

A digital holography technique for generating beams with arbitrary polarization and shape

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ABSTRACT

A method for generating beams with arbitrary polarization and shape is proposed. Our design requires the use of a Mach-Zehnder set-up combined with translucent liquid crystal displays in each arm of the interferometer; in this way, independent manipulation of each transverse beam components is possible. The target of this communication is to develop a numerical procedure for calculating the holograms required for dynamically encode any amplitude value and polarization state in each point of the wavefront. Several examples demonstrating the capabilities of the method are provided.

Keywords: spatially-variant polarization, computer-generated holography, spatial light modulators

1. INTRODUCTION

Recently, the interest for arbitrary spatially-variant polarized beams (ASPB) has increased significantly due to their special properties compared to homogeneously polarized beams thus enhancing the functionality of optical systems.¹ The generation process of ASPB using spatial light modulators (SLM), which act as controlled optical phase retarders or amplitude modulators, is still a challenging task.²⁻⁵ The aim of this communication is to develop an optical system able to encode and reconfigure both the polarization and the shape of the beam.

Our approach is based on a Mach-Zehnder interferometric configuration combined with a translucent phase-mostly modulator in each path of the interferometer.^{6,7} To separate horizontal and vertical component from each other the oscillation direction of one of the beams is rotated 90°. The transverse components of the incident light beam are processed independently and modified by means of specifically designed holograms. Subsequently, the components are recombined and led into the on-axis reconstruction system consisting of a 4f lens arrangement. In particular, the holograms have been calculated by means of an algorithm derived from Arrizon's method to encode complex optical signals using phase-mostly SLMs.⁸⁻¹⁰ This approach entitles us to encode any polarization state in each point of the wavefront even when the displays used are not able to modulate the phase from 0 to 2π and present amplitude coupling. Additionally, the amplitude of the wavefront may also be modeled so as to obtain a particular shape.

The numerical procedure to generate the holograms is discussed and illustrative examples with complex polarization configurations and shapes are also considered. The paper is organized as follows: in section 2 we present the optical setup required to generate ASPB and in section 3 the algorithm for calculating complex-valued phase-mostly holograms is introduced. Some computational results are presented in section 4 whereas in section 5, the main conclusions are summarized.

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2. OPTICAL SETUP

Figure 1 presents the proposed experimental setup. A polarized laser beam is split up into two beams by means of a polarizing beam splitter PBS_1 , being the incident polarization direction set at 45° with respect to the x -axis. Let $\mathbf{E}(x, y)$ a cylindrical ASPB whose electric field vibrates within the plane xy , normal to the propagation direction z . This beam is described by

$$\mathbf{E}(x, y) = E_x(x, y)\mathbf{i} + E_y(x, y)\mathbf{j}, \quad (1)$$

where

$$\begin{aligned} E_x(x, y) &= E_{x0}(x, y) \exp(i\phi_x(x, y)) \quad \text{and} \\ E_y(x, y) &= E_{y0}(x, y) \exp(i\phi_y(x, y)), \end{aligned}$$

are the complex amplitudes in every point (x, y) and $\phi_x(x, y)$ and $\phi_y(x, y)$ are the corresponding phase shifts. Notice that the amplitude and the polarization direction of $\mathbf{E}(x, y)$ can be different in every point. The total phase difference is $\phi(x, y) = \phi_x(x, y) - \phi_y(x, y)$.

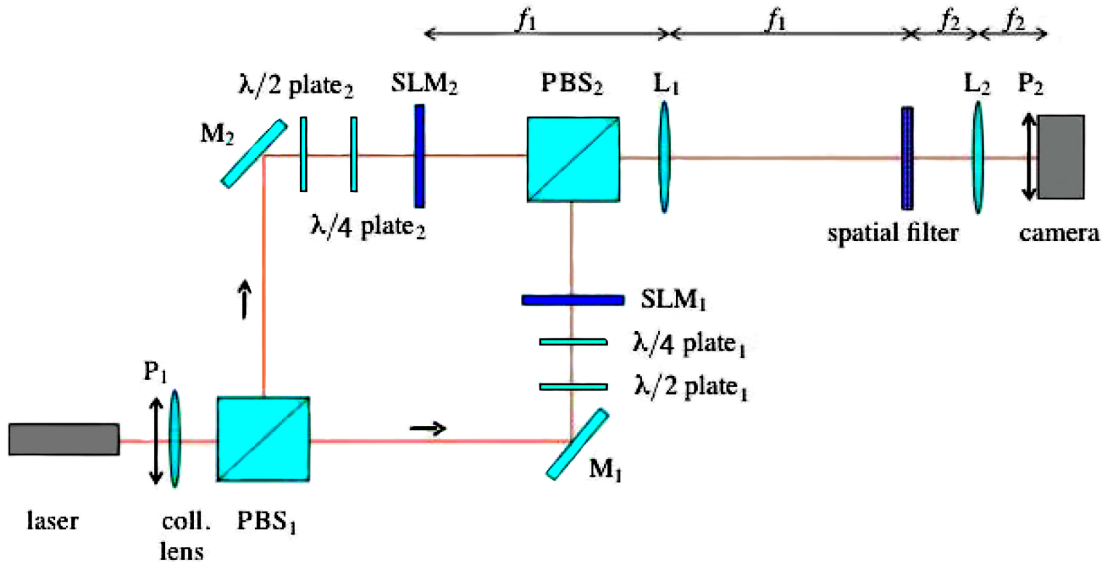


Figure 1: Sketch of the experimental setup.

A collimating lens aligns the entering unpolarized HeNe laser beam to propagate parallel along the optical path. The beam passes through linear polarizer P_1 (set at 45° with respect to the x direction) and a polarizing beam splitter PBS_1 . Reflected by mirrors M_1 or M_2 , the split beams pass through different wave plates which rotate the oscillating plane and set the modulator in order to achieve the expected response of the SLM. Afterward, light passes through modulators SLM_1 or SLM_2 . The displays used are two translucent twisted nematic Holoeye HEO 0017¹¹ with a resolution of 1024×768 pixels and $32 \mu m$ of pixel pitch. Then, light is recombined by means of the second polarizing beam splitter PBS_2 and led into the on-axis reconstruction system consisting of a $4f$ -Fourier lens system with L_1 with focal length f_1 and L_2 with focal length f_2 , respectively. Notice that a spatial filter in the back focal plane of L_1 is required for removing non-required higher-order diffracted terms generated by the hologram. Finally, the induced polarization is evaluated by analyzer P_2 and the CCD camera. The output field ($E_{out}(x, y)$) at the camera plane is

$$\mathbf{E}_{out}(x, y) = E_x(x, y)h_x(x, y)\mathbf{i} + E_y(x, y)h_y(x, y)\mathbf{j}, \quad (2)$$

where $h_x(x, y)$ and $h_y(x, y)$ are the computer-generated holograms for the x - and the y -component, respectively.

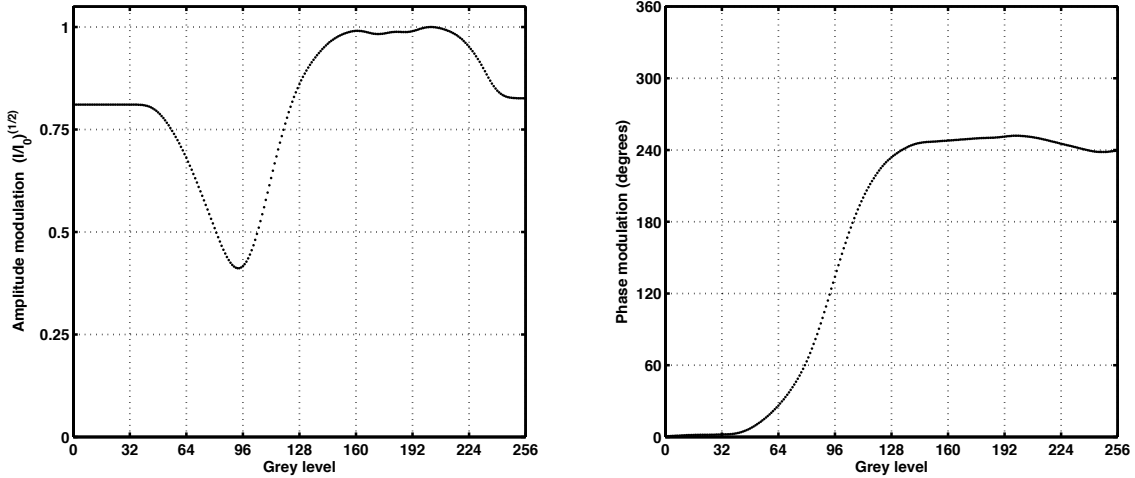


Figure 2: Modulation response for the Holoeye display: (a) amplitude and (b) phase.

Figure 2a show the measured transmittance as a function of the displayed gray level for SLM₁; the second one (SLM₂) performs in a very similar way. It is quite apparent that the amplitude is not constant so no phase-only modulation would be possible using this device. On the other hand, the phase (shown in Figure 2b) presents a nearly linear behavior when the gray level is within the interval 32 to 128. Note that only phase values from 0° to 240° can be reached. The amplitude-phase coupling can be overcome using the codification method explained in the next section.

3. CODIFICATION PROCEDURE

Arrizón developed an on-axis holography algorithm for encoding complex optical signals in SLMs with arbitrary amplitude and phase distributions.⁹ This method has been found very suitable for generating ASPB. Now, we briefly summarize the steps required to generate such holograms. Figure 3a shows the set of complex values accessible by SLM₁ (Figures 2a and 2b) using a polar diagram. Let C_{nm} a complex value at position (n, m) . If C_{nm} does not belong to the modulation curve M , it can be written as the combination of phasors $M_{nm}^1, M_{nm}^2, E_{nm}^1$ and E_{nm}^2 (see Figure 3a):

$$\begin{aligned} C_{nm} &= M_{nm}^1 - E_{nm}^1 \quad \text{and} \\ C_{nm} &= M_{nm}^2 - E_{nm}^2 \end{aligned} \quad (3)$$

where M_{nm}^1 and $M_{nm}^2 \in M$. Selecting M_{nm}^1 and M_{nm}^2 in such a way that $E_{nm}^1 = -E_{nm}^2$ then

$$C_{nm} = (M_{nm}^1 + M_{nm}^2) / 2 \quad (4)$$

Figure 3b shows (blue dots) all possible values that can be obtained as a combination of two points belonging to the modulation curve following the condition $E_{nm}^1 = -E_{nm}^2$. Notice that a subset of these values lies within a semicircle of transmittance $T = 0.4$ (black line). Moreover, the diameter of this semicircle forms an angle of 30° relative to the arbitrary phase origin. Full complex modulation can be achieved using a second display, provided that SLM₂ performs a similar modulation curve M . Fine tuning the optical path of the second arm, the phase origin in SLM₂ can be modified and, consequently, if this phase is delayed 180° with respect to the other display, the system can access any complex value within the circle of transmittance $T = 0.4$.

Following the cell-oriented holograms approach, four pixels in the SLM are required to encode each complex value C_{nm} , as depicted in Figure 4. It has been demonstrated¹⁰ that terms M_{nm}^1 and M_{nm}^2 are reconstructed on axis whereas the not desired terms E_{nm}^1 and E_{nm}^2 are diffracted off-axis; to avoid its contribution, an spatial filter in the back focal plane of lens L_1 has to be used.

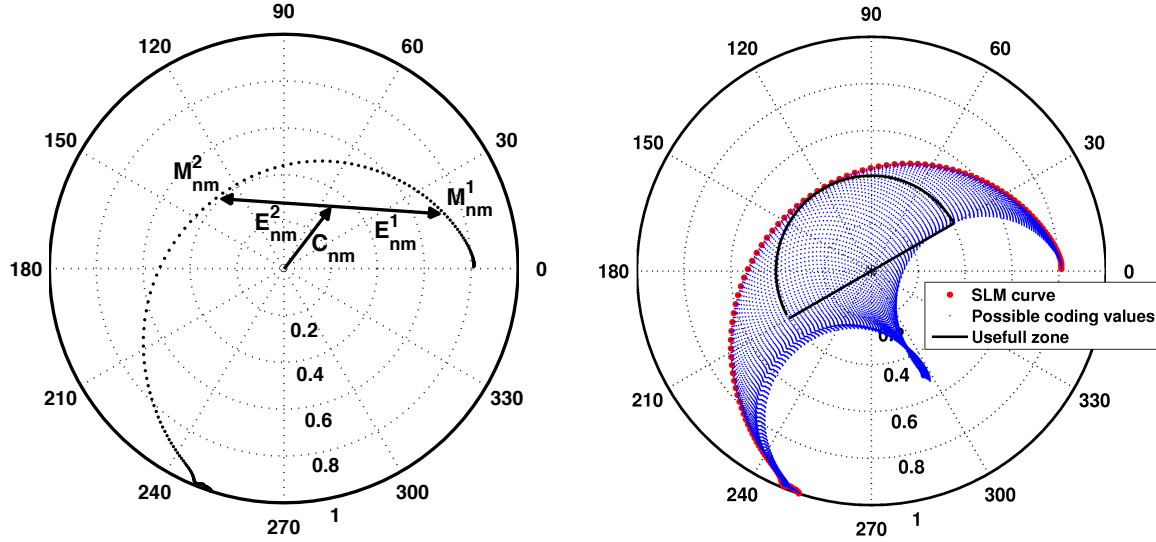


Figure 3: (a) Polar representation of the values accessible by SLM_1 . (b) Accessible values (in blue) using the codification procedure. The black solid line delimits the useful values.

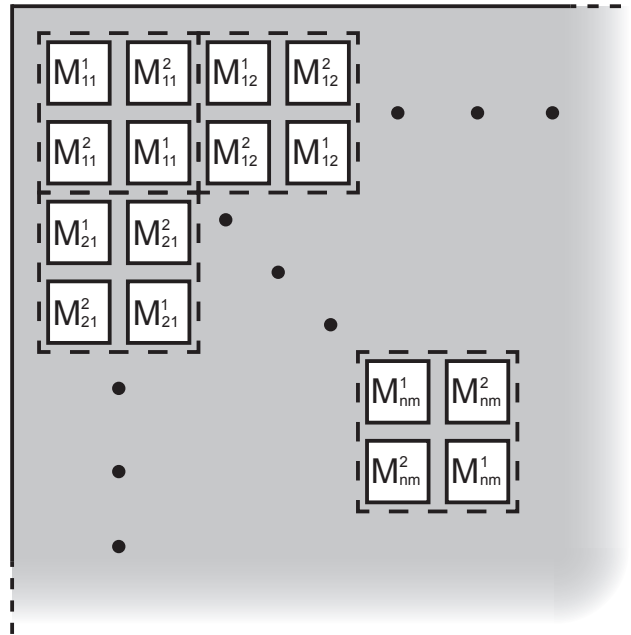


Figure 4: Cell-oriented hologram approach.

4. NUMERICAL EXPERIMENTS

Figure 5 show two examples of generalized ASPB beams. On the left, a constant amplitude beam displaying a complicated linearly polarized pattern is shown. The inner mode is radially polarized whereas in the outer mode, the oscillation orientation changes according to $\theta(x, y) = 4 \tan^{-1}(y/x)$. On the right, Figure 5b shows a Hermite-Gauss mode (2,1) with different polarization states in each section of the beam. Figure 6 displays the generated holograms for each display for the two examples considered. Finally, Figure 7 shows the numerical simulation of the irradiance of the output field at the the camera plane ($|\mathbf{E}_{out}(x, y)|^2$) when the orientation of the analyzer is set at different positions ($0^\circ, 45^\circ, 90^\circ$ and 135°).

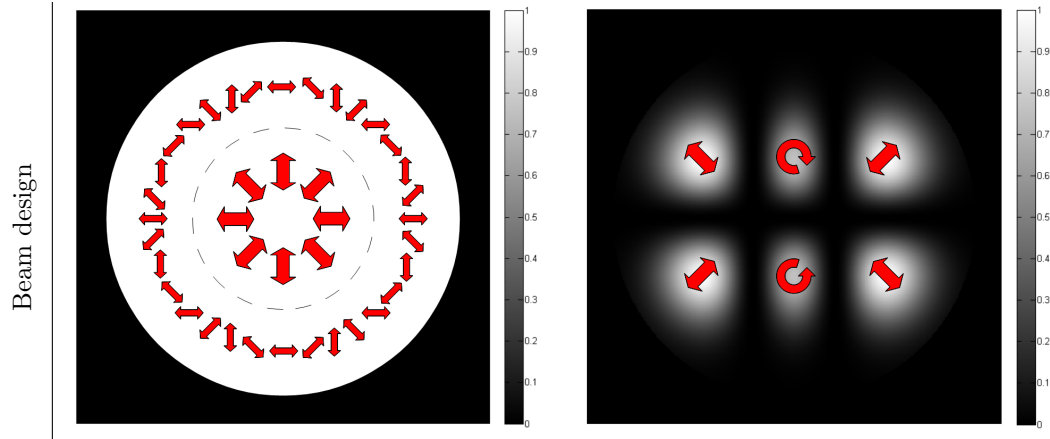


Figure 5: Examples of ASPB intensity patterns: (a) Constant amplitude with radial and star-like polarization, (b) Hermite-Gauss mode (2,1) combining linear and circular polarization.

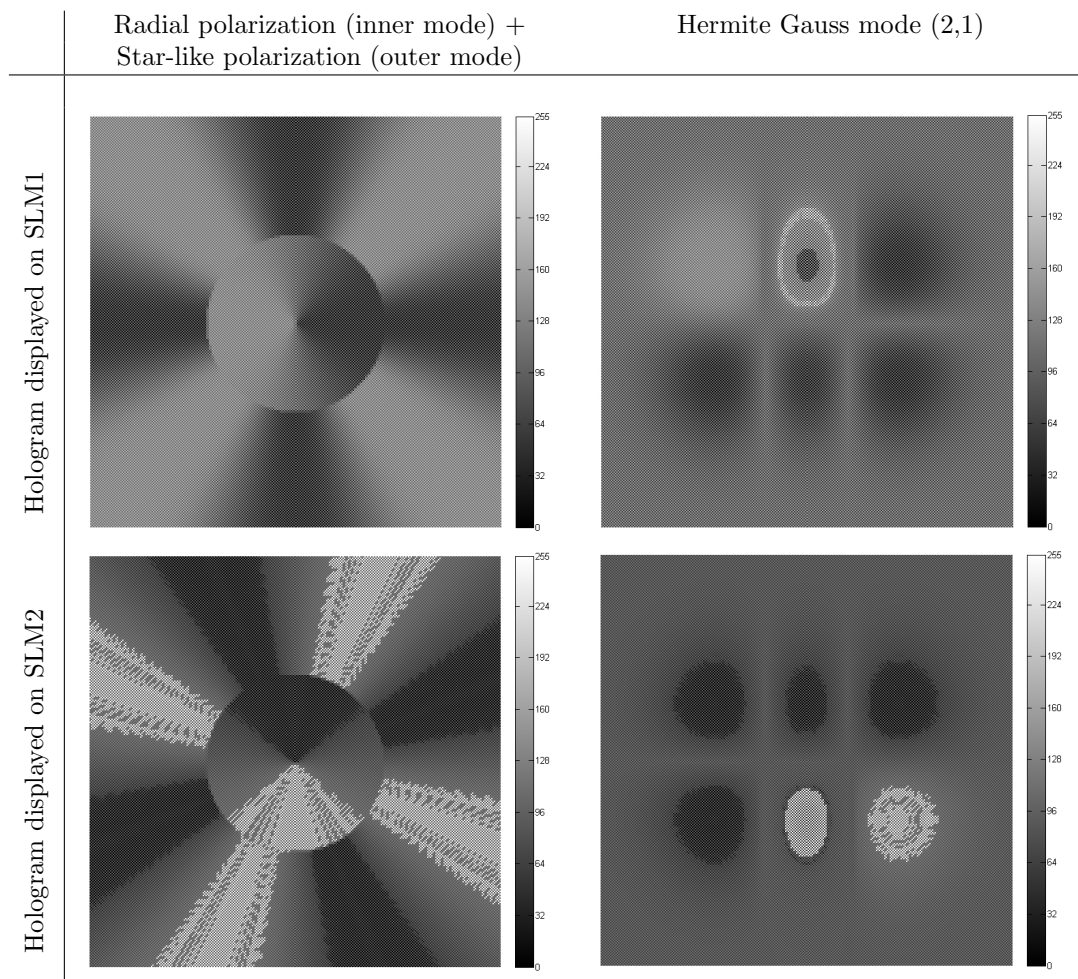


Figure 6: Calculated holograms.

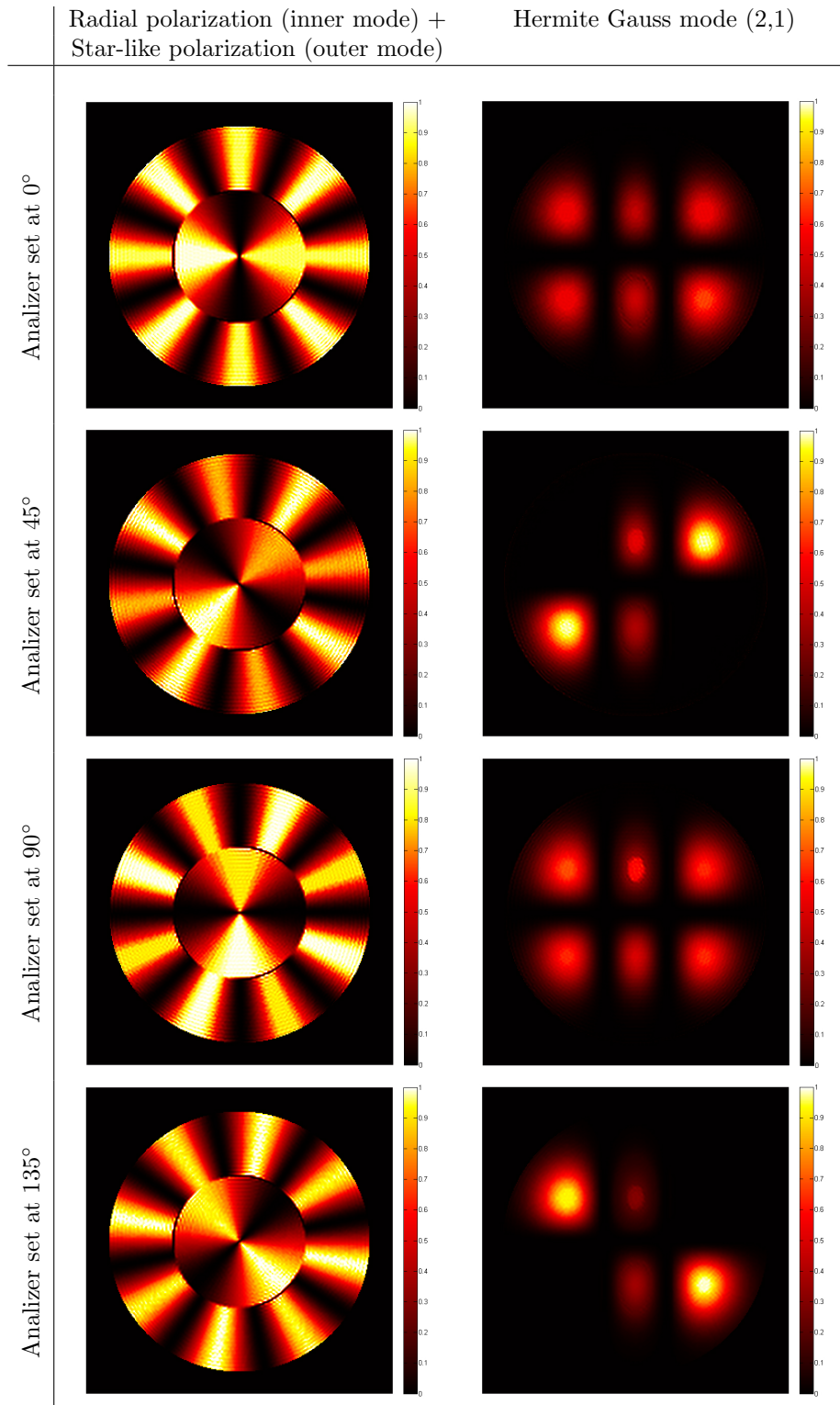


Figure 7: Simulated intensity patterns for different positions of the analyzer.

5. CONCLUDING REMARKS

In this communication we presented a method for generating light beams with controlled polarization and shape using an optical system based on a Mach-Zehnder setup. The transverse components of the beam can be manipulated independently through the use of liquid crystal displays in each arm of the interferometer. Given the limited modulation capabilities of the displays, computer generated holograms have to be used to encode the information. In particular, an adaptation of Arrizón's double-pixel approach was implemented; this method has been demonstrated as very suitable for this kind of problems. Numerical simulations of ASPB with complex polarization distributions and shapes have been carried out demonstrating the feasibility of the proposed technique.

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