the component Sr. In Figure 3 we can clearly see that the relative variations of all the components with SiO<sub>2</sub> are in good agreement with the relative variations of each component with all the others. On the contrary, the election of Sr as divisor imposes almost 82% of the variability on the logratio covariance matrix, and it also implies a distortion when reproducing the relative variations.

The result of the data treatment can be summarised in the dendrogram of the cluster analysis (Figure 4) performed using the components Fe<sub>2</sub>O<sub>3</sub>, Al<sub>2</sub>O<sub>3</sub>, MnO, P<sub>2</sub>O<sub>5</sub>,

TiO<sub>2</sub>, MgO, CaO, Na<sub>2</sub>O, K<sub>2</sub>O, SiO<sub>2</sub>, Ba, Rb, Zr, Sr and V, logratio transformed using SiO<sub>2</sub> as divisor. The cluster analysis has been performed, running the program Clustan (Wishart, 1987), using the mean squared Euclidean distance in order to emphasise the effect of those variables that, after the transformation, present a higher contribution to the variability. The centroid agglomerative algorithm was used because the few reversals do not imply any major transgression of the monotone invariance (Sneath & Sokal, 1973, 278) and, on the contrary, this algorithm has an interesting geometric reflection (Sneath & Sokal, 1973, 234). The value of the cophenetic correlation coefficient is 0.84, which reflects a high hierarchy within the data.

If we centre our attention on what now appears to be more important aspects, we can see a complex structure in the data with 79 out of 108 individuals placed in 4 groups (GA, GB, GC and GE). Table 3 shows the mean and standard deviations for the transformed data in each group, while Table 4 shows the mean and standard deviations for those groups but expressed in normalised subcompositions. In Table 3, we can see that the values  $\ln(\text{Na}_2\text{O}/\text{SiO}_2)$  are clearly higher for the group GE, while the values  $\ln(\text{K}_2\text{O}/\text{SiO}_2)$  are much lower. This explains the high value  $\tau_{\text{K}_2\text{O Na}_2\text{O}}$ , produced by the two asymmetries in opposite directions but affecting the same individuals, roughly those in the group GE. In relation to the components, CaO, Ba and Sr, we observe that the values  $\ln(\text{CaO}/\text{SiO}_2)$ ,  $\ln(\text{Ba}/\text{SiO}_2)$  and  $\ln(\text{Sr}/\text{SiO}_2)$  are markedly higher for group GA, where those individuals involved in the asymmetries exhibited by these three components are grouped. Finally, groups GB and GC represent those individuals not involved in any of these important relative variations. The differences between both groups are less significant, as is reflected in the dendrogram (Figure 4).

The component P<sub>2</sub>O<sub>5</sub>, which also makes a major contribution to the compositional variability, exhibits its special behaviour because of individual 14 (extreme right in the dendrogram) which presents a value of 2.20% in normalised subcompositions while all other values are below 0.37%.

### **The interpretation of the existing structure.**

Almost all the individuals exhibit an XRD pattern that can be related to one of the four categories of associations of crystalline phases proposed in Figure 5, according to the observed mineralogical changes. This evolution is supported by the high temperature experiment conducted on individual 25 (Figure 6), which exemplifies mineralogical category C1 in Figure 5, and by the results from SEM on the individuals ARS and the experiments of refiring (Buxeda, 1995a; Buxeda & Cau, 1995a). The equivalent firing temperatures were estimated from the data obtained by XRD and SEM, and can be divided into four groups: below 800-850°C for C1 (low fired), around 950°C for C2 (well fired) (crystallisation of gehlenite, pyroxene and plagioclase), between 1000 and 1050°C for C3 (overfired) (decomposition of illite-muscovite and gehlenite, further development of pyroxene and plagioclase) and over 1100-1150°C for C4 (severely overfired) (partial decomposition of quartz, crystallisation of leucite) (Maggetti, 1981; Maniatis *et al.*, 1981). It is also important to notice that these results are in good agreement with such indications as the matrix colour (C1, brown or orange depending on the crystallisation of hematite; C2, light orange; C3, yellowish; C4, greenish), and the deformation of some individuals in

category C4, because of the collapse due to the advanced liquid phase produced during firing (Picon, 1973).

If we exclude the few individuals that must be considered as particular cases, comparison between the chemical and the mineralogical data shows a significant degree of correspondence for 89 out of the 108 individuals retained. In Table 5 we have grouped the individuals, according to their deposition contexts in the site, in three categories: for the individuals coming from the kilns (areas U2, F1, F2 and B in Figure 1), from outside the kilns (areas E and Q2), and for those individuals of unknown deposition context. Thus, we can see that 4 out of 8 individuals of the chemical group GC are classified in mineralogical category C1, with the kilns as their deposition context. For the other 4 individuals of the chemical group GC we do not know the deposition context, but it is worth noting that 2 of them are classified in mineralogical category C1 and the other 2 are classified in mineralogical category C2. The correspondence between these data is still clearer for the individuals of the chemical group GA, in which 31 out of the 35 individuals are classified in mineralogical category C2 and come from the deposition contexts outside the kilns. The other 4 individuals grouped in GA also come from the same deposition context, but they are classified in mineralogical categories C1 (3 individuals) and C3 (1 individual), which are the mineralogical categories next to C2. In the case of the chemical group GB, 21 out of 23 individuals are classified in mineralogical category C3. Nevertheless, no relation is observed in this case between chemical group GB and a specific deposition context. Only 2 individuals of the chemical group GB are classified in mineralogical category C2, but they come from deposition contexts outside the kilns. Finally, 12 out of 13 individuals of the chemical group GE are classified in mineralogical category C4. As in the previous chemical group, no relation is observed between chemical group GE and a specific deposition context.

It can then be clearly observed that the structure in several chemical groups, provoked by the existence of several asymmetries involving certain individuals, is linked to the firing temperature (to the physical, mineralogical and chemical characteristics developed by the firing) and to the deposition context. The reason for this is the presence of selective alteration and contamination processes. In this sense, the values  $\ln(\text{CaO}/\text{SiO}_2)$ ,  $\ln(\text{Ba}/\text{SiO}_2)$  and  $\ln(\text{Sr}/\text{SiO}_2)$  reflect the perturbation operating on the components CaO, Ba and Sr (Figure 7). In the case of  $\ln(\text{CaO}/\text{SiO}_2)$ , these values are related to the crystallisation of secondary calcite (for example, Heimann & Maggetti, 1981; Maggetti *et al.*, 1984; Picon, 1985a), which would imply a partial enrichment with allochthonous  $\text{Ca}^{2+}$ . Notwithstanding, the phenomenon of secondary calcite is a very complex problem which needs the concurrence of more than one analytical technique for its identification, and especially for its interpretation in terms of enrichment with allochthonous calcium. In the case of Abella, the data support such an interpretation (*vid.*, Buxeda & Cau, 1995a). In relation with the values  $\ln(\text{Ba}/\text{SiO}_2)$  and  $\ln(\text{Sr}/\text{SiO}_2)$ , contaminations of Ba and Sr have also been reported (for example, Bieber, 1977; Olin *et al.*, 1978; Freestone *et al.*, 1985; Picon, 1985b; Picon, 1987; Schmitt, 1989; Béarat, 1990; Picon, 1991). In the case of Abella, the data suggest the existence of a certain association between the contamination of calcium, barium and strontium, especially affecting those individuals in mineralogical categories C1 and C2, that are buried in the deposition contexts E/Q2.

In Figure 8 we can observe the asymmetries detected in mineralogical category C4. In this fabric we can observe the effect of two different, possibly partially related, processes that cause the contamination of sodium and the lixiviation of potassium, perhaps because of the alteration of the glassy phase (for example, Picon, 1976; Segebade & Lutz, 1980; Lemoine *et al.*, 1981; Schmitt, 1989; Picon, 1991). This lixiviation is not observed in all the individuals in category C4, but, what has to be taken into consideration is that all the individuals in this category present, with different intensities, peaks of leucite, a potash feldspatoid (Figure 5 and Figure 6). This firing phase could act as a way of fixing the potassium, preventing its lixiviation. On the contrary, what is made clear is the contamination of sodium for all the individuals. In this case, this contamination of sodium is directly related to the crystallisation of a sodium zeolite, analcime (Figure 5), which is clearly a secondary phase (for example, Maggetti, 1981; Heimann & Maggetti, 1981; Walter, 1988). This process is also possibly favoured by the alteration of the glassy phase. The analcime was semiquantified on the basis of the intensity in counts per second (CPS) of its peak 5.59Å. The diagram analcime- $\ln(\text{Na}_2\text{O}/\text{SiO}_2)$  shows the relation between the presence of analcime and the sodium content.

Moreover, it should be pointed out that individual 14, which can be classified in mineralogical category C2 and which has markedly the highest observed variability in  $\text{P}_2\text{O}_5$ , is the only individual from the La Rectoria site. In contrast to the production site of Abella, La Rectoria was an inhabited Roman villa that was used as a cemetery during the Medieval Ages. This may have given rise to the relation between this contamination and the organic matter on the site. However, none of our data directly support this identification, that is the phase where the phosphorous is fixed, or the mechanism of its formation (Buxeda, 1995a).

Finally, cobalt and tungsten, not considered in the previous discussion, are typical examples of alterations and contaminations produced in the laboratory. Here, the use of a tungsten carbide cell mill is the cause of these contaminations. If we recalculate the variation matrix including these two components, we obtain a value  $vt/\tau_{\text{Co}}$  of 50.53%, where the contribution of the total variation to the logratio covariance matrix is as low as 50%. In the case of tungsten, the value  $vt/\tau_{\text{W}}$  is significantly lower, 9.41%. These results were expected because cobalt is a minor element in the composition of the cell, while tungsten is a major one. Furthermore, it is important to notice that the lowest value in the column of W is  $\tau_{\text{Co W}}$ , this reflects the relationship between both components in the composition of the cell and the parallel occurrence in this contamination (for a similar problem see Attas *et al.*, 1984).

### **The distribution function.**

The Abella case shows that the perturbing vector is a function of three wide groups of variables (Buxeda, 1995a):

$$\mathbf{u}=\mathbf{f}(\mathbf{F},\mathbf{E},t),$$

where F is the fabric (which includes the chemistry, the mineralogy, the structural characteristics, etc. for the individuals, and which is the result of the transformations during firing of the initial paste), E is the environment (i.e. any environment in which the ceramic was placed during use, burial, etc.; it includes chemistry, pH, temperature,

etc.), and  $t$  is time (the duration of the contact between the ceramic and a special environment with stable or changing conditions). In the present example, the variables ‘association of crystalline phases obtained by XRD’ and ‘deposition context in the site’ operate as simply two very rough estimates of fabric and environment, respectively.

If the component used as divisor is always directly operated by the neutral element, the use of logratio transformed data retains the effect of the perturbations within the components directly perturbed. It also allows the original ratios (i.e. the original distances) to be recovered between those components of different individuals directly operated by the neutral element. With this procedure, we avoid the estimation of the values of the components of the perturbing vector  $\mathbf{u}$  (Aitchinson, 1986), which in practice is almost impossible (Woronow & Love, 1990). This control over indirect operations is important in defining the reference group when estimating mean (16), variance (17) and covariance (18), because the effect of the perturbations is kept within the directly perturbed components. Therefore, when we define the distribution function, if this is a normal multivariate, as

$$N^{S-1}(\boldsymbol{\mu}, \boldsymbol{\Sigma}),$$

where we consider only the subcomposition of the  $S$  elements as always being directly operated by the neutral element, we recover the original distribution function for this subcomposition.

### **Final implications: loss on ignition and tempering.**

The data treatment derived from transformation (11) allows us to control a difficult problem, the loss on ignition (LOI) value. The LOI value incorporates several terms: the volatile elements (Cogswell *et al.*, 1996) and, especially, certain elements such as hydrogen, oxygen and carbon that are usually not determined and that are related to the organic matter, the compositional water of primary phases and anions such as  $\text{CO}_3^{2-}$ , which are present in the original paste. This process, which is not a perturbation operation as defined in this paper, can actually be modelled as a perturbation induced by firing temperature during the transformation process from paste to fabric. Therefore, the logratio transformation also allows us to control the effect of this paste-to-fabric change, and the diversification of compositions with the apparent dilution effect for the determined concentrations (Kilikoglou *et al.*, 1988).

If we recalculate the variation matrix of Table 2, taking into consideration the LOI, we obtain a value  $vt/\tau_{\text{LOI}}$  of 15.41%, and values clearly lower in column LOI for the variances  $\tau_{\text{CaO LOI}}$ ,  $\tau_{\text{Ba LOI}}$  and  $\tau_{\text{Sr LOI}}$ . These results were expected because the alterations and contaminations affecting the enrichment in calcium, barium and strontium are observed in the individuals classified in mineralogical categories C1 and C2, which correspond to the lowest firing temperatures. The means in raw data of the LOI are (in %) GC 10.31 ( $\pm 2.08$ ), GA 8.71 ( $\pm 2.41$ ), GB 4.15 ( $\pm 1.08$ ), and GE 3.21 ( $\pm 1.63$ ), which show the dramatic effect of the indirect operations induced by LOI.

This model can also be applied to tempering. The tempering problem has been extensively discussed in the literature as the dilution problem imposed by the decrease in concentrations for the determined elements when the temper is added (Neff *et al.*,

1988; Neff *et al.*, 1989; Beier & Mommsen, 1994). If we take the raw material as a compositional vector and the temper as a perturbing one, the addition of temper has two effects: 1) through the direct operation it changes the original concentrations of those components operated by values other than the neutral element (all values are  $u_j > 1$ , except  $u_j = 1$  when the corresponding element is not present in the temper), and 2) through the indirect operation being divided by  $k$  (4), due to the constraining operator of compositional data, which affects all the components independently of the direct operation. For example, quartz temper affects trace element determinations through the indirect operation. Thus, it is clear that what has been called an inert diluent does not actually exist (Neff *et al.*, 1989). What does exist, however, are cases in which the direct perturbation affects only undetermined components. In this sense, we can see that the logratio transformation can deal with the so-called dilution problem.

As an example, if we repeat the cluster analysis in Figure 4, without including the components  $\ln(P_2O_5/SiO_2)$ ,  $\ln(CaO/SiO_2)$ ,  $\ln(Na_2O/SiO_2)$ ,  $\ln(K_2O/SiO_2)$ ,  $\ln(Ba/SiO_2)$  and  $\ln(Sr/SiO_2)$  in the subcomposition used, the present structure disappears. Individual 14, affected by the contamination in  $P_2O_5$ , is also placed amongst the other individuals. The lower ultrametric distances reflect large reduction in the variability. Also, some new differences are now apparent having previously been obscured by the perturbations dominating the data treatment, and in particular it appears that individuals 108 and 109 exhibit a quite distinct chemical composition. The most interesting point is that individual 87, a clear outlier in Figure 4, is now placed among all the individuals. This fact is important if we consider that this individual is the only one that presents a low calcareous clay (in normalised subcomposition the CaO is 2.99%). This result clearly shows that using the logratio transformation in the appropriate way we can avoid differences such as calcium content, which can be changed by the potter through the addition of temper, thus recovering the original values in raw materials.

## **Conclusions.**

The study of chemical data from Abella kiln material has allowed us to identify a high compositional variability, particularly for certain components. Comparing chemical and mineralogical data, as well as physical properties, has made the interpretation of the compositional variability, insofar as it is related to alteration and contamination processes, possible. These processes have affected the individuals differently, because of the fabric and the deposition context.

The advantages of using the logratio transformation rather than the centred logratio are clear theoretically, since the asymmetric transformation is more robust when facing the perturbations. The logratio transformation highlights the existence of compositional variability, perhaps imposed by perturbation operations, through the variances in the variation matrix. It also allows the indirect perturbation to be avoided, by dividing the data in (11) with a component that is not directly perturbed, as well as the direct perturbation by excluding the directly perturbed components in the data treatment. In this way, the unknown original distances and distribution functions are recovered for the subcomposition of the determined components which are not directly perturbed.

Notwithstanding, if what we face is the need to explain mathematically the compositional variability of the chemical characterisation, this explanation implies certain assumptions that cannot be demonstrated in the mathematical solution itself. Thus, the explanation of the compositional variability requires the identification and interpretation as perturbation (including alteration and contamination processes, LOI, tempering and technology) or as polygenic provenance (Buxeda, 1995b). Furthermore, the interpretation and explanation of this compositional variability requires the use of data other than chemical, and also the concurrence of validation archaeological data.

To achieve these objectives, the logratio transformation proposed by Aitchinson has been found to be the most appropriate, and it is robust enough to allow the use of all the determined components since initially they have equal value, which ought to be the only assumption allowed during the data treatment (Sneath & Sokal, 1973).

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	Terra Sigillata	Moulds	Gas extraction tubes	Common pottery	Total
U2 (UE 2)				103-104	2
F1 (UE 1)		19,21-22,24-25		57-59	8
E (UE 1)				99-102	4
Q2 (S UE 1)				76-79	4
Q2 (UE 1)	3,5-6,8,17,30-31,39			80-87	16
Q2 (UE 2)	1,4,7,9-12,16,33-36			88-98	23
F2 (UE 1)	13,18,38,41-43			60-73	20
F2 (UE 3)				74-75	2
B (UE 1)				105	1
B (UE 2)				106	1
A (UE 2)				107-110	4
A (UE 3)				111	1
A (UE 4)				112-114	3
L.R. Q2	14				1
Unknown	15,32,44-50,52-56		26-29		18
Total	41	5	4	58	108

Table 1. Sampling undertaken at Abella, according to ceramic class and deposition context. L.R.: La Rectoria site. Unknown: unknown deposition context.

Abella	Fe2O3	Al2O3	MnO	P2O5	TiO2	MgO	CaO	Na2O	K2O	SiO2	Ba
Fe2O3	0	0.001777	0.031249	0.096188	0.004312	0.015097	0.110873	0.269304	0.110053	0.006158	0.118946
Al2O3	0.001777	0	0.037241	0.100605	0.005031	0.017245	0.104537	0.26623	0.109725	0.006608	0.126118
MnO	0.031249	0.037241	0	0.084481	0.031609	0.046816	0.103647	0.361184	0.11794	0.025097	0.086605
P2O5	0.096188	0.100605	0.084481	0	0.093163	0.120994	0.15318	0.367292	0.192029	0.084002	0.135132
TiO2	0.004312	0.005031	0.031609	0.093163	0	0.020077	0.110393	0.279858	0.116992	0.004302	0.114014
MgO	0.015097	0.017245	0.046816	0.120994	0.020077	0	0.111939	0.274693	0.127323	0.025395	0.138286
CaO	0.110873	0.104537	0.103647	0.15318	0.110393	0.111939	0	0.36721	0.211734	0.092566	0.141542
Na2O	0.269304	0.26623	0.361184	0.367292	0.279858	0.274693	0.36721	0	0.590159	0.284622	0.547182
K2O	0.110053	0.109725	0.11794	0.192029	0.116992	0.127323	0.211734	0.590159	0	0.107394	0.191148
SiO2	0.006158	0.006608	0.025097	0.084002	0.004302	0.025395	0.092566	0.284622	0.107394	0	0.099738
Ba	0.118946	0.126118	0.086605	0.135132	0.114014	0.138286	0.141542	0.547182	0.191148	0.099738	0
Rb	0.030688	0.027162	0.074619	0.15225	0.03616	0.044282	0.163036	0.303896	0.082915	0.040146	0.199376
Th	0.012658	0.010938	0.054612	0.110807	0.014986	0.030215	0.12442	0.259769	0.123354	0.018837	0.143876
Nb	0.012109	0.010124	0.040384	0.09928	0.011124	0.022892	0.097619	0.26278	0.121254	0.010451	0.121095
Zr	0.020827	0.020675	0.043916	0.094083	0.014245	0.04532	0.108013	0.263974	0.141494	0.010596	0.12384
Y	0.008685	0.008969	0.028505	0.083674	0.009866	0.026737	0.090793	0.283442	0.100248	0.004799	0.100921
Sr	0.263001	0.26399	0.218733	0.268219	0.258756	0.259267	0.141794	0.618825	0.322636	0.230112	0.130223
Ce	0.007119	0.006499	0.036125	0.088166	0.007728	0.027889	0.110547	0.27296	0.113019	0.007053	0.11712
Ga	0.008933	0.006156	0.049549	0.129313	0.013913	0.019902	0.134403	0.268649	0.106185	0.018263	0.165892
V	0.020527	0.019024	0.063515	0.142524	0.028348	0.039461	0.172505	0.289321	0.120946	0.031511	0.173336
Zn	0.023496	0.0254	0.052316	0.128366	0.030485	0.030094	0.147351	0.289227	0.114778	0.034226	0.168937
Ni	0.003795	0.001687	0.039472	0.1073	0.007621	0.018088	0.102779	0.269974	0.110522	0.009091	0.128255
Li	1.173099	1.175741	1.627614	2.831046	1.212981	1.462012	2.90088	6.990552	3.331852	1.150966	3.271582
vt/Li	0.918192	0.916128	0.661784	0.380471	0.888002	0.736745	0.371311	0.154084	0.323283	0.935848	0.329238
r <sub>v,t</sub>	0.991806	0.989418	0.968463	0.957692	0.995791	0.9897	0.798091	0.90853	0.944167	0.999027	0.727872
	Rb	Th	Nb	Zr	Y	Sr	Ce	Ga	V	Zn	Ni
Fe2O3	0.030688	0.012658	0.012109	0.020827	0.008685	0.260301	0.007119	0.008933	0.020527	0.023496	0.003795
Al2O3	0.027162	0.010938	0.010124	0.020675	0.008969	0.26399	0.006499	0.006156	0.019024	0.0254	0.001687
MnO	0.074619	0.054612	0.040384	0.043916	0.028505	0.218733	0.036125	0.049549	0.063515	0.052316	0.039472
P2O5	0.15225	0.110807	0.09928	0.094083	0.083674	0.268219	0.088166	0.129313	0.142524	0.128366	0.1073
TiO2	0.03616	0.014986	0.011124	0.014245	0.009866	0.258756	0.007728	0.013913	0.028348	0.030485	0.007621
MgO	0.044282	0.030215	0.022892	0.04532	0.026737	0.259267	0.027889	0.019902	0.039461	0.030094	0.018088
CaO	0.163036	0.12442	0.097619	0.108013	0.090793	0.141794	0.110547	0.134403	0.172505	0.147351	0.102779
Na2O	0.303896	0.259769	0.26278	0.263974	0.283442	0.618825	0.27296	0.268649	0.289321	0.289227	0.269974
K2O	0.082915	0.123354	0.121254	0.141494	0.100248	0.322636	0.113019	0.106185	0.120946	0.114778	0.110522
SiO2	0.040146	0.018837	0.010451	0.010596	0.004799	0.230112	0.007053	0.018263	0.031511	0.034226	0.009091
Ba	0.199376	0.143876	0.121095	0.12384	0.100921	0.130223	0.11712	0.165892	0.173336	0.168937	0.128255
Rb	0	0.034246	0.038567	0.058399	0.042275	0.351945	0.034814	0.017424	0.033881	0.039155	0.029029
Th	0.034246	0	0.018625	0.028486	0.018618	0.287623	0.013528	0.016522	0.035417	0.037933	0.014477
Nb	0.038567	0.018625	0	0.016773	0.012399	0.246847	0.012527	0.018861	0.03694	0.038627	0.010766
Zr	0.058399	0.028486	0.016773	0	0.013085	0.274872	0.015733	0.035152	0.05048	0.053652	0.022668
Y	0.042275	0.018618	0.012399	0.013085	0	0.230144	0.008944	0.019886	0.034345	0.033292	0.0102
Sr	0.351945	0.287623	0.246847	0.274872	0.230144	0	0.258924	0.316327	0.346695	0.329734	0.260841
Ce	0.034814	0.013528	0.012527	0.015733	0.008944	0.258924	0	0.016072	0.029205	0.033955	0.00861
Ga	0.017424	0.016522	0.018861	0.035152	0.019886	0.316327	0.016072	0	0.013294	0.022282	0.006949
V	0.033881	0.035417	0.03694	0.05048	0.034345	0.346695	0.029205	0.013294	0	0.031463	0.018448
Zn	0.039155	0.037933	0.038627	0.053652	0.033292	0.329734	0.033955	0.022282	0.031463	0	0.025609
Ni	0.029029	0.014477	0.010766	0.022668	0.0102	0.260841	0.00861	0.006949	0.018448	0.025609	0
Li	1.834265	1.409945	1.260044	1.456282	1.169827	5.876807	1.226536	1.403927	1.731186	1.690377	1.206183
vt/Li	0.587227	0.763952	0.854835	0.739644	0.92076	0.183285	0.878188	0.767226	0.622192	0.637213	0.893007
r <sub>v,t</sub>	0.947039	0.978674	0.994628	0.98701	0.998922	0.606868	0.994236	0.960733	0.957708	0.968623	0.989902
St <sub>i</sub>	47.3937										
vt	1.07713										

Table 2. Compositional variation matrix from Abella. In each column  $i$  ( $i=1,\dots,S$ ) are the variances after a logratio transformation using the component  $x_i$  as divisor.  $vt$ =total variation.  $\tau_i$ =total sum of variances in column  $i$ .  $vt/\tau_i$ =percentage of variance in the logratio covariance matrix using the component  $x_i$  as divisor due to the total variation.  $r_{v,\tau}$ =correlation between the values  $\tau_{ij}$  ( $i\neq j$ ) and the corresponding values  $\tau_j$  ( $j=1,\dots,i-1,i+1,\dots,S$ ).  $\Sigma\tau_i$ =sum of the  $\tau_i$  values.

	GA (n=35)	GB (n=23)	GC (n=8)	GD (n=3)	GE (n=13)
Ln(Fe2O3/SiO2)	-2.0918 ±0.0316	-2.0028 ±0.0338	-2.0227 ±0.0208	-2.1327 ±0.0079	-1.9981 ±0.0512
Ln(Al2O3/SiO2)	-0.9677 ±0.0519	-0.8665 ±0.0304	-0.9065 ±0.0108	-1.0791 ±0.0167	-0.8590 ±0.0411
Ln(MnO/SiO2)	-6.3676 ±0.0896	-6.4723 ±0.0903	-6.1586 ±0.1651	-6.3574 ±0.0713	-6.4462 ±0.1121
Ln(P2O5/SiO2)	-5.5165 ±0.1078	-5.5990 ±0.0979	-5.5658 ±0.0938	-5.5793 ±0.0351	-5.6899 ±0.0927
Ln(TiO2/SiO2)	-4.2993 ±0.0390	-4.2332 ±0.0583	-4.2816 ±0.0322	-4.2889 ±0.0817	-4.2261 ±0.0658
Ln(MgO/SiO2)	-2.8025 ±0.0798	-2.7143 ±0.0601	-2.8811 ±0.0679	-2.9800 ±0.0810	-2.6552 ±0.0394
Ln(CaO/SiO2)	-0.8210 ±0.1518	-1.1846 ±0.1349	-1.1255 ±0.1498	-0.9154 ±0.0295	-1.0277 ±0.1453
Ln(Na2O/SiO2)	-4.9234 ±0.2587	-4.8612 ±0.1999	-5.2303 ±0.1769	-4.4443 ±0.0982	-3.7066 ±0.4156
Ln(K2O/SiO2)	-2.5774 ±0.1183	-2.4616 ±0.0664	-2.4001 ±0.0229	-2.6678 ±0.0159	-2.9313 ±0.5107
Ln(Ba/SiO2)	-6.0893 ±0.1657	-6.5900 ±0.1070	-6.2902 ±0.0713	-6.4899 ±0.1333	-6.7175 ±0.1858
Ln(Rb/SiO2)	-8.0803 ±0.1114	-7.8372 ±0.0680	-7.9144 ±0.0484	-8.1880 ±0.0116	-7.7426 ±0.1853
Ln(Th/SiO2)	-10.429 ±0.1258	-10.312 ±0.0763	-10.389 ±0.0969	-10.461 ±0.0950	-10.306 ±0.0844
Ln(Nb/SiO2)	-10.170 ±0.1042	-10.139 ±0.0641	-10.239 ±0.0748	-10.314 ±0.0831	-10.070 ±0.1559
Ln(Zr/SiO2)	-8.3199 ±0.0867	-8.3414 ±0.0361	-8.3875 ±0.0323	-8.2271 ±0.0362	-8.2819 ±0.0535
Ln(Y/SiO2)	-9.8011 ±0.0827	-9.8008 ±0.0452	-9.7980 ±0.0351	-9.7524 ±0.0232	-9.8249 ±0.0434
Ln(Sr/SiO2)	-6.0136 ±0.2467	-6.9041 ±0.1116	-6.7826 ±0.0921	-6.5811 ±0.0752	-6.8927 ±0.1841
Ln(Ce/SiO2)	-8.8812 ±0.0833	-8.8096 ±0.0584	-8.8288 ±0.0755	-8.9021 ±0.1116	-8.8322 ±0.0677
Ln(Ga/SiO2)	-10.076 ±0.0718	-9.8578 ±0.0492	-9.8856 ±0.0521	-10.145 ±0.0343	-9.8324 ±0.1001
Ln(V/SiO2)	-8.5207 ±0.0982	-8.2844 ±0.1162	-8.1445 ±0.1088	-8.7168 ±0.0403	-8.2842 ±0.1131
Ln(Zn/SiO2)	-8.4279 ±0.0799	-8.2288 ±0.0727	-8.1844 ±0.1483	-8.4230 ±0.0299	-8.2104 ±0.1269
Ln(Ni/SiO2)	-9.2569 ±0.0909	-9.1576 ±0.0400	-9.1872 ±0.0363	-9.4142 ±0.0324	-9.1526 ±0.0564

Table 3. Means and one standard deviation for the 5 defined groups, for the logratio data transformed SiO<sub>2</sub> as divisor.

	GA (n=35)	GB (n=23)	GC (n=8)	GD (n=3)	GE (n=13)
Fe <sub>2</sub> O <sub>3</sub> %	5.83 ±0.17	6.60 ±0.28	6.49 ±0.26	5.88 ±0.02	6.47 ±0.38
Al <sub>2</sub> O <sub>3</sub> %	17.95 ±0.47	20.54 ±0.71	19.80 ±0.55	16.87 ±0.15	20.19 ±0.98
MnO %	0.08 ±0.008	0.08 ±0.007	0.10 ±0.019	0.09 ±0.006	0.08 ±0.008
P <sub>2</sub> O <sub>5</sub> %	0.19 ±0.02	0.18 ±0.02	0.19 ±0.02	0.19 ±0.01	0.16 ±0.01
TiO <sub>2</sub> %	0.64 ±0.03	0.71 ±0.05	0.68 ±0.03	0.68 ±0.05	0.70 ±0.05
MgO %	2.87 ±0.23	3.24 ±0.17	2.75 ±0.18	2.53 ±0.20	3.35 ±0.13
CaO %	20.90 ±2.34	15.04 ±1.84	16.02 ±2.02	19.88 ±0.45	17.17 ±2.29
Na <sub>2</sub> O %	0.35 ±0.08	0.38 ±0.08	0.26 ±0.04	0.58 ±0.05	1.27 ±0.54
K <sub>2</sub> O %	3.61 ±0.43	4.18 ±0.31	4.45 ±0.17	3.44 ±0.08	2.81 ±1.13
SiO <sub>2</sub> %	47.26 ±1.96	48.85 ±0.83	49.02 ±1.03	49.64 ±0.44	47.62 ±0.91
Ba ppm	1089 ±209	675 ±73	912 ±77	758 ±102	587 ±137
Rb ppm	147 ±17	193 ±13	179 ±9	138 ±1	210 ±35
Th ppm	14 ±2	16 ±1	15 ±2	14 ±1	16 ±1
Nb ppm	18 ±2	19 ±1	17 ±2	17 ±1	20 ±3
Zr ppm	115 ±9	116 ±4	112 ±5	133 ±3	121 ±5
Y ppm	26 ±2	27 ±1	27 ±1	29 ±6	26 ±1
Sr ppm	1187 ±295	493 ±51	557 ±48	690 ±57	490 ±89
Ce ppm	66 ±5	73 ±4	72 ±6	68 ±8	69 ±4
Ga ppm	20 ±1	26 ±1	25 ±1	19 ±1	26 ±2
V ppm	95 ±9	124 ±15	143 ±15	81 ±4	121 ±14
Zn ppm	104 ±9	131 ±10	138 ±21	109 ±3	130 ±16
Ni ppm	45 ±3	52 ±2	50 ±2	40 ±1	50 ±3

Table 4. Means and one standard deviation for the 5 defined groups, for normalised subcompositions.

	C1 (n=12)					C2 (n=43)					C3 (n=22)					C4 (n=12)				
	C	A	B	E	ou	C	A	B	E	ou	C	A	B	E	ou	C	A	B	E	ou
Kilns	4					2	31	2		4									6	
E/Q2		3			3					3									1	
Unknown	2					2				1									5	

Table 5. Number of individuals in each category of association of crystalline phases by XRD (C1, C2, C3 and C4), according to the chemical group in which they were classified (C for GC, A for GA, B for GB and E for GE; ou=outlier) and to the deposition context (kilns, sectors E/Q2 or unknown).

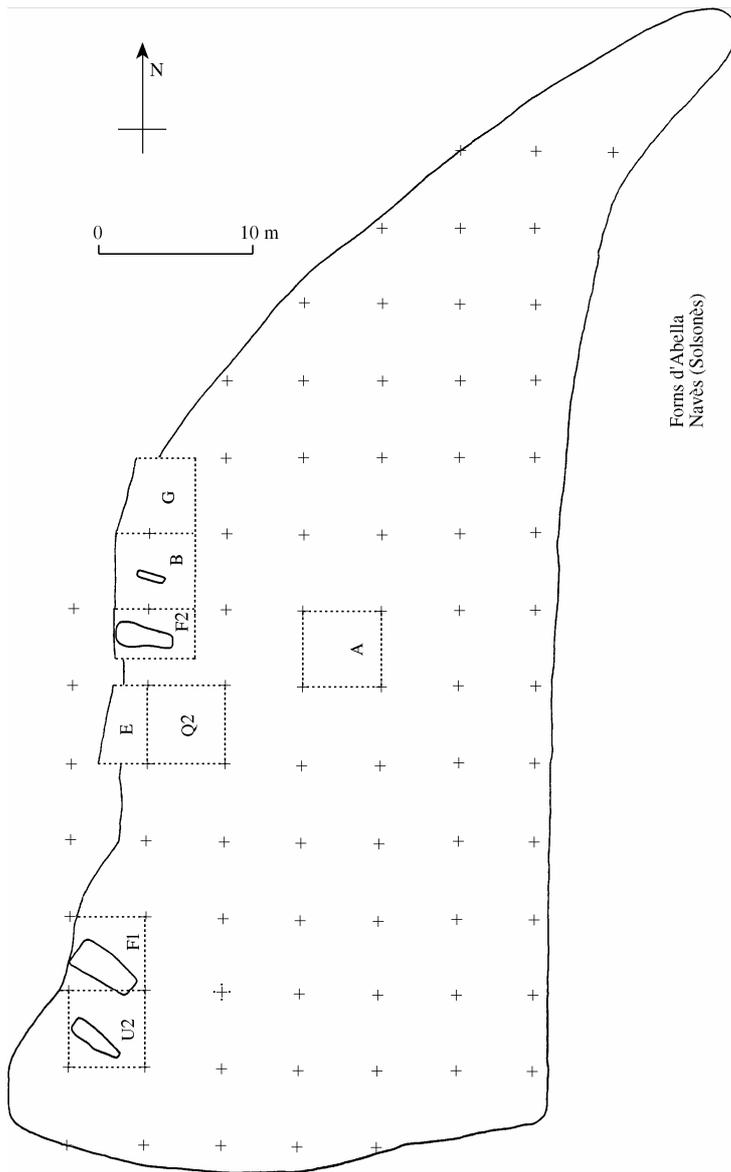


Figure 1. Area where the workshop of Abella was found. The surveyed areas are labelled. The kilns were found in the areas U2, F1, F2 and B.

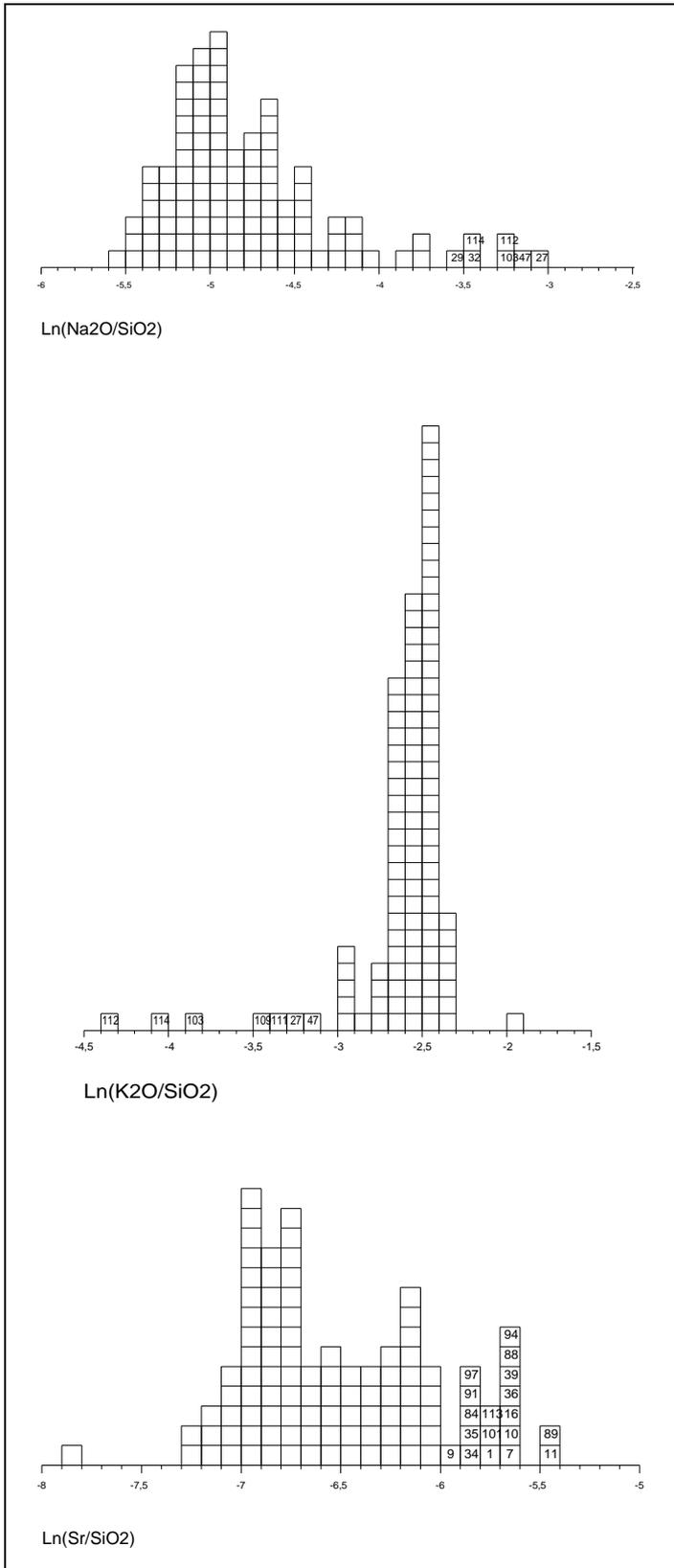


Figure 2. From top to bottom, histograms of the values  $\ln(\text{Na}_2\text{O}/\text{SiO}_2)$ ,  $\ln(\text{K}_2\text{O}/\text{SiO}_2)$  and  $\ln(\text{Sr}/\text{SiO}_2)$ , showing major asymmetries. Each square corresponds to one individual.

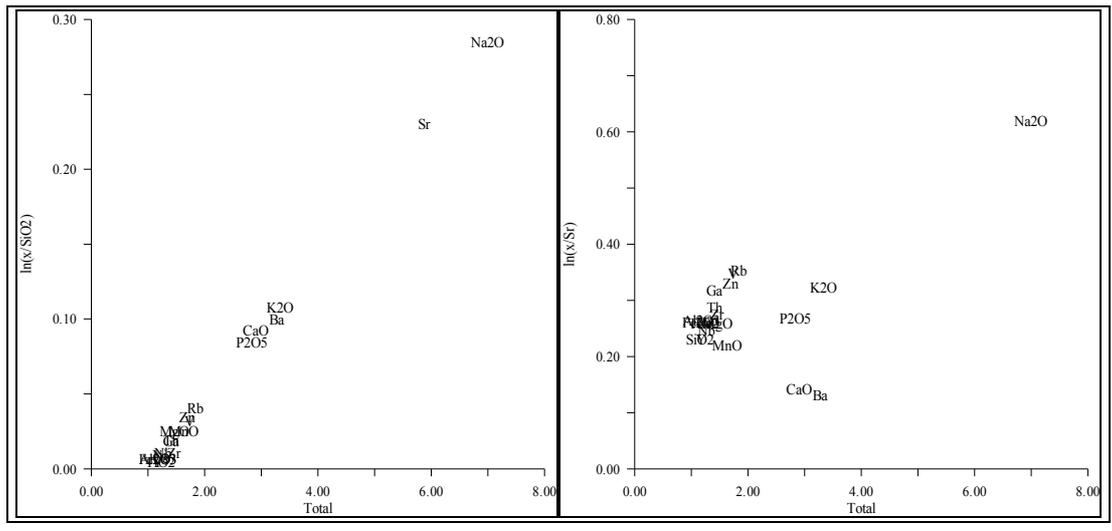


Figure 3. Bivariate graphics with the values  $\tau_j$  on the x axis and the values  $\tau_{ji}$  on the y axis ( $j=1, \dots, i-1, i+1, \dots, S$ ). Left-hand side  $ith=x_{SiO_2}$ , right-hand side  $ith=x_{Sr}$ .

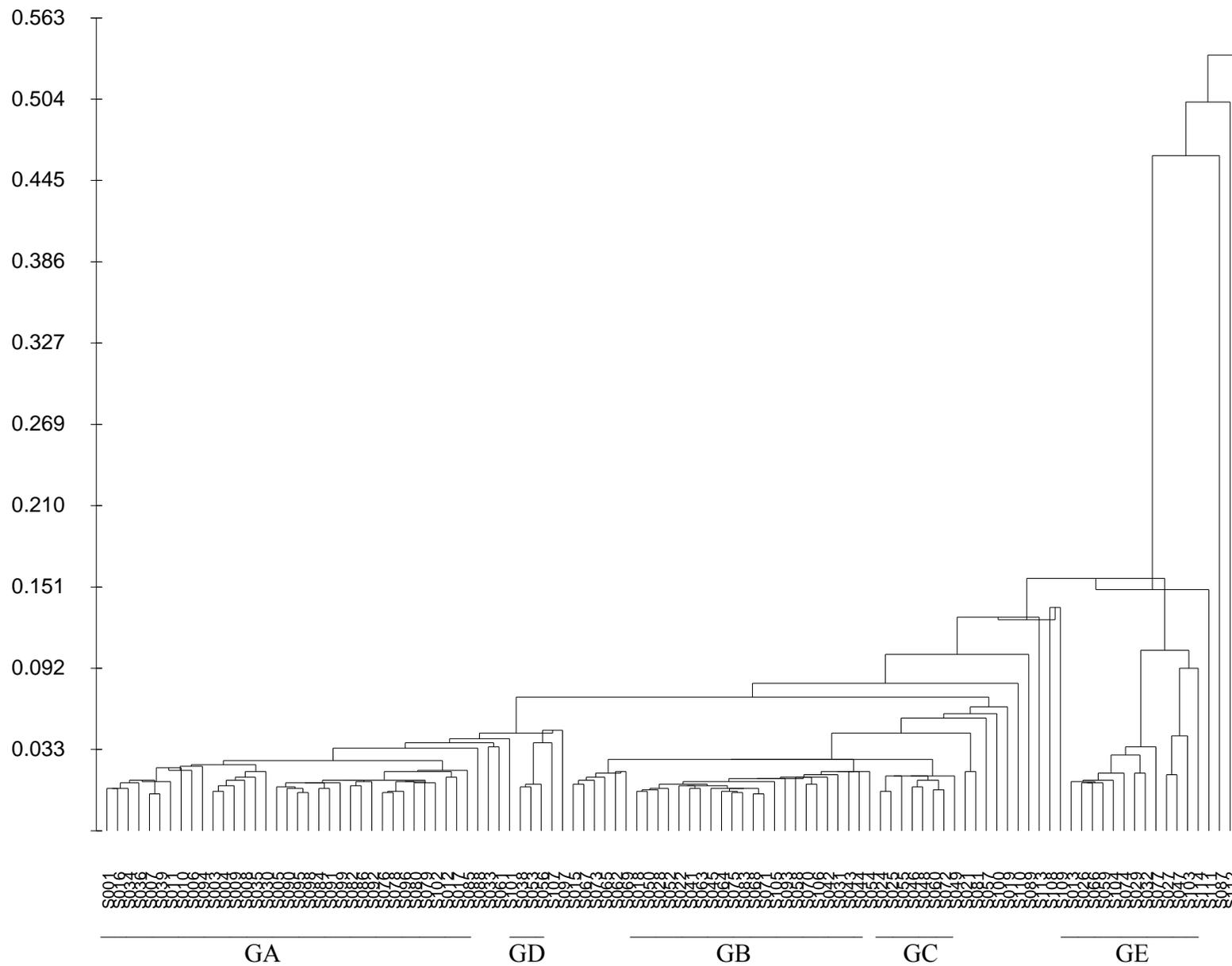


Figure 4. Dendrogram resulting from the cluster analysis using the squared mean Euclidean distance and the centroid agglomerative algorithm on the subcomposition  $\text{Fe}_2\text{O}_3$ ,  $\text{Al}_2\text{O}_3$ ,  $\text{MnO}$ ,  $\text{P}_2\text{O}_5$ ,  $\text{TiO}_2$ ,  $\text{MgO}$ ,  $\text{CaO}$ ,  $\text{Na}_2\text{O}$ ,  $\text{K}_2\text{O}$ ,  $\text{SiO}_2$ , Ba, Rb, Zr, Sr and V, using  $\text{SiO}_2$  as divisor in the logratio transformation.



Figure 5. Typical XRD patterns for the four categories of association of crystalline phases as detected by XRD. From top to bottom: C1 (represented by individual 25 in its as-received-state (ASR)), C2 (represented by individual 36 ARS), C3 (represented by individual 18 ARS), and C4 (represented by individual 13 ARS). Q: quartz; I-M: illite-muscovite; H: hematite; KF: potassium-feldspars; C: calcite; G: gehlenite; D: pyroxenes; P: plagioclase; L: leucite; An: analcime. Area of spectra: from 5 to  $45^{\circ}2\theta$ .

S00025 (ARS)

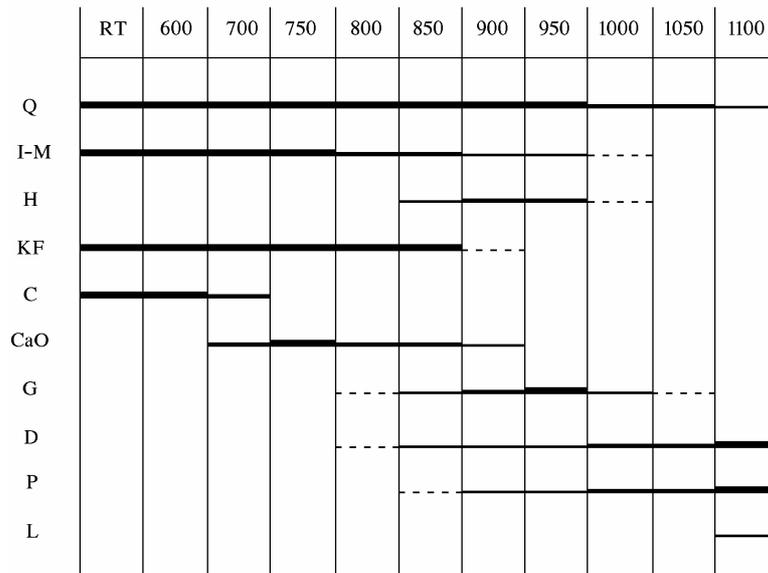
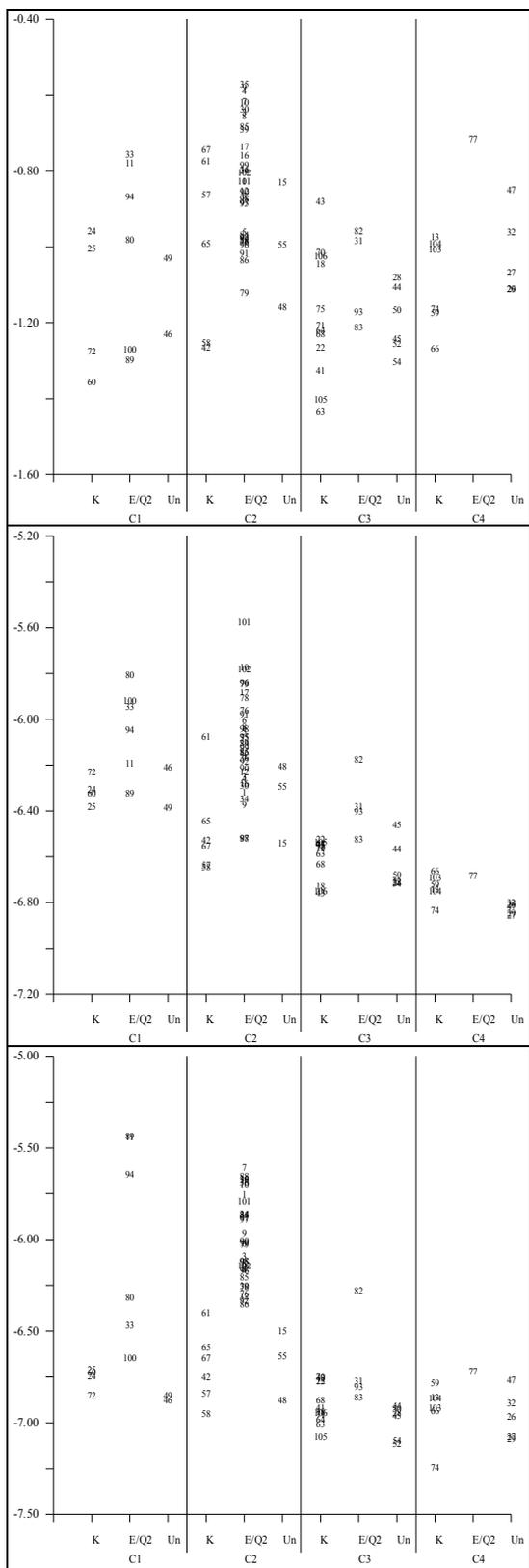


Figure 6. High temperature XRD experiment conducted on individual 25. Diffractograms were taken at room temperature (RT), 600, 700, 750, 800, 850, 900, 950, 1000, 1050 and 1100°C. Q: quartz; I-M: illite-muscovite; H: hematite; KF: potassium-feldspars; C: calcite; CaO: lime; G: gehlenite; D: pyroxenes; P: plagioclase; L: leucite.

Figure 7. Bivariate graphics with a two-way classification on x axis corresponding to the categories of association of crystalline phases by XRD and the deposition contexts (K: kilns; Un: unknown). From top to bottom, on y axis,  $\ln(\text{CaO}/\text{SiO}_2)$ ,  $\ln(\text{Ba}/\text{SiO}_2)$  and  $\ln(\text{Sr}/\text{SiO}_2)$ .



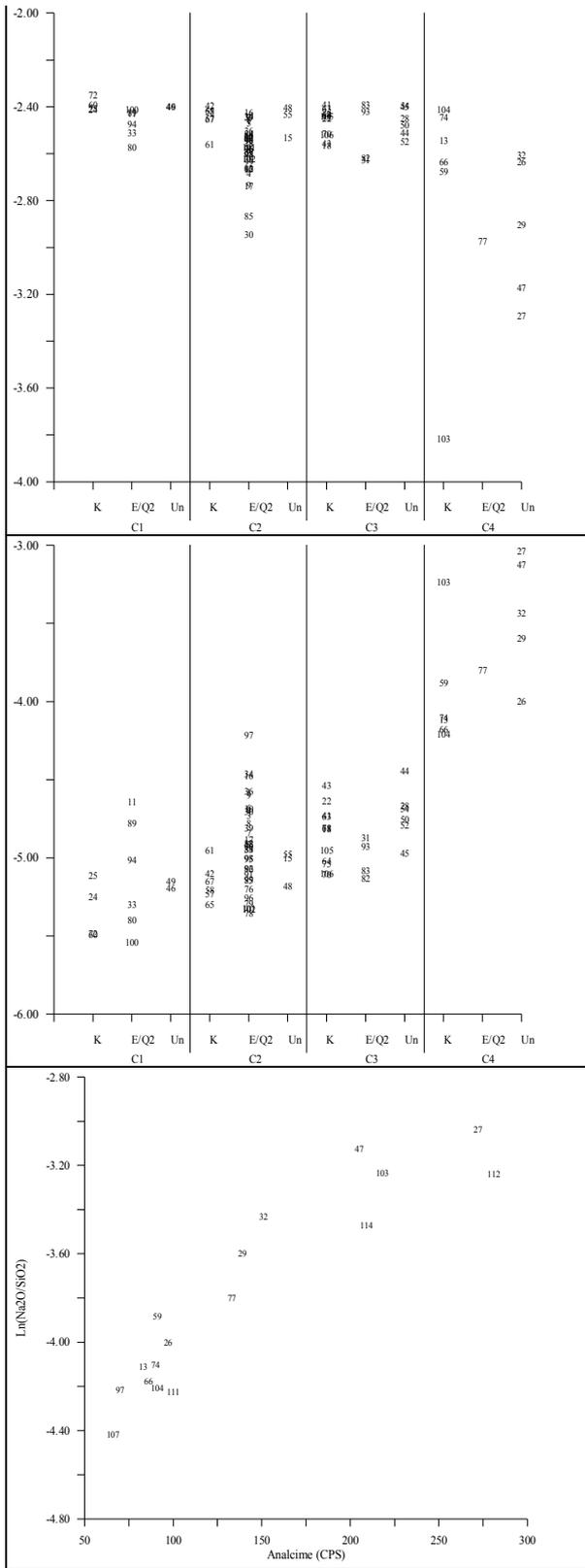


Figure 8. Bivariate graphics with a two-way classification on x axis corresponding to the categories of association of crystalline phases by XRD and the deposition contexts (K: kilns; Un: unknown). Top and middle, on y axis,  $\ln(K_2O/SiO_2)$  and  $\ln(Na_2O/SiO_2)$ . Bottom: bivariate graphic analcime- $\ln(Na_2O/SiO_2)$ .