

Water treatment sludge as precursor in non-dehydroxylated kaolin-based alkali-activated cements

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1 **Abstract**

2 Cement industry production and its materials demand are growing every year, leading to a
3 CO₂ and energy footprint increase. The drinking water production is increasing in water
4 treatment plants due to the population growth, raising in turn the waste materials produced.
5 Since these wastes are mainly managed in landfills, this preliminary research work is focused
6 on providing a new sustainable option for valorisation processes, based on the environmental
7 demand of the cement industry. Alkali-activated cements (AACs) can become a proper
8 option to give the water treatment sludge a new life cycle, as they can compete with ordinary
9 Portland cement (OPC) both in properties and sustainability. The main purpose of this study
10 was to evaluate and formulate different AACs based on the use of both raw clay and the water
11 treatment sludge (WTS), as precursors. The raw clay was used without previous thermal
12 dehydroxylation treatment, and the WTS, an aluminosilicate-rich waste, was used partially
13 replacing the raw clay in the AACs formulations. Both precursors and the formulated AACs
14 were characterized by X-ray diffraction (XRD), X-ray fluorescence (XRF) and Fourier-
15 transformed infrared spectroscopy (FT-IR). In addition, the compressive strength, the
16 chemical stability (hydrolytic degradation), and the environmental impact for each AACs
17 formulation were also determined. The results showed that AACs specimens formulated with
18 20 wt.% of WTS (replacing the raw clay) provided the best results, considering both
19 compressive strength and resistance to hydrolytic degradation. Then, it is possible to
20 formulate AACs using raw clay, without prior thermal dehydroxylation treatment, and WTS
21 as precursors.

22 **Keywords:** Alkali-activated materials; geopolymers; water treatment sludge; raw clay.

23 **1. Introduction**

24 Ordinary Portland cement (OPC) is produced in more than 150 countries across the globe,
25 where over half of the world's cement is currently produced in China. During 2018, the global
26 production capacity of cement was approximately 4,100 Mt (Reilly, 2019). The OPC industry
27 is one of the most energy consuming sector, (12 to 15% of industrial energy) and one of the
28 most contributors to CO₂ emissions (6 to 8% of the global carbon emissions) (Andrew, 2017;
29 Shen et al., 2017). This is due to the huge amount of cement produced and the thermal
30 processes used in its manufacture. In Spain, the cement industry consumes around 3 Mt per
31 year of fossil fuel, releasing 18 Mt of CO₂ to the atmosphere, representing the 7% of the total
32 CO₂ national emissions (García-Gusano et al., 2015).

33 In order to achieve proper sustainable production, cement manufacturers are trying to
34 decrease both emissions and energy consumption. To reach this goal, the industry is
35 decreasing the usage of the primary material and it is increasing the renewable resources use.
36 Besides, according to a circular economy model (Hossain et al., 2017), it is giving a new
37 productive life to some waste materials. This circular model involves the reusing and
38 recycling end-of-life materials and products criteria, extending their life cycle. Thus, it
39 increased the use of waste as secondary resources for new materials development. Alkali-
40 activated materials (AAMs), and especially the alkali-activated cements (AACs), turn up as
41 a feasible binder's solution to OPC. AACs have low energy consumption during its
42 processing and the reuse of industrial waste or by-products formulations as precursors
43 contributes to the greenhouse gas (GHG) emissions savings (Duxson and Provis, 2008;
44 Provis and Bernal, 2014).

45 A wide range of alumina- and silica-containing industrial waste has been used as
46 precursors in AAMs formulations. Some examples considering both low- and high-calcium

47 content in AAMs are metallurgical slags, power plant fly ashes, municipal solid waste
48 incineration bottom ash (Duxson et al., 2007; Provis and Bernal, 2014; Wongsu et al., 2017;
49 Provis, 2018; Maldonado-Alameda et al., 2020), etc. Moreover, abundant natural resources
50 can also be employed as AAMs precursors, like clay or clay-based minerals (Ruiz-
51 Santaquiteria et al., 2013; Liew et al., 2016; Zhang et al., 2020c). The selection of the optimal
52 precursor depends on the local availability of suitable raw materials (Provis, 2018). Clay and
53 clay-based materials, that are abundant through the Earth's crust, could be potential
54 precursors for AACs formulations. However, due to the low reactivity of clays, their usage
55 as precursor requires previous dehydroxylation thermal treatment (between 500°C and
56 850°C), which depends on the clay and the aluminosilicate structural layer stacking order
57 (Seiffarth et al., 2013; Belmokhtar et al., 2018; Bouna et al., 2020; Haw et al., 2020).
58 Dehydroxylated disordered clay shows higher pozzolanic activity than the starting materials
59 (e.g. metakaolin from kaolinite). The thermal process transforms the crystalline phases into
60 metastable phases, increasing the SiO₂ and Al₂O₃ availability, which are the required
61 compounds for the formation of previous forming gels (N-A-S-H). It should be noted that
62 this thermal treatment implies an additional energetic and economic cost, entailing a low
63 sustainable AACs synthesis and environment footprint.

64 The chemical and/or mechanical activation of clays (e.g. kaolinitic clay), without prior
65 dehydroxylation heating treatment, was studied elsewhere with promising results
66 (Mackenzie, 2009; Slaty et al., 2013; Hounsi et al., 2014; Esaifan et al., 2015; Zhang et al.,
67 2020a, 2020b). Although the SiO₂/Al₂O₃ availability was not as large as in the
68 dehydroxylated clay, chemical and/or mechanical treatments allow obtaining AACs, usually

69 mortars using silica sand as filler, with good performance for its use as a construction
70 material.

71 On the other hand, drinking water consumption is increasing steadily due to population
72 growth and the need to supply tap water with the health guarantees required for human health
73 (Rodríguez et al., 2010). The drinking water supply requires proper treatment of continental
74 water (surface water), which is performed in the water treatment plants (WTP). During the
75 surface water treatment process, i.e. coagulation-flocculation, sedimentation, filtration and
76 disinfection (Ahmad et al., 2016), a large volume of water treatment sludge (WTS) is
77 generated. In this regard, it is estimated that a typical WTP produces about 100 kt of WTS
78 per year (Bourgeois et al., 2004). The WTS is a clay-based waste mainly formed by
79 suspended sediments carried by the surface waters, which are aluminosilicates rich materials,
80 precipitates formed during the treatment process, and traces of unreacted chemicals. Most of
81 the WTS is collected in the coagulation-flocculation step, where the use of aluminium-based
82 agents is usual. WTS is mainly disposed of in landfills (Cremades et al., 2018; De Carvalho
83 Gomes et al., 2019), as its use is not regulated yet. Consequently, the need to find a new
84 destination for these sludge wastes has arisen, where the ceramic and cement industries are
85 some of the most promising targets (Cremades et al., 2018; Godoy et al., 2019).

86 The main goal of this study was to evaluate the potential of new AACs binders formulated
87 with WTS, partially replacing a commercial raw clay commonly used in the ceramic industry.
88 To increase sustainability and applicability, this preliminary research work was focused on
89 the use of both precursors without prior thermal activation and using alkali-activators in the
90 formulation of the AACs. The use of common non-dehydroxylated clay and a clay-based
91 waste with higher available aluminium content in the formulation of AACs contributes to the

92 development of alternative sustainable binder materials and provides an important added
93 value to the WTS.

94 **2. Materials and methods**

95 2.1. Materials

96 A commercial raw clay supplied by the Argiles Colades S.A. company (Girona, Spain)
97 was used as precursor in the different AACs formulations. The same natural raw clay was
98 used as a binder for the formulation of alkali-activated mortars, using silica sand as filler, in
99 previous research work, with promising results (Calderón, 2019). In the above-mentioned
100 cited study the clay was not thermally dehydroxylated, its activation was carried out by means
101 of an alkali solution of Na(OH)/Na₂SiO₃.

102 WTS used in this research was supplied by Aigües del Ter Llobregat (ATL) company
103 from the WTP located in Abrera (Barcelona, Spain). This treatment plant manages the
104 upstream water supply for the metropolitan area of Barcelona (Spain). Currently, as far as it
105 is known, the WTS generated in this plant is not reused and it is managed as non-hazardous
106 waste in landfills.

107 Sodium hydroxide (NaOH) in the form of 98.5% pure pellets (Labkem) was used as the
108 activator in the AACs formulations. It was dissolved in deionized water to obtain the different
109 molarity (M) dissolutions used in the experimental trials (2M, 4M, 8M, 10M, and 12M).

110 2.2. Experimental procedure

111 Activation of a non-dehydroxylated clay by the addition of NaOH and/or sodium silicate
112 activating solutions has already been addressed (Calderón, 2019; Emmanuel et al., 2019;
113 Marsh et al., 2019). However, in this preliminary study, only the use of NaOH solutions as

114 activators has been considered. Prior to the preparation of the different AACs formulations,
115 the proper concentration of the NaOH activator solution and the optimal L/S ratio were
116 determined. The L/S ratio is referred between the activator solution (attributed to the liquid,
117 L) and the precursor (specified as solid, S). The availability of SiO₂ and Al₂O₃ as reactive
118 phases for both precursors were determined through chemical attacks with NaOH solutions
119 (2M, 4M, 8M, 10M, and 12M). For these experimental trials, 1g of each precursor was mixed
120 with 100 mL of each different molarity solution and stirred constantly for 5 h at 80 °C in a
121 sealed plastic container (Ruiz-Santaquiteria et al., 2011). The resulting solution was filtered
122 and analysed per duplicate through inductively coupled plasma optical emission
123 spectrometry (ICP-OES), using Perkin Elmer Optima ICP-OES 3200 RL equipment. It was
124 quantified the Si and Al leached. From the availability of both elements, the proper
125 concentration (M) of the activator solution was determined.

126 Different formulations were carried out (Table 1) to assess the effect of partially replacing
127 WTS as precursor in the AACs formulations. Six cubic shape specimens (25x25x25 mm)
128 were prepared (Fig. 1) for each formulation. L/S ratio was fixed for minimum workability
129 found in previous tests with the best mechanical resistance. The L/S ratio was 0.6 except for
130 the case of WTS-80 because of the lack of workability, where the ratio was 0.75. After
131 formulating and moulding the pastes, the moulds were placed into a closed plastic bag and
132 set in a stove at constant temperature (80 °C) for 24 h (Calderón, 2019). Subsequently, the
133 moulds were removed from the stove and cooled at room temperature. Afterwards, specimens
134 were demoulded and stored for 14 days at room temperature before testing.

135 At 14 days of curing one specimen of each AACs formulation was milled to determine
136 the neoformed mineral phases and to evaluate the most representative functional groups,

137 through XRD and Fourier-transform infrared spectroscopy (FT-IR) techniques, respectively.
138 FT-IR spectra were acquired in attenuated total reflectance mode (ATR) in the range 4000 -
139 450 cm^{-1} , with a resolution of 4 cm^{-1} , using a Spectrum Two™ Perkin Elmer spectrometer.

140 2.3. Mechanical and chemical tests

141 Mechanical properties were tested through compressive strength (σ_c) for each AACs
142 formulated. The σ_c tests after 14 curing days were performed per triplicate following the
143 UNE-EN 196-1 standard, using a universal testing machine Incotecnic MULTI-R1, equipped
144 with 20 kN load cell. A progressive load until fracture was applied with a loading rate of 240
145 $\text{kg}\cdot\text{s}^{-1}$.

146 The chemical stability of the cured AACs was evaluated introducing the cubic (25x25x25
147 mm) specimens of each formulation in boiling water for 20 min (Davidovits, 2008; Zhu et
148 al., 2018). Afterwards, the specimens remained at room temperature until constant weight in
149 a desiccator with silica gel. Before and after the chemical stability tests, the samples were
150 weighed to determine the mass loss and to verify the chemical stability and resistance to the
151 specimens' dissolution. If the sample was still whole or with a weight loss of less than 10%,
152 the chemical stability was considered adequate and the test was considered a success.

153 Finally, to assess the environmental impact and to evaluate the hazardousness of the
154 AACs formulated with WTS as precursor, the leaching potential of heavy metals and
155 metalloids were studied. Leaching tests in deionised water for 24 h were conducted according
156 to the European standard (EN 12547-4). PerkinElmer ELAN 6000 ICP mass spectrometry
157 (ICP-MS) device was used to analyse some heavy metal(loid)s in the obtained eluates (As,
158 Ba, Cd, Cr, Cu, Hg, Mo, Pb, Ni, Se, Sb, and Zn).

159 3. Results and discussion

160 3.1. Precursors' composition

161 Table 2 shows the chemical composition of the dry clay (105°C overnight). It was determined
162 by X-ray fluorescence (XRF), using a Philips PW2400 X-ray sequential spectrophotometer.
163 As expected, the major compounds were SiO₂ (59.9 wt.% of clay) and Al₂O₃ (22.9 wt.% of
164 clay). The X-ray diffraction (XRD) pattern of the clay, using a Bragg-Brentano Siemens D-
165 500 powder diffractometer with CuK α -radiation, showed kaolinite and quartz as the main
166 crystalline mineral phases. The presence of hematite, calcite, muscovite, and halloysite was
167 also identified. Particle size distribution, determined with a laser analyser Beckman Coulter®
168 LSTM 13 320, showed a narrow distribution, with 50% of particles (d₅₀) below 21.58 μ m
169 and 90% of particles (d₉₀) below 52.52 μ m.

170 Chemical composition of WTS, determined by XRF, is shown in Table 2. As expected,
171 the major compounds of the sludge were SiO₂ and Al₂O₃, although the CaO content was also
172 significant. It is important to highlight the high value of loss of ignition (LOI, Table 2) of the
173 WTS sample. According to the results obtained by thermogravimetric analysis (TGA, Fig.
174 2), using an SDT Q600 device from TA Instruments in an air atmosphere (50 mL·min⁻¹) with
175 a heating rate of 10 °C·min⁻¹ up to 1,000 °C, the LOI result obtained in Table 2 can be
176 attributed to the presence of adsorbed water (2.20 wt. %), molecularly-bound water (5.21 wt.
177 %), hydroxides (11.66 wt.% of WTS), organic matter (3.46 wt.% of WTS) and a high content
178 of carbonates (13.39 wt.% of WTS).

179 The XRD pattern of the WTS showed quartz, illite and muscovite as main crystalline
180 mineral phases. Dolomite, calcite, and hematite were also identified. The particle size
181 distribution of WTS showed a d₅₀ of 45.24 μ m and a fraction d₉₀ lower than 227.5 μ m.

182 Previously to the AACs formulations, the whole WTS sample was sieved up to 80 μm , and
183 the fraction coarser than 80 μm was milled and sieved again. Therefore, all the WTS particles
184 must be below 80 μm .

185 3.2. Alkali-activation products

186 The availability of both gel-forming compounds of the SiO_2 and Al_2O_3 cementing phases,
187 resulting from the chemical attacks with different molarities of NaOH solutions, are shown
188 in Fig. 3 for both precursors, clay and WTS.

189 As can be seen in Fig. 3 (a, b) approximately 18 wt.% of the SiO_2 content and 36 wt.%
190 of the Al_2O_3 content was activated by the alkali attack, despite the clay was not thermally
191 activated. As expected, the activation of clay through an alkali reaction is much less than the
192 activation carried out from a previously thermally dehydroxylated clay (Emmanuel et al.,
193 2019). Moreover, considering the 8M, 10M, and 12M, the $\text{SiO}_2/\text{Al}_2\text{O}_3$ molar ratio was very
194 close to 2.00 (2.32 - 1.92), which is considered the proper molar ratio to form AACs (Duxson
195 et al., 2005). In contrast, as it is shown in Fig. 3 (c, d) the alkali activation from the WTS was
196 significantly lower than the obtained from the clay. While the availability of SiO_2 in WTS
197 increased when the concentration of the alkali solution increased, the availability of Al_2O_3
198 did not vary significantly. The maximum activation in WTS of SiO_2 was 10 wt.% of the SiO_2
199 contained in the precursor, using a 12M NaOH solution, while the activation of Al_2O_3 ranged
200 between 16 to 20 wt.%. It is surprising that, although the Al_2O_3 content was lower than the
201 SiO_2 content as showed in Table 1, the activation of Al_2O_3 was greater than the SiO_2 one.
202 This fact can be attributed to the presence of amorphous phase contained in the WTS,
203 consisting mainly of amorphous $\text{Al}(\text{OH})_3$ gels generated from the products added in the
204 coagulation-flocculation processes.

205 Regarding the results of the chemical attacks above described, it was considered to use
206 the 10M NaOH solution as the proper activate solution for all the AACs studied formulations
207 (Table 2). Furthermore, an excess of activator (e.g. 12M NaOH) induced to efflorescence of
208 unreacted sodium and the formation of a sodium carbonate coating on the samples' surface
209 (see bottom row in Fig. 1).

210 XRD diffractograms of WTS-0 and WTS-20 samples are shown in Fig. 4. XRD patterns
211 for the different percentages of WTS partially replacing clay were similar to each other and
212 resembled that of the WTS-0. As can be seen, the major crystalline phases in both alkali-
213 activated samples were quartz, kaolinite and muscovite. These mineral phases come from the
214 unreacted raw clay used as precursor. Note that halloysite determined in the raw clay was not
215 detected in the alkali-activated samples. Moreover, the weakening of the diffraction peaks of
216 kaolinite suggests that this mineral phase might also have participated in the alkali-activation
217 reactions. After alkali activation, several phases appeared as a result of the reaction, attributed
218 to sodium aluminium silicate hydrate and phillipsite, this last belonging to the zeolite group.
219 Sodium carbonate was also identified. It should be noted that small peaks of calcium silicate
220 hydrate (C-S-H) in the XRD diffractogram of WTS-20 were also identified (see upper right
221 of Fig. 4), which involves the calcium in the gelation process of alkali-activated formulations
222 where WTS was also used as precursor. In addition, the reddish tone of the raw clay due to
223 hematite was drastically reduced when this mineral phase disappeared, and the iron was
224 incorporated in the neoformed phases.

225 FT-IR spectra for both clay and WTS precursors before the alkali activation are shown
226 in Fig. 5. The bands at 3693 cm^{-1} , 3622 cm^{-1} were attributed to OH^- stretching and the band
227 at 1645 cm^{-1} to OH^- bending vibrations (El Hafid and Hajjaji, 2015). In the midwavenumber

228 region, the peaks at 1115 cm^{-1} , 792 cm^{-1} , and 749 cm^{-1} were associated to Si-O-Si
229 symmetrical stretching (Heah et al., 2012), which vanished during alkali activation. The main
230 peaks at 1027 cm^{-1} and $997 - 1000\text{ cm}^{-1}$ were assigned to Si-O-T (T=Si, Al) asymmetric
231 stretching vibration. The displacement of these last bands to lower wavenumbers, affecting
232 the Al-O and Si-O bonds, can be related to the formation of AACs (El Hafid et al., 2017).
233 The band at 912 cm^{-1} was attributed to Al-OH bending mode (Puligilla and Mondal, 2015).
234 Unlike the clay, the WTS spectrum also showed two other peaks at 1430 cm^{-1} and 875 cm^{-1} .
235 These were associated to O-C-O bonds (El Hafid et al., 2017), indicating the presence of
236 carbonates in the sludge (dolomite and calcite), as previously determined by XRD.

237 Fig. 6 shows the FT-IR spectra of clay before and after alkali-activation (WTS-0). The
238 peaks of the clay corresponding to Si-O-T asymmetric stretching were shifted to a lower
239 frequency, which was around 965 cm^{-1} , as well as the fading of other bands described
240 previously in the FT-IR of the precursor. Moreover, the broadband at $1490 - 1300\text{ cm}^{-1}$ was
241 associated to the O-C-O bonds, indicating a certain amount of sodium carbonates formed by
242 the atmospheric CO_2 adsorption at high alkali pH (El Hafid et al., 2017; Gao et al., 2017;
243 Belmokhtar et al., 2018).

244 The FT-IR midwavenumber region spectra of the AACs specimens formulated with WTS
245 as precursor, replacing different percentages of clay (0, 5, 10, and 20 wt.%), are shown in
246 Fig. 7. Increasing WTS percentage, the main peak at $965\text{-}979\text{ cm}^{-1}$ shifts to higher
247 frequencies. This broadband is actually due to the contribution of multiple bands which are
248 overlapped (El Hafid et al., 2017; Belmokhtar et al., 2018). These displacements could
249 initially be attributed to a higher contribution of Si-O-T (T = Si, Al) asymmetric stretching
250 vibration, due to a greater addition of the WTS as precursor. However, these shifts could also

251 indicate changes in the AACs structures, possibly due to the participation of calcium in the
252 gelation and the formation of calcium silicate hydrate gel, both C-S-H and C-(N)-A-S-H gels
253 (García-Lodeiro et al., 2008).

254 To clarify and reveal the overlap of the fundamental band, the deconvolution of the FT-
255 IR spectra in the midwavenumber region ($1100 - 850 \text{ cm}^{-1}$) is shown in Fig. 8. Gaussian
256 functions were added to adjust the shape of the spectra. The deconvoluted band of raw clay
257 (Fig. 8a) showed the presence of bands at 1028 cm^{-1} , 999 cm^{-1} , and 986 cm^{-1} , which were
258 assigned to Si-O-T (Si, Al) stretching vibrations (El Hafid and Hajjaji, 2015), and two peaks
259 at 933 cm^{-1} and 909 cm^{-1} , both corresponding to $\text{Al}_2\text{-OH}$ bending vibrations (Tironi et al.,
260 2012; Tămășan et al., 2013; El Hafid and Hajjaji, 2015). The deconvoluted band of the alkali-
261 activated specimens (Fig. 8b-e) showed the same peaks at $1029 - 1026 \text{ cm}^{-1}$, $996 - 999 \text{ cm}^{-1}$
262 and 911 cm^{-1} , also determined in the deconvolution of clay (Fig. 8a). These peaks were
263 attributed to vibrations of the unreacted clay. Note that the contribution of these non-shifted
264 peaks to the fitted curve decreases significantly in the alkaline activated samples. In contrast,
265 the peak at 986 cm^{-1} (Fig. 8a) was shifted to lower wavenumber (964 cm^{-1}) and increased its
266 contribution to the fitted curve in the alkali-activated clay (WTS-0, Fig. 8b), as a consequence
267 of the polymerization of the raw clay and the formation of N-A-S-H gel. Subsequently, as
268 the percentage of WTS replacing clay increases, this peak shifts again towards higher
269 frequencies ($970 - 976 \text{ cm}^{-1}$, Fig. 8c-e). This behaviour can also be observed in the shift of
270 the peak at $933 - 934 \text{ cm}^{-1}$ towards higher wavenumbers ($936 - 950 \text{ cm}^{-1}$, Fig. 8c-e). These
271 displacements are attributed to the increased availability of aluminium and calcium from
272 WTS, as well as the formation of both C-S-H and C-A-S-H gels (García-Lodeiro et al., 2008).

273 3.3. Mechanical strength

274 Fig. 9 presents the variation of compressive strength (σ_c) as a function of WTS
275 percentage in the AACs formulation. The obtained results were in agreement with the
276 published elsewhere by using non-dehydroxylated kaolin (Heah et al., 2012). From WTS-0
277 to WTS-5, a slight σ_c decrease from 2.4 MPa to 2.2 MPa can be noticed. After 5 wt.%, the σ_c
278 increased with the percentage of WTS added, reaching a maximum of 3.4 MPa with the 20
279 wt.% of WTS addition. Subsequently, the tendency began to decrease as the addition of WTS
280 increased. Heah et al. (Heah et al., 2012) attributed the differences found in the σ_c of
281 geopolymers formulated with non-dehydroxylated kaolin to the variations in the $\text{SiO}_2/\text{Al}_2\text{O}_3$,
282 $\text{SiO}_2/\text{Na}_2\text{O}$, and $\text{Al}_2\text{O}_3/\text{Na}_2\text{O}$ molar ratios. In this assumption, given the poor reactivity of
283 both clay and WTS (see Fig. 3), it is expected that the $\text{SiO}_2/\text{Na}_2\text{O}$ and $\text{Al}_2\text{O}_3/\text{Na}_2\text{O}$ molar
284 ratios would be very low in all the AACs formulated. This fact justifies the low compressive
285 strength results obtained. Only the calcium contribution in the formation of gels, giving C-
286 S-H and C-(N)-A-S-H type gels structures, can justify the slight increase in compressive
287 strength for some formulations, as some authors suggested (Provis, 2014). It should be noted
288 that the formulation offering the greatest resistance to hydrolytic degradation (20 wt.% of
289 WTS, see Table 3) was also the one exhibiting the greatest compressive strength. This shows
290 the structural cohesion of the cementitious phase.

291 3.4. Chemical stability

292 Table 3 shows the chemical stability tests results for the different AACs, where three
293 formulations succeed in boiling water. Both specimens formulated with 0 wt.% and 80 wt.%
294 of WTS failed during the tests, collapsing their structure. In these cases, the expected network
295 was not formed, and the main cementitious phase, probably dry water glass (Na_2SiO_3), was
296 not stable and consistent enough under the tests conditions. Furthermore, although the

297 specimen formulated with 40 wt.% of WTS as precursor passed the tests, the sample lost
298 more than 10 % of its mass and was therefore considered failed. This mass loss was enough
299 to affect the structural consistency of the binder. Hence, three formulations presented the
300 expected integrity, showing that these AACs formulations resisted to hydrolytic degradation
301 and maintained the structural cohesion. This fact indicates the binder phases were not due to
302 the water glass drying but rather to the alkali activation of the precursors.

303 3.5. Environmental behaviour

304 Leaching tests for granular waste materials were performed to assess the potential
305 environmental impact of the AACs formulated using waste as precursor. The standard
306 leaching test EN 12457-4 was conducted for the three AACs formulation that did not show
307 the hydrolytic degradation (see Table 3), and the mean results of the duplicates are shown in
308 Table 4. The leaching tests results for both precursors (clay and WTS) and the limits and
309 criteria of non-hazardous and hazardous waste are also presented in Table 4.

310 In general, from Table 4 can be seen that the concentrations of heavy metals and
311 metalloids in leachates obtained for both precursors and the three AACs formulations were
312 below the limits established for their classification as non-hazardous waste. Most of the
313 metal(loid)s studied are below the threshold for classification as inert material. Only Cr and
314 As slightly exceed the limit of inert, being well below the threshold of non-hazardous waste.
315 Note the slight increase of the metal(loid)s concentrations in leachates generated from the
316 AACs, compared to the raw materials used in their formulations. This fact is due to the high
317 alkali pH and therefore, the strong precursor activation. The small differences between the
318 AACs formulations were more likely due to the heterogeneity of clay and WTS than
319 differences between AACs formulations.

320 **4. Conclusions**

321 The possibility of formulating AACs using a commercial raw clay as precursor without
322 prior thermal dehydroxylation treatment has been studied. Partial substitutions of raw clay
323 for WTS have been performed to provide an added value to this waste. AACs with WTS
324 content up to 80 wt.% were formulated and their properties were characterised. The following
325 conclusions must be highlighted:

- 326 - The addition of WTS affected the properties of the AACs, adding Al_2O_3 and CaO ,
327 promoting the formation of C-S-H and C-A-S-H gels.
- 328 - The availability of SiO_2 and Al_2O_3 for both precursors was low, hence most of the
329 precursors remained unreacted, and the amount of newly formed binder phases was
330 low.
- 331 - Low compressive strengths were obtained for the AACs, similar to other non-
332 dehydroxylated clay-based AACs.
- 333 - The optimal formulation was reached by adding 20 wt.% of WTS. The AACs
334 presented the maximum content of C-S-H and C-A-S-H gels, the highest compressive
335 strengths and the best chemical stability.
- 336 - The effect of WTS addition to the environmental impact was negligible. The contents
337 of heavy metals and metalloids were well below the limits for non-hazardous
338 materials for all AACs and precursors.

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510

Table 1. Formulations of AACs using clay and WTS as precursors.

	(wt.% - wt.%)					
Clay - WTS	100 - 0	95 - 5	90 - 10	80 - 20	60 - 40	20 - 80
Reference	WTS-0	WTS-5	WTS-10	WTS-20	WTS-40	WTS-80

Table 2. Chemical composition (XRF) of clay and WTS used as precursors.

	SiO₂	Al₂O₃	Fe₂O₃	K₂O	TiO₂	CaO	MgO	MnO	P₂O₅	Na₂O	*LOI
Clay	59.87	22.87	6.33	1.38	1.04	0.73	0.61	0.02	0.06	0.32	6.09
WTS	28.25	15.72	3.10	2.16	0.45	10.65	2.04	0.80	0.80	0.29	34.72

*LOI: Loss of ignition at 1100°C

Table 3. Chemical stability according to the boiling water test (Zhu et al., 2018; Davidovits, 2020).

WTS (wt.%)	Initial weight (g)	Final weight (g)	Loss (g)	Lost (%)	Result
0	11.587	-	-	-	Failure
5	11.107	10.399	0.708	6.37	Success
10	11.302	10.680	0.622	5.50	Success
20	11.544	11.168	0.376	3.26	Success
40	11.663	10.093	1.57	13.46	Failure
80	11.762	-	-	-	Failure

Table 4. Leaching test results following the EN 12457-4 standard ($\text{mg}\cdot\text{kg}^{-1}$).

	Clay	WTS	WTS-5	WTS-10	WTS-20	Inert	Non-hazardous	Hazardous
As	0.112	0.265	1.527	1.630	1.574	0.5	2	25
Ba	0.149	0.860	0.210	0.650	0.442	20	100	300
Cd	<0.001	<0.001	<0.001	<0.001	<0.001	0.04	1	5
Cr	0.025	0.013	0.975	0.983	0.839	0.5	10	70
Cu	0.150	0.080	0.542	0.757	1.318	2	50	100
Hg	<0.002	<0.005	<0.002	<0.002	<0.002	0.01	0.2	2
Mo	0.040	0.030	0.127	0.128	0.130	0.5	10	30
Ni	0.005	0.065	0.155	0.105	0.110	0.4	10	40
Pb	0.060	0.036	0.229	0.235	0.318	0.5	10	50
Se	0.022	<0.01	<0.02	<0.02	<0.02	0.1	0.5	7
Sb	0.011	<0.01	<0.01	<0.01	<0.01	0.06	0.7	5
Zn	0.052	0.173	0.875	0.952	1.201	4	50	200

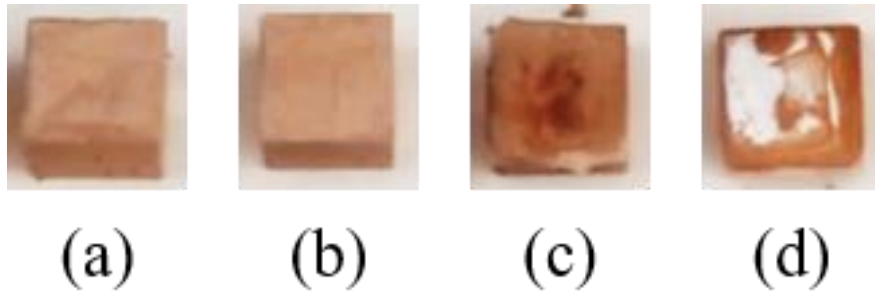


Fig.1. Cubic specimens (25x25x25 mm size) of clay AACs formulated with NaOH as activator (a) 2M, (b) 4M, (c) 8M and (d) 12M.

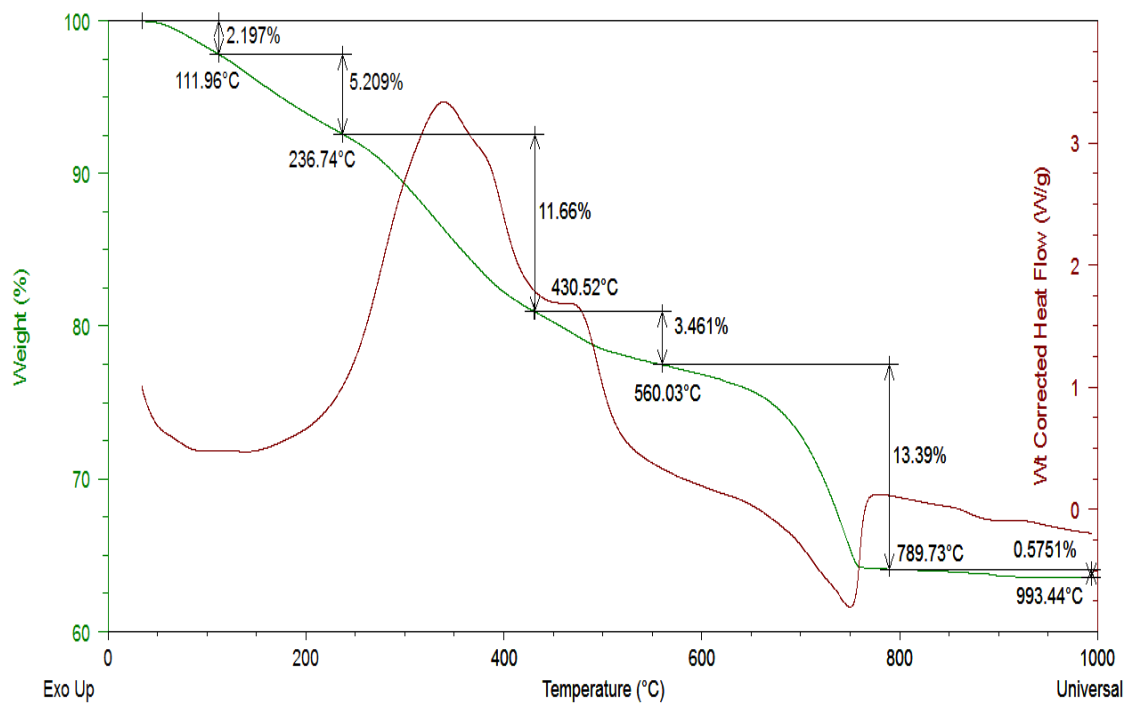


Fig. 2. TGA of WTS used as a precursor.

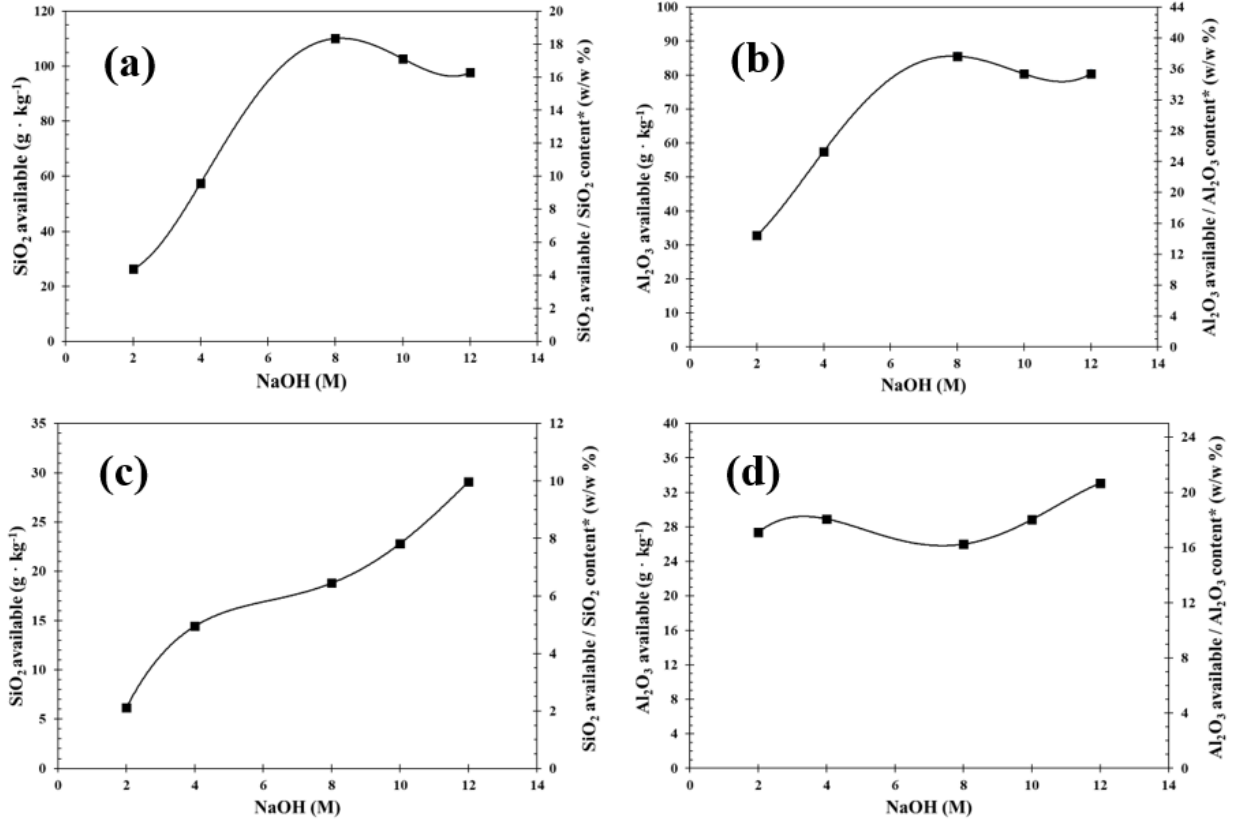


Fig. 3. Availability of SiO₂ and Al₂O₃ resulting from the chemical attacks of (a,b) clay and (c,d) WTS. *Results obtained from the XRF analysis (Table 2).

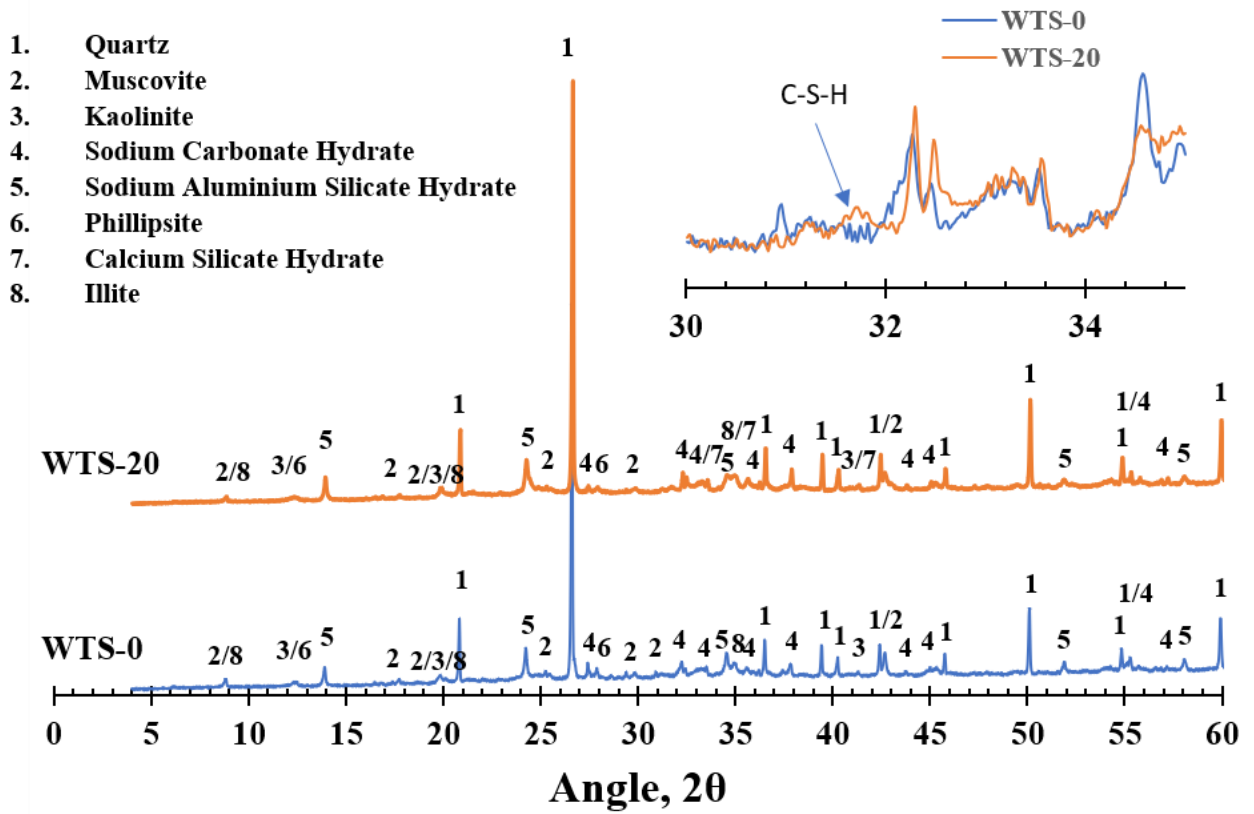


Fig.4. XRD diffractograms of WTS-0 and WTS-20 samples.

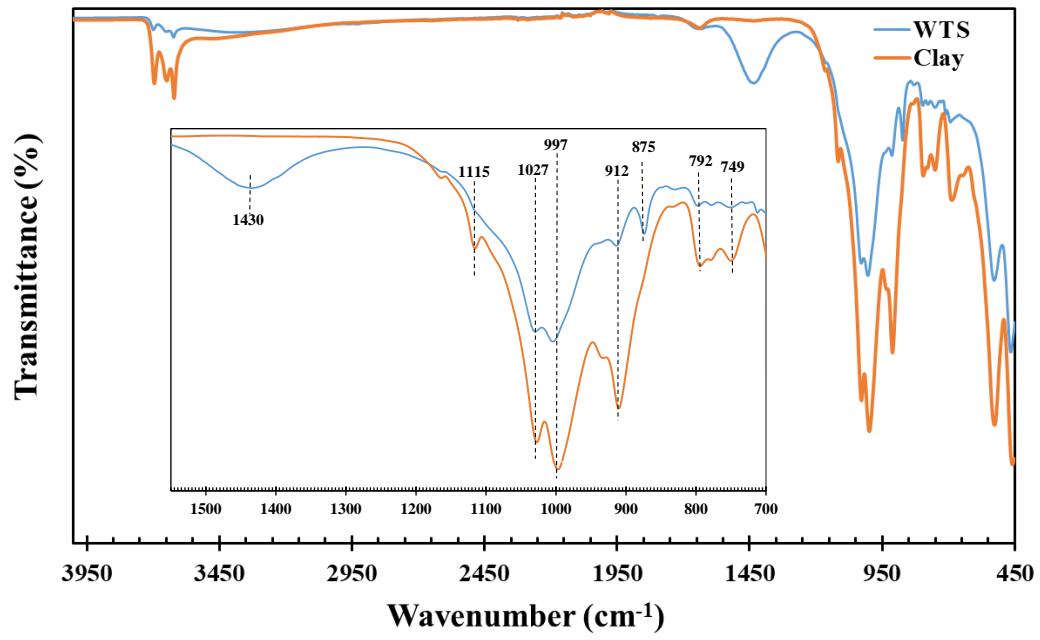


Fig. 5. FT-IR spectra of clay and WTS before the alkali activation.

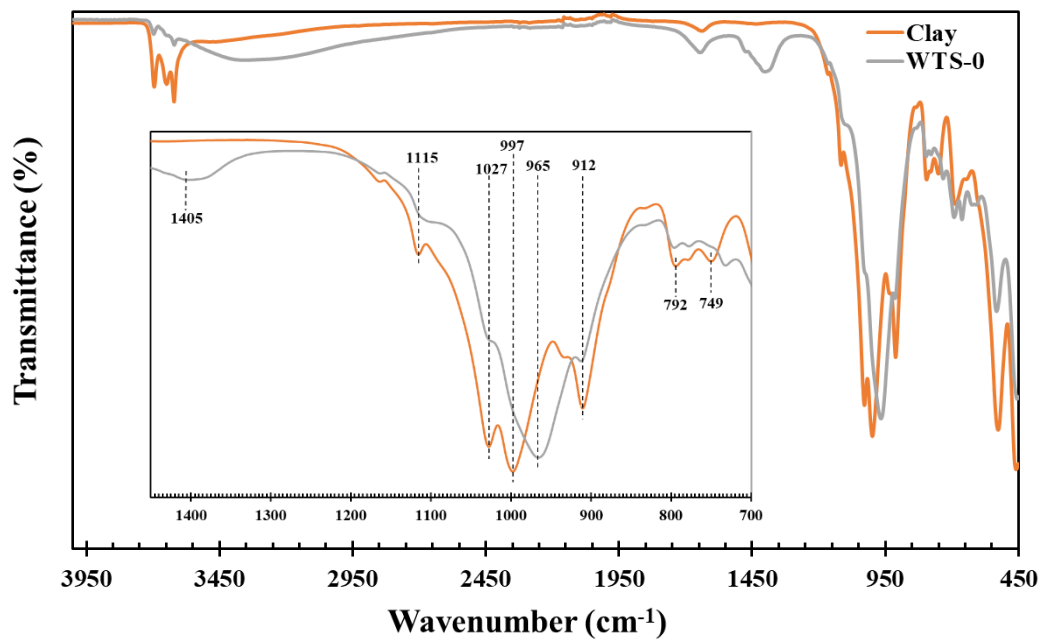


Fig. 6. FT-IR spectra of clay and WTS-0 samples.

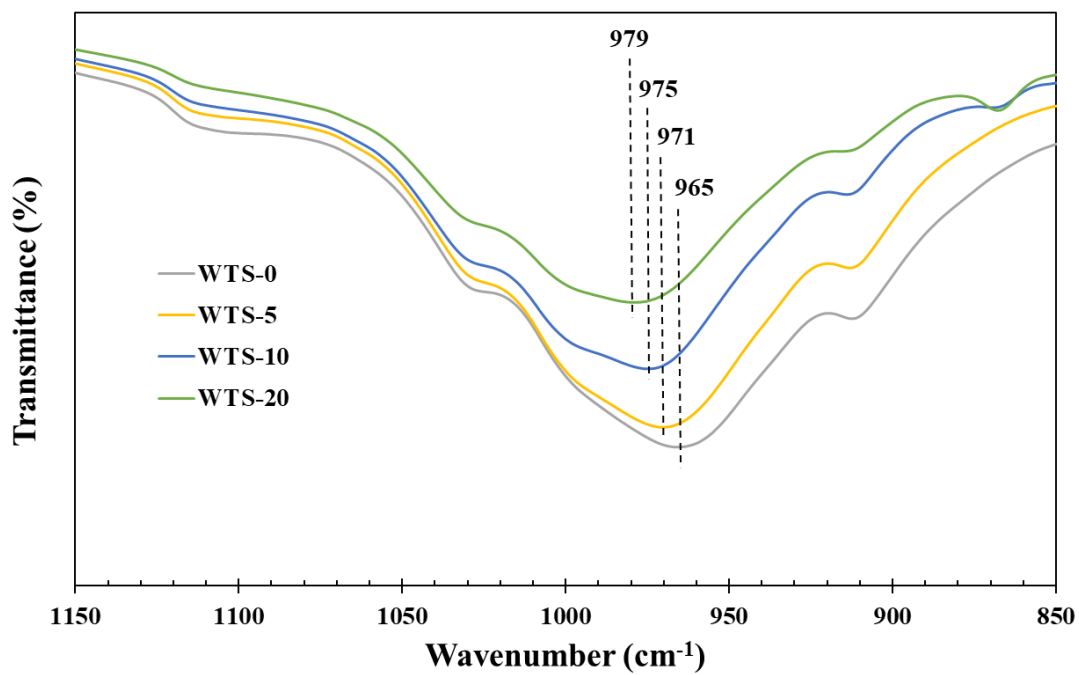


Fig. 7. FT-IR spectra of AAC where clay was replaced as precursor by different percentages (wt.%) of WTS.

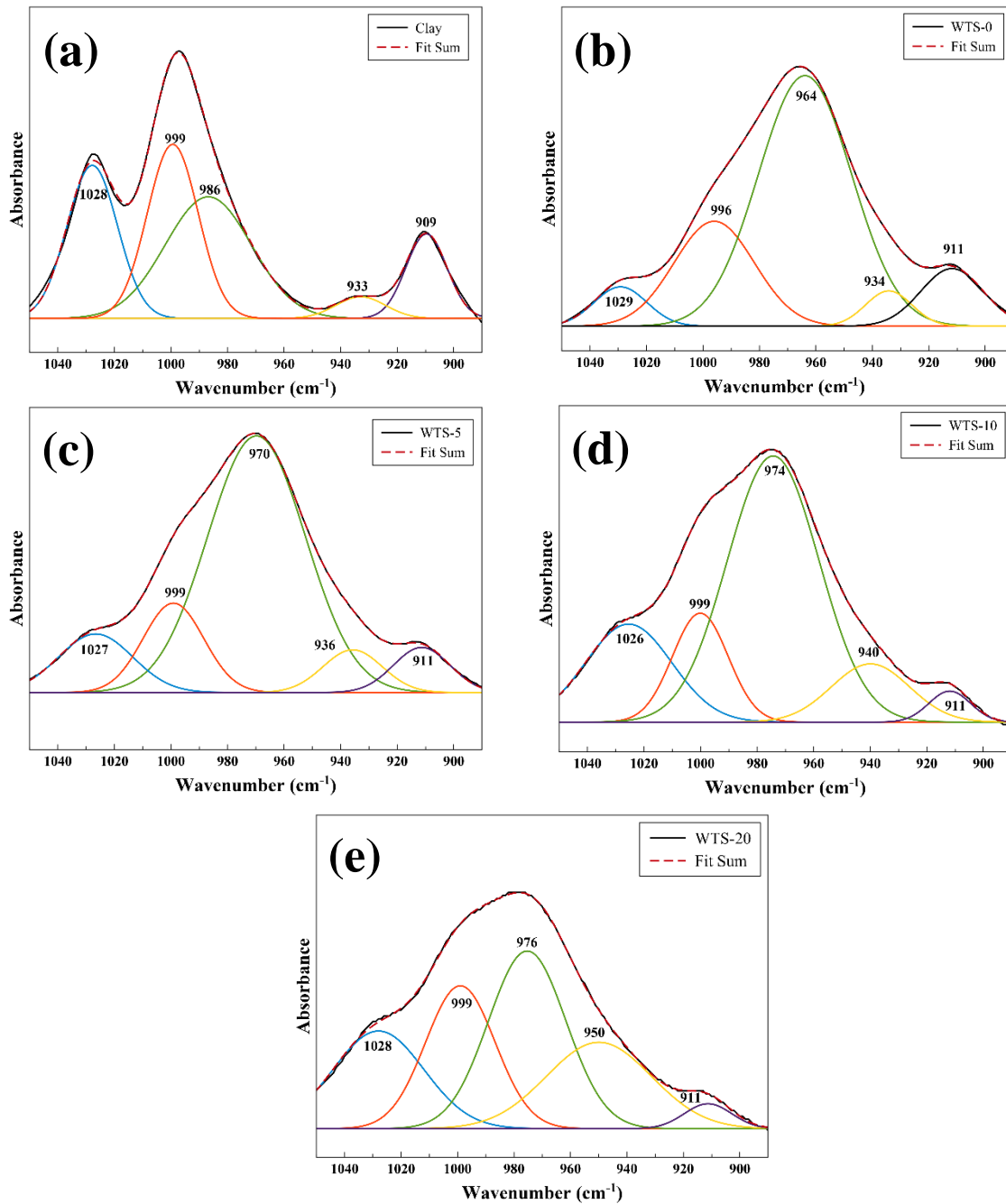


Fig 8. FT-IR spectral deconvolution of the midwavenumber region (1100 – 850 cm^{-1}) for (a) clay and (b) WTS-0, (c) WTS-5, (d) WTS-10 and (e) WTS-20 samples.

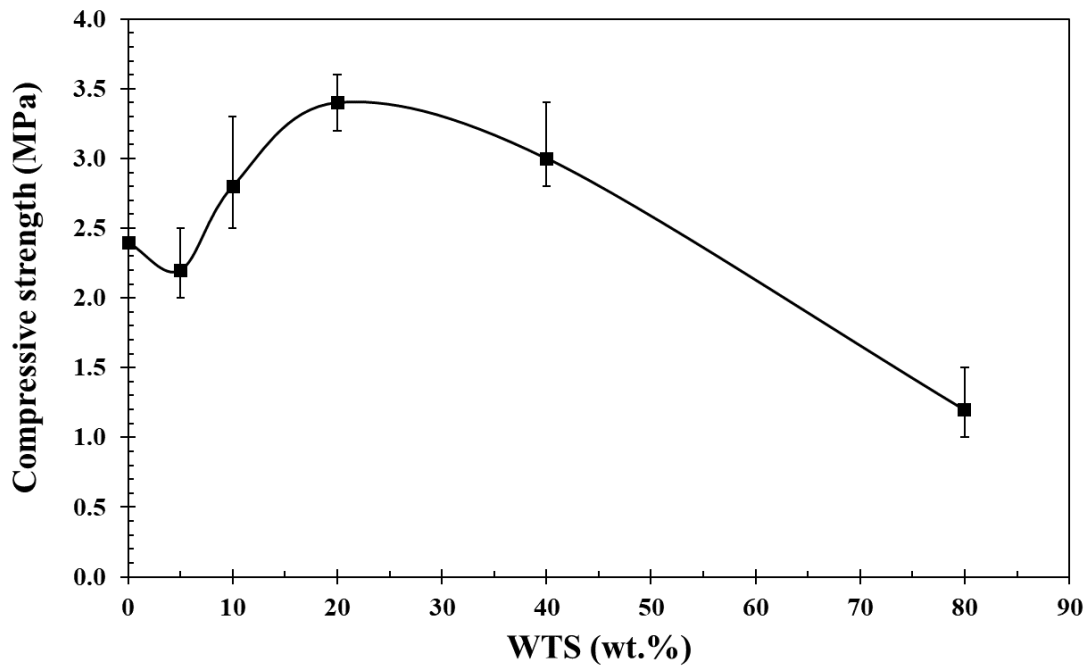


Fig. 9. Compressive strength (σ_c) of AAC specimens formulated using different percentage of WTS as precursor.